

# Homogenisation for transient waves in periodic 1D media: dispersion, interfaces and source points

Rémi Cornaggia

Bojan B. Guzina<sup>1</sup>, Bruno Lombard<sup>2</sup>

Journée Ondes, GDR MePhy – MecaWave  
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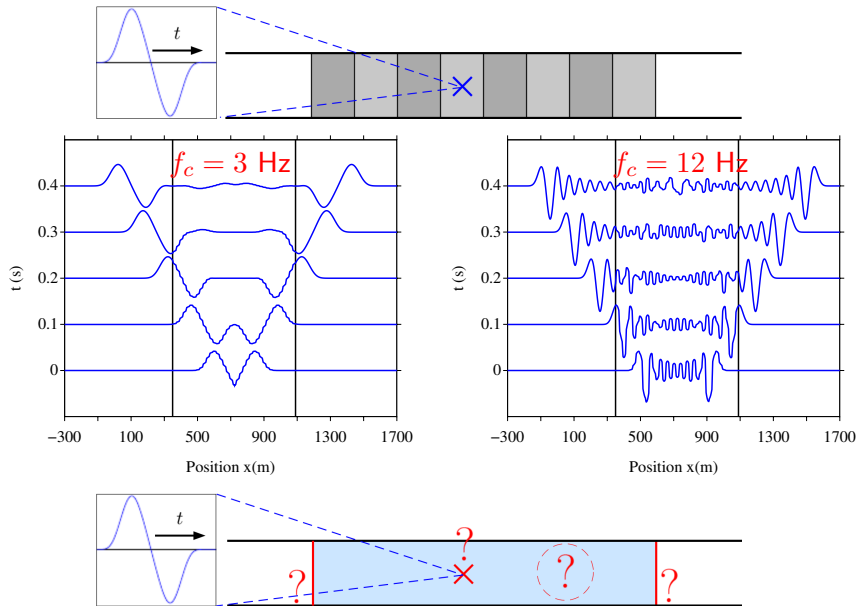


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<sup>1</sup>Department of Civil, Environmental and Geo-Engineering, University of Minnesota, Twin Cities, MN, USA

<sup>2</sup>Laboratoire de mécanique et d'acoustique, Aix-Marseille Université, CNRS, Centrale Marseille

# Dispersion, interfaces and source points

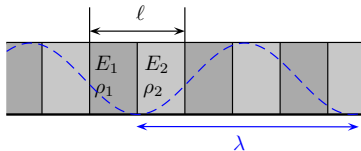


# Contents

- 1 Second-order asymptotic homogenization for waves in 1D domains
  - Second-order models
  - Hyperbolic formulation
- 2 Transmission conditions
- 3 Application to point sources
- 4 Conclusions and perspectives

# Two-scale asymptotic homogenization in a 1D periodic medium

[Sanchez-Palencia, 1974, Bensoussan et al., 1978, Cioranescu and Donato, 1999] ...



- Wave equation in a  $\ell$ -periodic medium

$$\rho\left(\frac{x}{\ell}\right) \frac{\partial^2 u_\ell}{\partial t^2} - \frac{\partial}{\partial x} \left[ E\left(\frac{x}{\ell}\right) \frac{\partial u_\ell}{\partial x} \right] = 0$$

- Reference wavelength  $\lambda > \ell$

- Separated variable solution featuring a mean field  $U(x, t)$  and cell functions  $P_j(x/\ell)$ :

$$u_\ell(x, t) = U(x, t) + \ell U_{,x}(x, t) P_1\left(\frac{x}{\ell}\right) + \ell^2 U_{,xx}(x, t) P_2\left(\frac{x}{\ell}\right) + o(\ell^2),$$

- Effective wave equations for the mean field, from [Wautier and Guzina, 2015]

$$\frac{1}{c_0^2} U_{,tt} - U_{,xx} - \ell^2 \left( \beta_x U_{,xxxx} - \frac{\beta_m}{c_0^2} U_{,xxtt} - \frac{\beta_t}{c_0^4} U_{,tttt} \right) = 0, \quad \beta_x - \beta_m - \beta_t = \beta$$

- ... featuring effective coefficients computed from the cell functions:

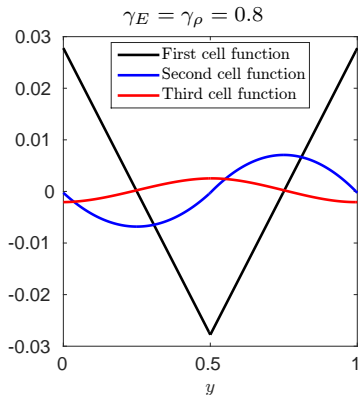
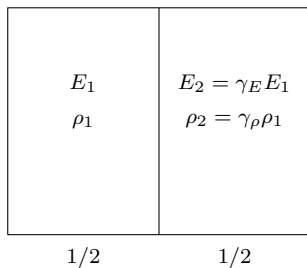
$$c_0^2 = \frac{\mathcal{E}_0}{\varrho_0} \quad \text{and} \quad \beta = \left[ \frac{\mathcal{E}_2}{\mathcal{E}_0} - \frac{\varrho_2}{\varrho_0} \right] \quad \text{with} \quad \begin{cases} \rho_j = \langle \rho P_j \rangle, \\ \mathcal{E}_j = \langle E(P_j + P_{j+1,y}) \rangle \end{cases}$$

- ... and two degrees of freedom to choose  $(\beta_x, \beta_m, \beta_t)$ .

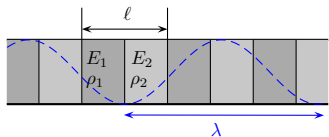
# Cell functions

$(P_1, P_2, P_3)$ : solutions of **static equilibrium problems** posed in the unit cell  $Y = [0, 1]$

$$\partial_y [E \partial_y P_j] = \mathcal{F}(E, \rho, P_{j-1}, P_{j-2}), \quad P_j \text{ is 1-periodic}, \quad \langle P_j \rangle = 0$$



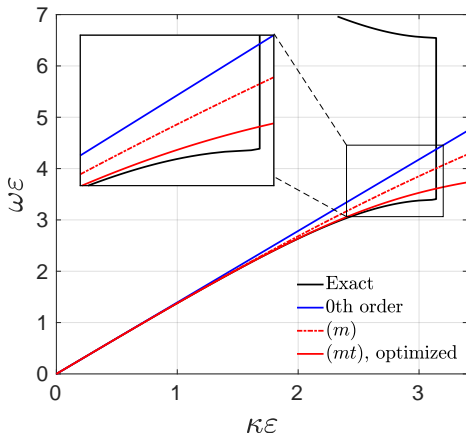
# Choosing a $(mt)$ model by fitting dispersion curves



Material contrasts:  $\frac{E_2}{E_1} = 6, \quad \frac{\rho_2}{\rho_1} = 1.5$

Phase ratio:  $\frac{\ell_2}{\ell_1} = 3$

( $\approx$  maximal dispersion [Santosa and Symes, 1991])



- Bloch wave:  $u(x, y; t) = \phi(y)e^{i(\kappa x - \omega t)}$   
 $\Rightarrow$  Dispersion relation  $\kappa = f(\omega)$
- 0th-order:  $U_{,tt} - c_0^2 U_{,xx} = 0$   
 $\Rightarrow$  non-dispersive
- 2nd-order  $(m)$ :  
 $\Rightarrow O((\kappa \ell)^2)$  approximation
- Optimized  $(mt)$ :  
 $\Rightarrow O((\kappa \ell)^4)$  approximation  
 [Pichugin et al., 2008,  
 Cornaggia and Guzina, 2020]

# Equivalent hyperbolic system for the $(mt)$ model

Second-order homogenization,  $(mt)$  model:

$$\frac{1}{c_0^2} \left[ 1 + \ell^2 \beta_m \partial_{xx} + \ell^2 \frac{\beta_t}{c_0^2} \partial_{tt} \right] U_{,tt} = U_{,xx}, \quad (\beta_m, \beta_t) \text{ obtained by fitting dispersion curve.}$$

“Stress gradient” system by [Forest and Sab, 2017]:

$$\begin{cases} \sigma = E \partial_x (u + \phi) \\ r = D \phi \end{cases} \quad \begin{cases} \rho \partial_{tt} u = \partial_x \sigma \\ \rho J \partial_{tt} \phi = \partial_x \sigma - r \end{cases}$$

So that: 
$$\frac{\rho}{E} \left[ 1 - \frac{E(1+J)}{D} \partial_{xx} + \frac{\rho J}{D} \partial_{tt} \right] u_{,tt} = u_{,xx}$$

$$\Rightarrow \begin{cases} \partial_t V - \frac{a}{\varrho_0} \partial_x S & = -\frac{a-1}{\varrho_0} r \\ \partial_t S - \mathcal{E}_0 \partial_x V & = 0 \\ \partial_t \varphi - \frac{a-1}{\varrho_0} \partial_x S & = -\frac{a-1}{\varrho_0} r \\ \partial_t r & = \frac{\mathcal{E}_0}{\ell^2 \beta} \varphi \end{cases}$$

- Macroscopic fields  $V = \partial_t (v + \phi)$  and  $S = \sigma$
- **Auxiliary fields**  $\varphi = \partial_t \phi$  and  $r$
- Parameter  $a = -\beta_m / \beta_t$  to select a  $(mt)$  model.

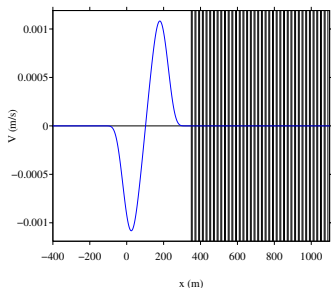
**Hyperbolicity and stability for:**

$$\beta_m < 0 \quad \text{and} \quad \beta_t > 0$$

# Outline

- 1 Second-order asymptotic homogenization for waves in 1D domains
  - Second-order models
  - Hyperbolic formulation
- 2 **Transmission conditions**
- 3 Application to point sources
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# First-order transmission conditions - regularization



- Fields of interest:

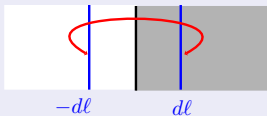
$$\begin{cases} (V, S) = (\partial_t U, E_- \partial_x U) & x < 0 \\ (V, S, \varphi, r) & x > 0 \end{cases}$$

- Transmission conditions from **total fields continuity**:

$$\begin{cases} V(0^-) = V(0^+) + \ell P_1(0) V_{,x}(0^+) \\ S(0^-) = S(0^+) + \ell \Sigma_1(0) S_{,x}(0^+) \end{cases}$$

$\Rightarrow$  Assymmetric conditions, sometimes **unstable**

**Spring-mass conditions across a thin interface**  $I_d = [-d\ell, d\ell]$  (additional  $o(\ell)$  error):



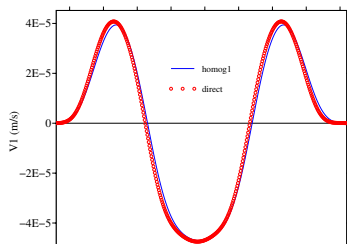
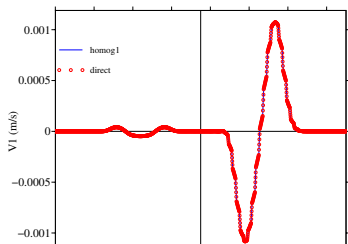
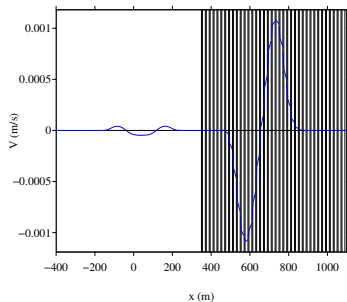
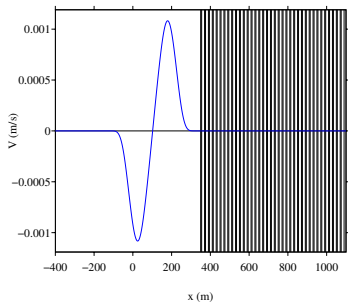
$$\begin{cases} \llbracket V \rrbracket_{I_d} = \ell A_1 \partial_t \langle S \rangle_{I_d} & A_1 = -P_1(0) \mathcal{E}_0^{-1} + d(E_-^{-1} + \mathcal{E}_0^{-1}) \\ \llbracket S \rrbracket_{I_d} = \ell B_1 \partial_t \langle V \rangle_{I_d} & B_1 = -\Sigma_1(0) \varrho_0 + d(\rho_- + \varrho_0) \end{cases}$$

**Stability** of {Hyperbolic system + transmission conditions} for  $A_1 \geq 0$  and  $B_1 \geq 0$

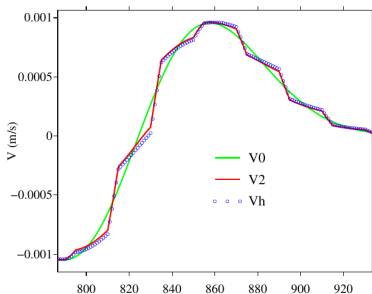
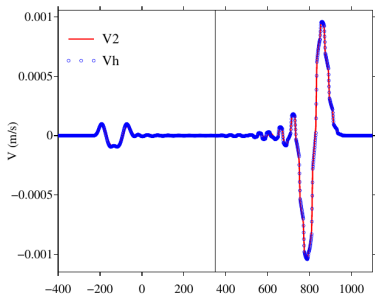
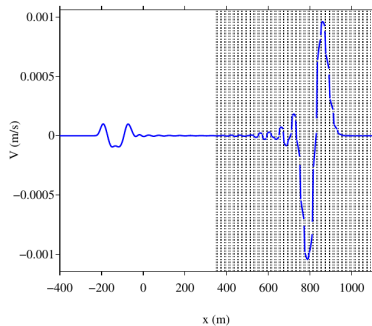
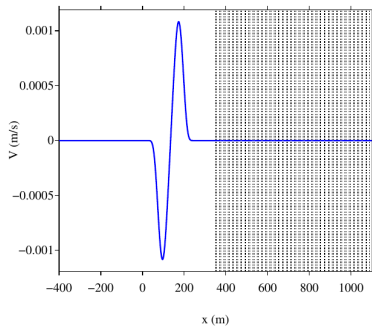
$$\Rightarrow \text{Choice of } d \geq d_{\min} := \max \left( \frac{E_- P_1(0)}{E_- + \mathcal{E}_0}, \frac{\varrho_0 \Sigma_1(0)}{\rho_- + \varrho_0}, 0 \right)$$

# Transmission conditions for $\varepsilon = \ell/\lambda_c \approx 0.04$ (Numerics by B. Lombard)

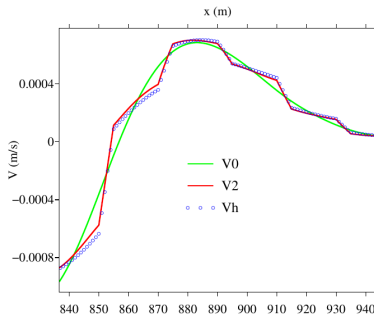
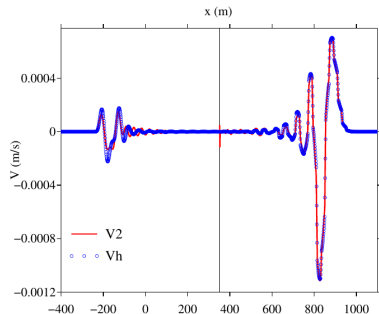
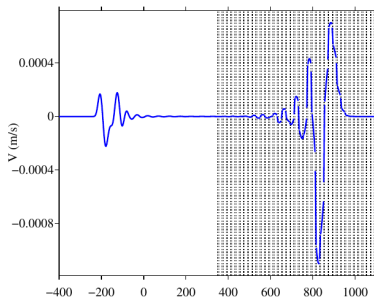
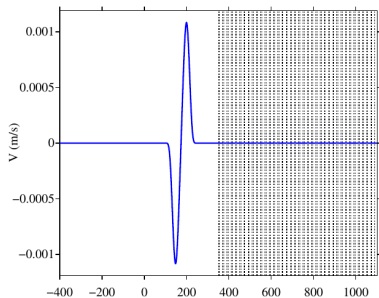
$E_{-}\rho_{-} = \mathcal{E}_0 g_0 \implies$  reflected wave is a 1st-order effect



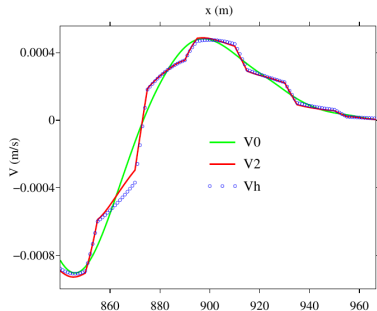
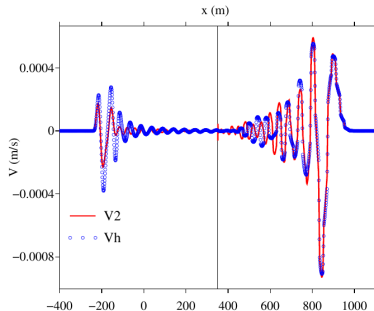
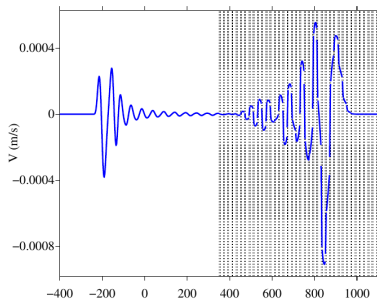
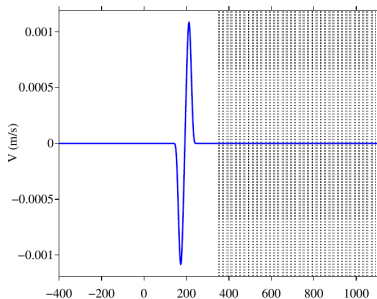
# Transmission conditions, increasing central frequency, $\varepsilon \approx 0.09$



# Transmission conditions, increasing central frequency, $\varepsilon \approx 0.13$



# Transmission conditions, increasing central frequency, $\varepsilon \approx 0.17$

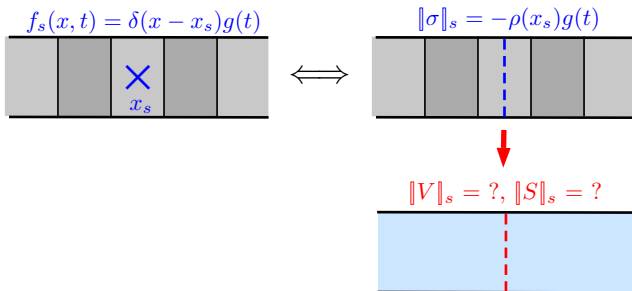


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In 1D, source points  $\Leftrightarrow$  interfaces with stress jumps

$$\begin{cases} \partial_t v_\ell - \frac{1}{\rho_\ell} \partial_x \sigma_\ell = \delta_s g(t) & x \in \mathbb{R} \\ \partial_t \sigma_\ell - E_\ell \partial_x v_\ell = 0 & x \in \mathbb{R} \end{cases} \Leftrightarrow \begin{cases} \partial_t v_\ell - \frac{1}{\rho_\ell} \partial_x \sigma_\ell = 0 & x < x_s \text{ and } x > x_s, \\ \partial_t \sigma_\ell - E_\ell \partial_x v_\ell = 0 & x < x_s \text{ and } x > x_s, \\ \llbracket v_\ell \rrbracket_s = 0 & x = x_s, \\ \llbracket \sigma_\ell \rrbracket_s = -\rho_s g & x = x_s, \end{cases}$$



# First-order correction

- **Same tools** (and no need for an enlarged interface):

$$\begin{cases} \llbracket V \rrbracket_s = \ell P_1(x_s/\ell) \frac{\rho_s}{\mathcal{E}_0} \partial_t g, \\ \llbracket S \rrbracket_s = -\rho_s g, \end{cases}$$

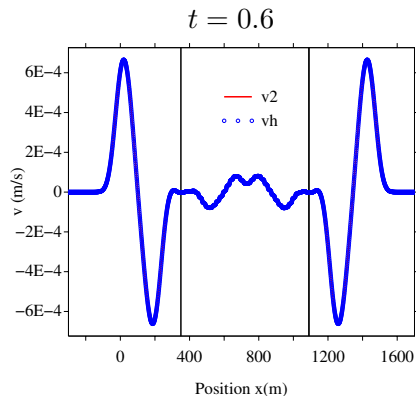
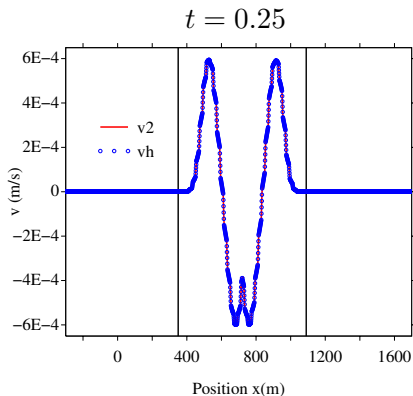
- ▶ **First-order** corrector on  $V$  involving  $\partial_t g$  and the local values  $\rho_s$  and  $P_1(x_s/\ell)$ .
- ▶ Already given by [Capdeville et al., 2010] with another argument.

- Equivalent system with Dirac notation:

$$\begin{cases} \partial_t V - \frac{a}{\varrho_0} \partial_x S &= -\frac{a-1}{\varrho_0} r + \frac{a}{\varrho_0} \rho_s g \delta_s, \\ \partial_t S - \mathcal{E}_0 \partial_x V &= -\ell \rho_s P_1(x_s/\ell) \partial_t g \delta_s, \\ \partial_t \varphi - \frac{a-1}{\varrho_0} \partial_x S &= -\frac{a-1}{\varrho_0} r + \frac{a-1}{\varrho_0} \rho_s g \delta_s, \\ \partial_t r &= \frac{\mathcal{E}_0}{\ell^2 \beta} \varphi. \end{cases}$$

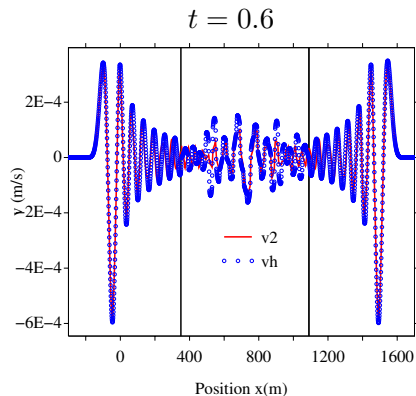
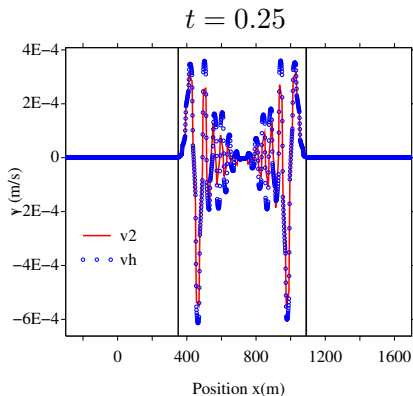
# Velocity fields in a slab with a source point

$$f_c = 3 \text{ Hz}, \varepsilon = 0.04$$



# Velocity fields in a slab with a source point

$$f_c = 12 \text{ Hz}, \varepsilon = 0.29$$



## Key ideas

- The second-order asymptotic homogenization accounts for dispersive effects.
- Boundary and transmission conditions can be designed to complement the inner expansion.  
(including in 2-3D [Vinoles, 2016, Maurel and Marigo, 2018, Cakoni et al., 2019, Beneteau, 2021] ...)
- For transient waves, **stability** can be addressed using (i) hyperbolic formalism and (ii) enlarged interfaces (in 1D for now).
- Source points can be addressed using the same tools (specific to 1D).

## Perspectives

- Pursue the transient case up to *full second-order model*  
(as done in the stationary case [Cornaggia and Guzina, 2020])
  - Apply the built framework to other 1D configurations:
    - ▶ High-frequency homogenization [Craster et al., 2010, Guzina et al., 2019]
    - ▶ Solids with inner imperfect interfaces
    - ▶ Non-linearities
- ⇒ See Cédric Bellis' talk before lunch.
- Hyperbolic formalism for higher dimensions and other models ? (2D acoustics, elasticity ...)

Thanks for your attention !

*Second-order homogenization of boundary and transmission conditions  
for one-dimensional waves in periodic media*

Rémi Cornaggia, Bojan B. Guzina

International Journal of Solids and Structures, 2020

*An homogenized model accounting for dispersion, interfaces and source points  
for transient waves in 1D periodic media*

Rémi Cornaggia, Bruno Lombard

submitted, preprint available on HAL: <https://hal.archives-ouvertes.fr/hal-03652455>

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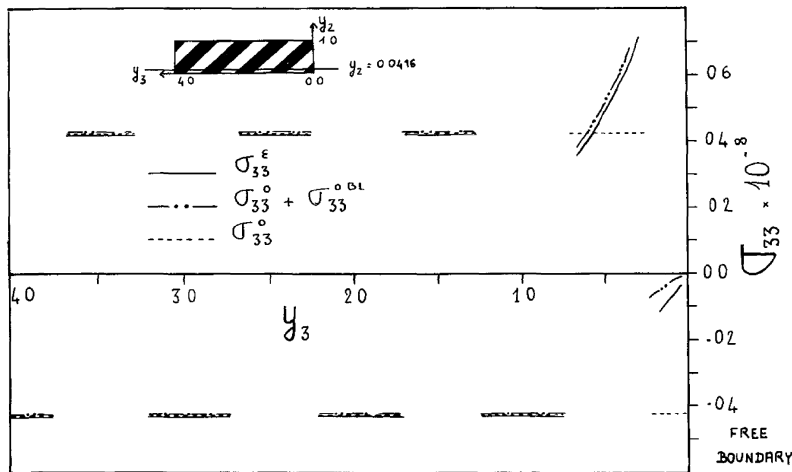


Figure 4. — The  $(3, 3)$  components of the real stresses  $\sigma^E$ , of the micro-stresses  $\sigma^0$  and of the boundary layer stresses  $\sigma^{OBL}$  added to  $\sigma^0$ , plotted against  $y_3$ , at  $y_2 = 0.0416$  fixed.

... to time-harmonic dynamics [Beneteau, 2021] with S. Fliss, X. Claeys

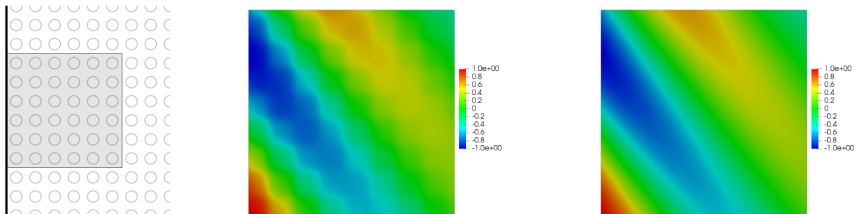


FIGURE 2.4 –  $u_\varepsilon$  pour  $\varepsilon = 1/8$  (à gauche) et  $u_0$  (à droite) dans  $\Omega = (0, 1)^2$

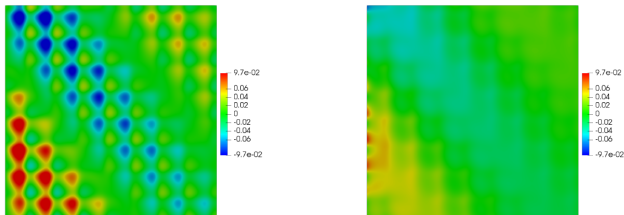
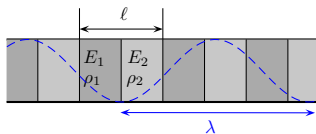


FIGURE 2.7 –  $u_\varepsilon - u_0$  (à gauche) et  $u_\varepsilon - (u_0 + \varepsilon u_1^{osc})$  (à droite) dans  $\Omega = (0, 1)^2$  pour  $\varepsilon = 1/8$

# Choosing a $(mt)$ model from dispersion relations in layered media



- Bloch wave  $u_\ell(X, t) = \tilde{u}(x)e^{i(\kappa x - \omega t)} \implies$  dispersion relation  $\omega = f(\kappa)$ .  
About  $(\omega, \kappa) = (0, 0)$  (on the acoustic branch):

$$\frac{\omega}{c_0} = \kappa \left[ 1 - \frac{\beta}{2}(\kappa\ell)^2 + \frac{\beta(2 - 27\beta - 8\bar{\beta})}{40}(\kappa\ell)^4 + O(\ell^6) \right],$$

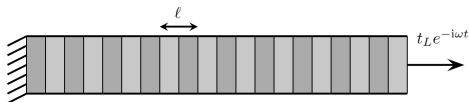
( $\bar{\beta}$  known for layered media)

- Plane wave  $U(x, t) = \tilde{U}e^{i(\kappa x - \omega t)}$  in the second-order  $(mt)$  homogenized model:

$$\frac{\omega}{c_0} = \kappa \left[ 1 + \frac{\beta_m + \beta_t}{2}(\kappa\ell)^2 + \frac{(\beta_m + \beta_t)(3\beta_m + 7\beta_t)}{8}(\kappa\ell)^4 + O(\ell^6) \right].$$

- Second-order approximation of  $\omega/c_0$  obtained for any  $(\beta_m, \beta_t)$  satisfying  $-\beta_m - \beta_t = \beta$ .  
Also true in 2-3D [Allaire et al., 2016].
- Fourth-order approximation for  $\beta_m = \frac{-1 - 4\beta + 4\bar{\beta}}{10}$  and  $\beta_t = \frac{1 - 6\beta - 4\bar{\beta}}{10}$   
Similar approximation for spring-mass lattice in [Pichugin et al., 2008]

# Model problem and leading-order approximation



- Time-harmonic model problem:

$$\begin{cases} [E(x/\ell)u_{,x}]_{,x} + \rho(x/\ell)\omega^2 u = 0 & x \in Y_L := ]0, L[ \\ u = 0 & x = 0 \\ \sigma = E(x)u_{,x} = \sigma_L & x = L \end{cases}$$

- Leading-order homogenization:  $(u, \sigma) \rightarrow (U, \mathcal{E}_0 U_{,x})$

$$\begin{cases} U_{,xx} + k_0^2 U = 0 & x \in Y_L, & k_0 := \omega/c_0 \\ U = 0 & x = 0 \\ U_{,x} = \sigma_L/\mathcal{E}_0 & x = L \end{cases}$$

## Using full-field approximations [Cornaggia and Guzina, 2020]

First-order approximations of displacement and stress  $(u, \sigma)$ :

$$\begin{cases} \tilde{u}^{(1)}(x) = U(x) + \ell P_1 \left( \frac{x}{\ell} \right) U_{,x}(x) \\ \tilde{\sigma}^{(1)}(x) = \mathcal{E}_0 \left[ U_{,x}(x) + \ell \Sigma_1 \left( \frac{x}{\ell} \right) U_{,xx}(x) \right] \end{cases}$$

Using cell stress functions:  $\Sigma_j := (E/\mathcal{E}_0) [P_j + P_{j+1,y}]$

Boundary-value problem for the mean field  $U$ :

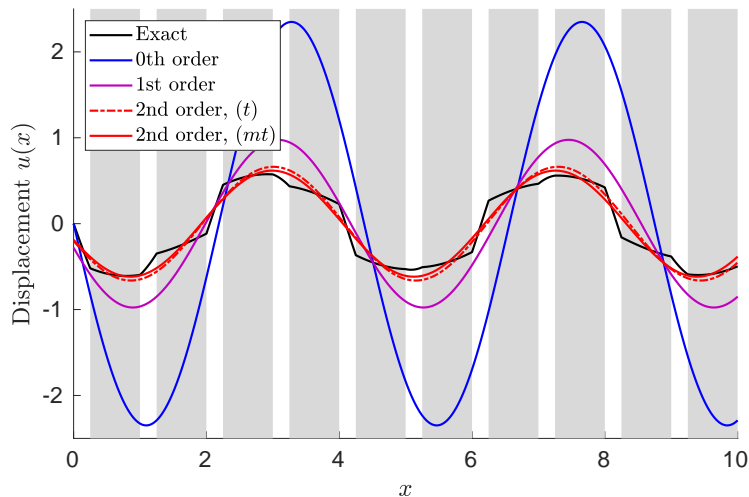
$$\begin{cases} U_{,xx} + k_0^2 U = 0 & x \in Y_L \\ \tilde{u}^{(1)} = 0 & x = 0 \\ \tilde{\sigma}^{(1)} = \sigma_L & x = L \end{cases}$$

$$\begin{cases} U_{,xx} + k_0^2 U = 0 & x \in Y_L \\ U + \ell P_1(0) U_{,x} = 0 & x = 0 \\ U_{,x} + \ell \Sigma_1(0) U_{,xx} = \sigma_L / \mathcal{E}_0 & x = L \end{cases}$$

$$\begin{cases} U_{,xx} + k_0^2 U = 0 & x \in Y_L \\ U + \ell P_1(0) U_{,x} = 0 & x = 0 \\ U_{,x} - \ell \Sigma_1(0) k_0^2 U = \sigma_L / \mathcal{E}_0 & x = L \end{cases}$$

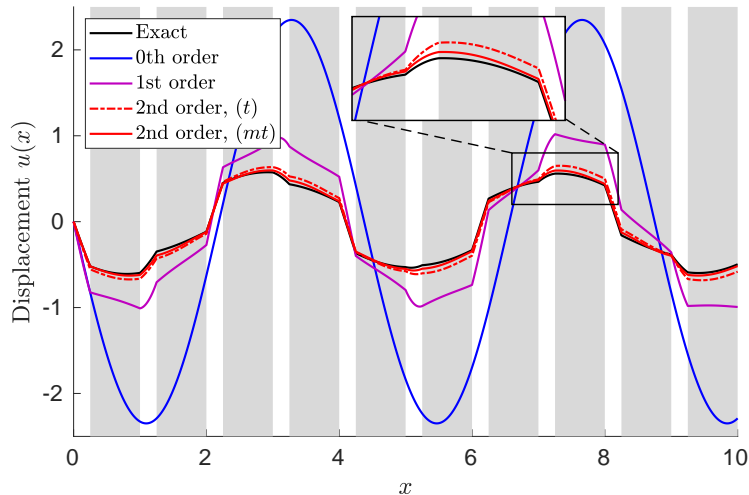
## Example for a layered material - mean fields $U$

$$\varepsilon = \ell/\lambda_0 \approx 0.3$$



## Example for a layered material - total displacement $u$

$$\varepsilon = \ell/\lambda_0 \approx 0.3$$



## Example for a layered material - axial stress $\sigma$

$$\varepsilon = \ell/\lambda_0 \approx 0.3$$

