

Fiber-Bundle models in fracture

A tentative overview



Daniel Bonamy

*Service de Physique de l'Etat condensé -- SPEC
CEA Saclay -- Orme des Merisiers*



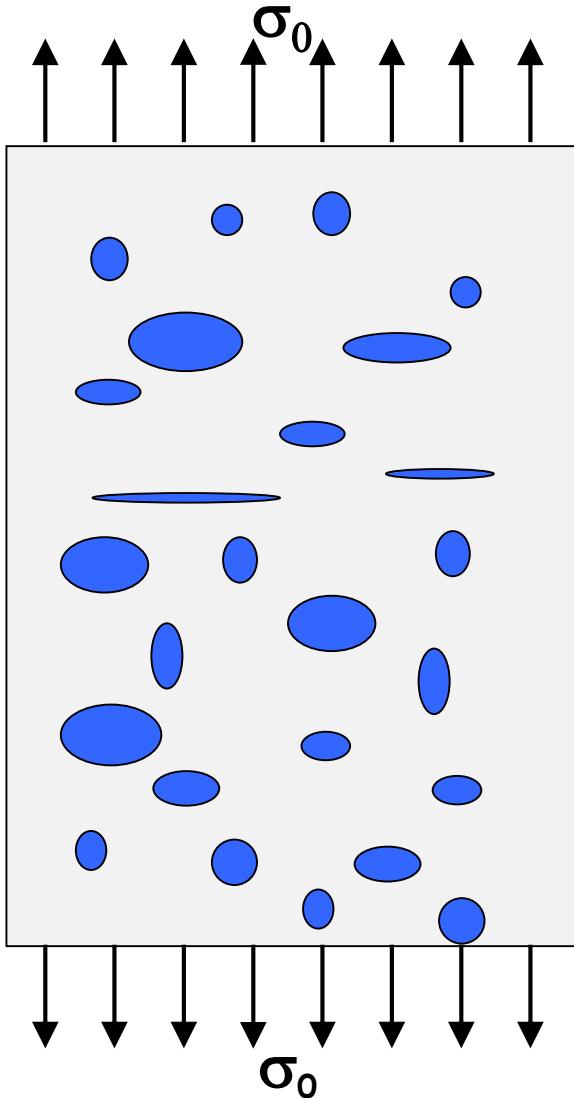
Alex Hansen, Per C. Hemmer, Srutarshi Pradhan

**The Fiber Bundle
Model**

Modeling Failure in Materials



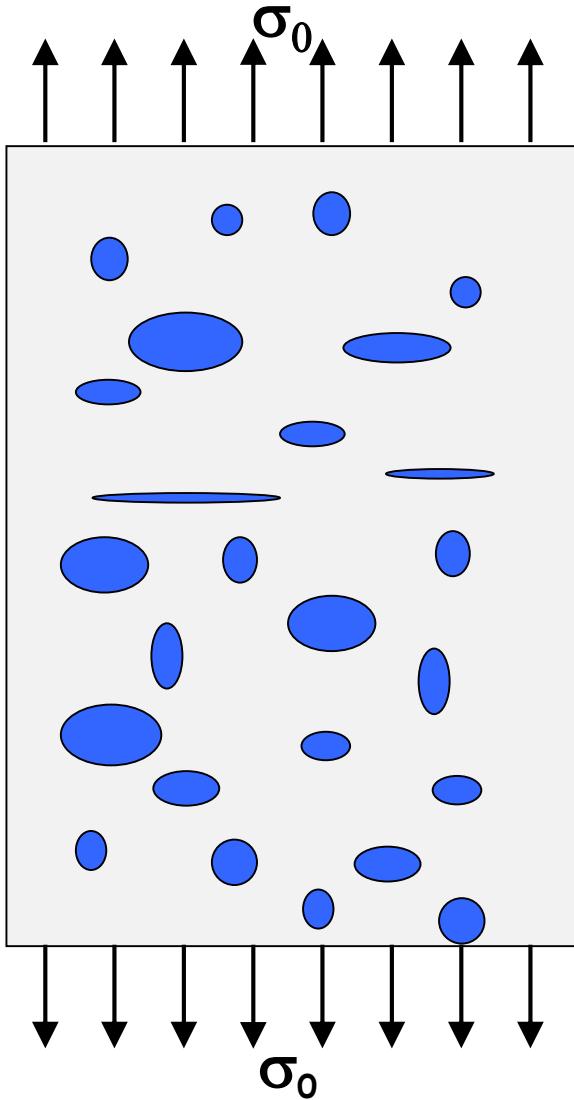
Complexity in fracture



Elastic response, elastic properties

$$E_{global} \simeq mean(E_{local})$$

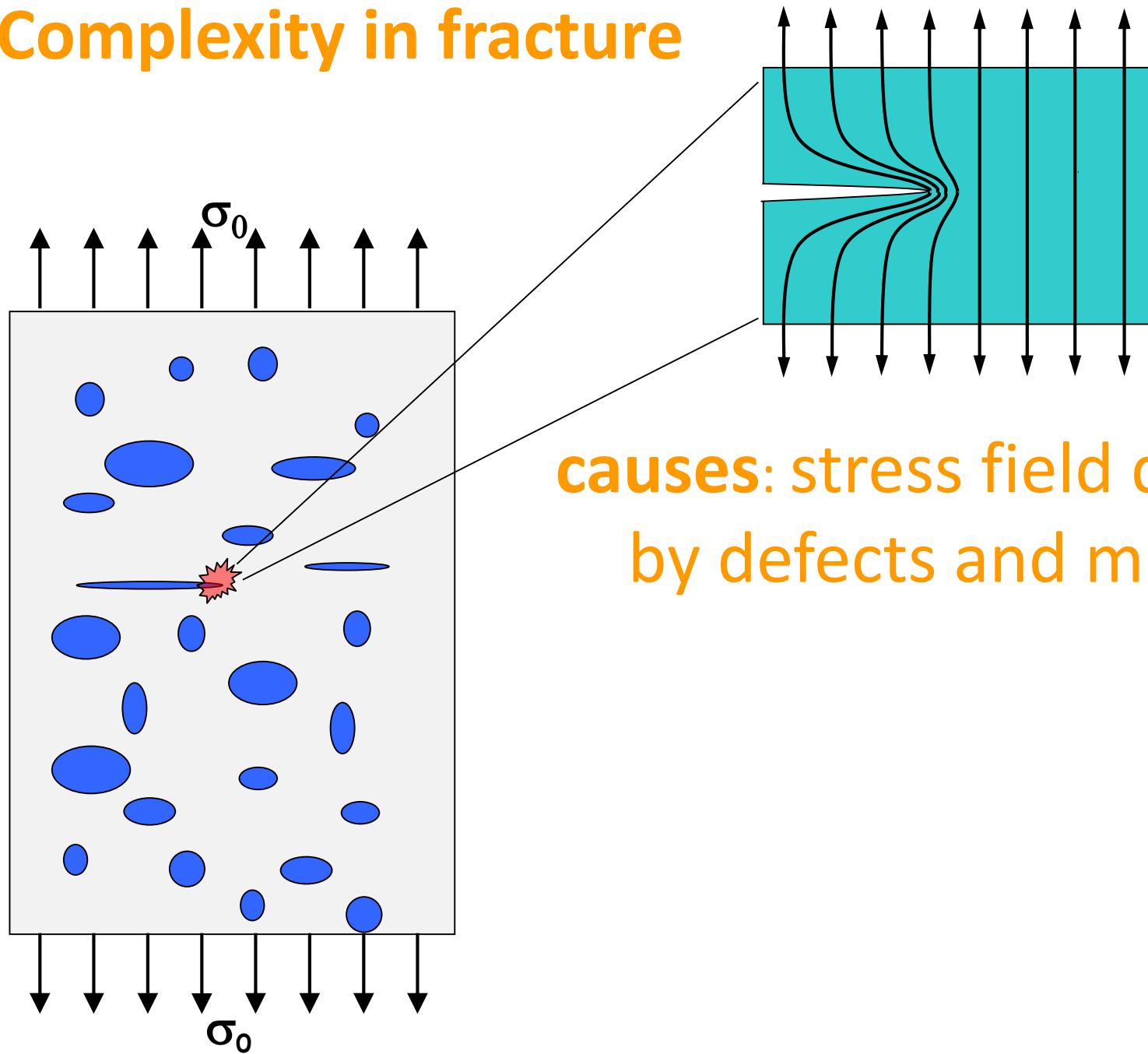
Complexity in fracture



Failure, strength in materials

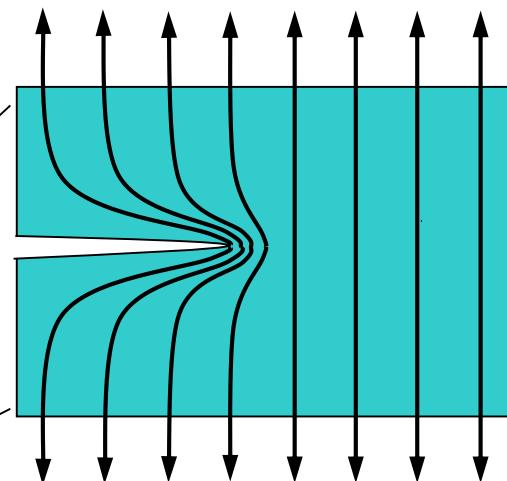
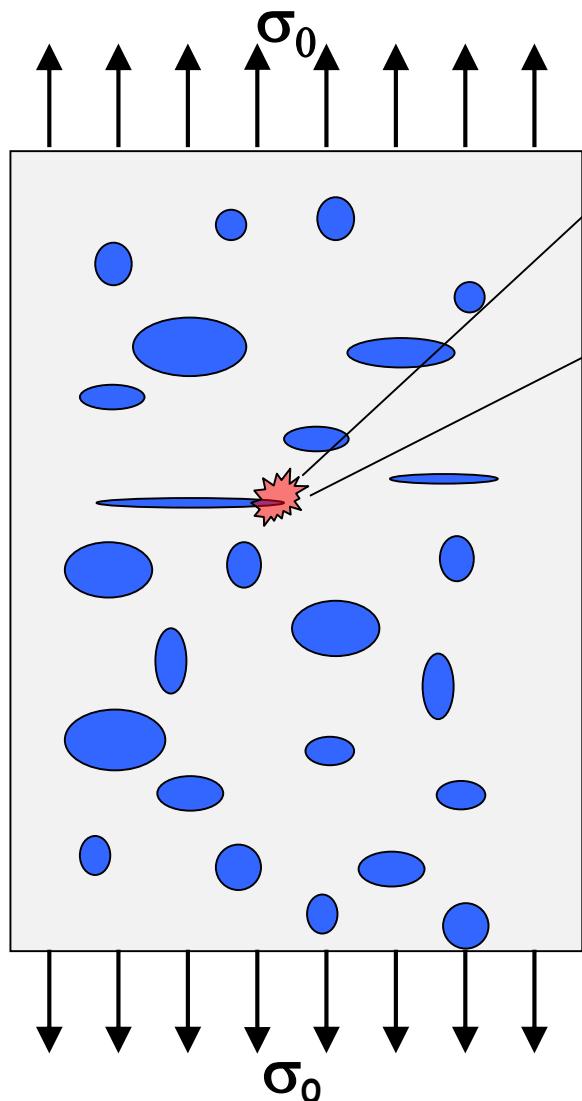
$$\sigma_{global}^f \neq \text{mean}(\sigma_{local}^f)$$

Complexity in fracture



causes: stress field distortion
by defects and microcracks

Complexity in fracture

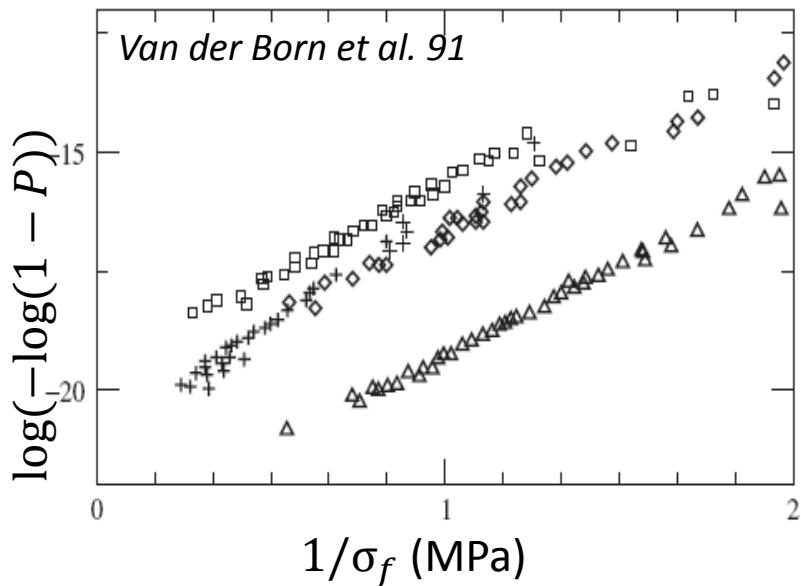


**causes: stress field distortion
by defects and microcracks**

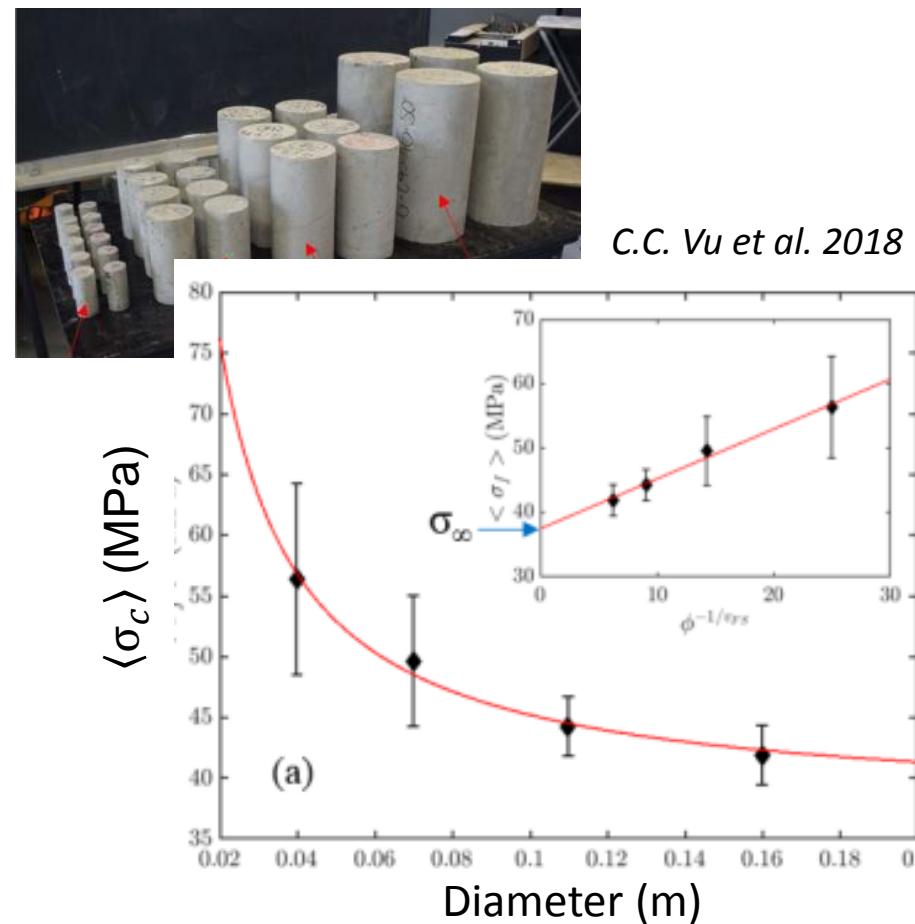
- ➔ Driven by rare & extreme defects, macroscale sensitivity to microscale inhomogeneities,
 - ➔ Non-trivial statistics & size effects for strength
 - ➔ Unpredictability at the macroscale
- ➔ Not really compatible with continuum engineering mechanics**

Complexity in fracture : illustrations (1/2)

Extreme event statistics on strength
[Here Duxbury-Leath law on
ceramics components]

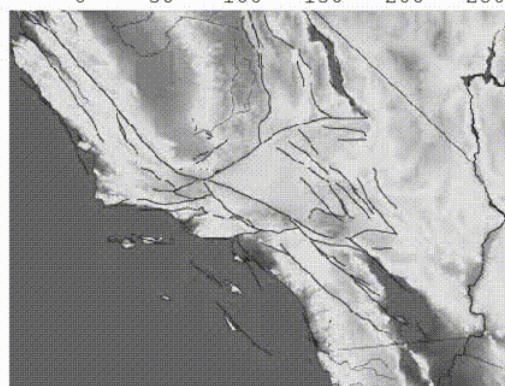
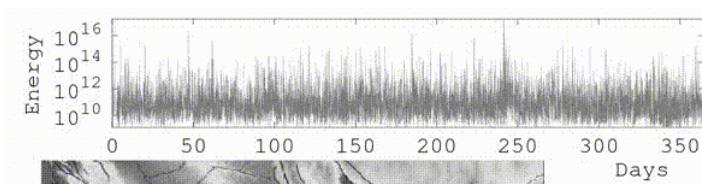
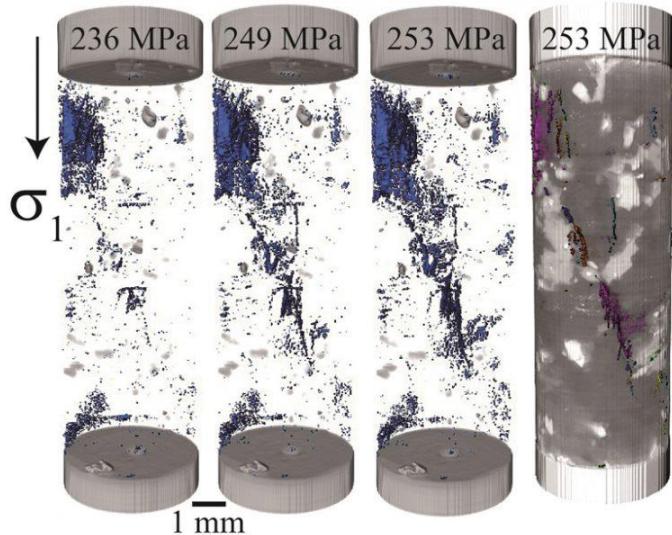


Non-trivial size dependency on
strength [Here on concrete]



Complexity in fracture : illustrations (2/2)

X-ray tomography imaging
of damage in rocks *Renard et al. 2018*



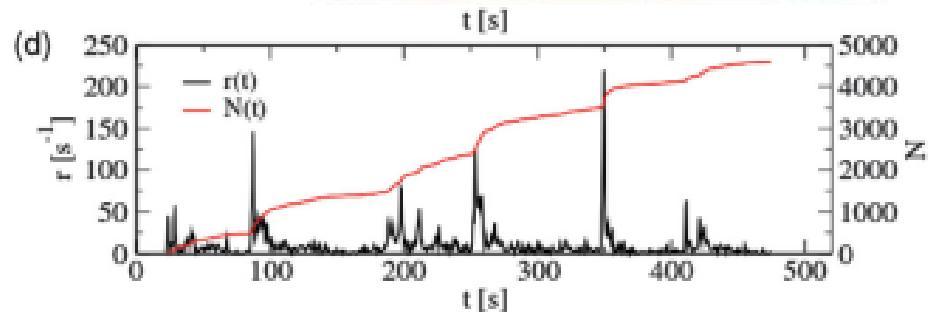
Sismicity in
California, 2012

Bares. 2013

Acoustic emission in compressed wood



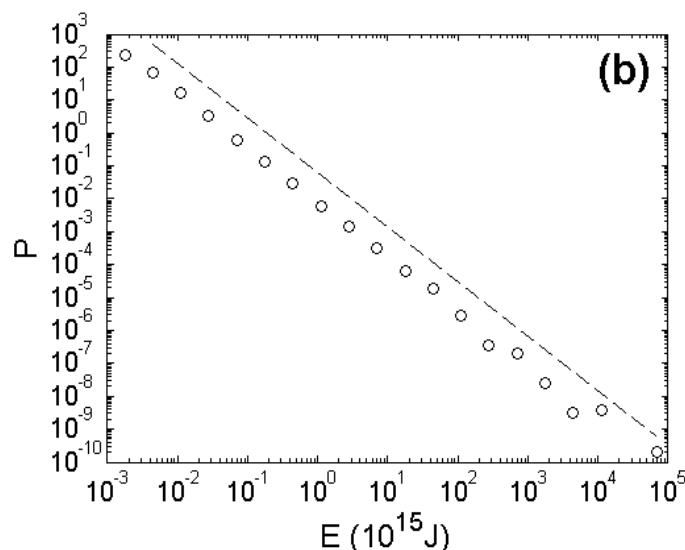
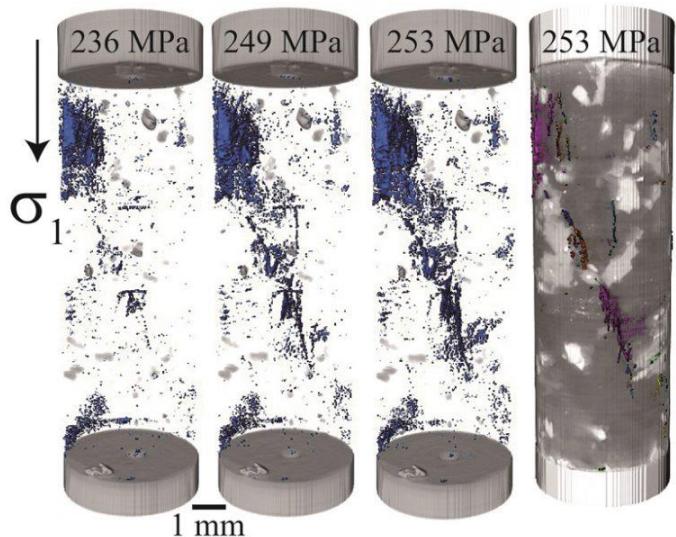
Makinen et al. 2015



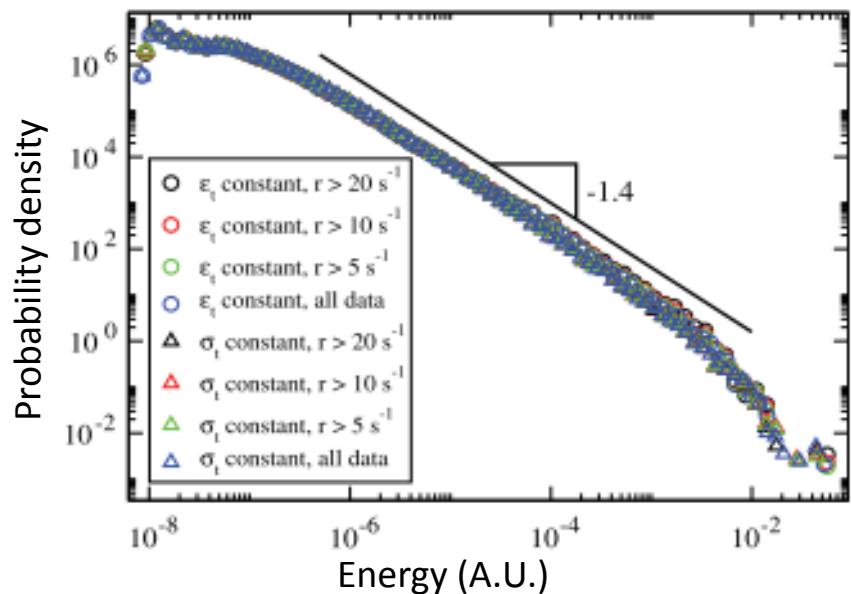
Highly intermittent dynamics
Damage localization in space

Complexity in fracture : illustrations (2/2)

X-ray tomography imaging
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Acoustic emission in compressed wood



Highly intermittent dynamics
Damage localization in space
Scale-free avalanches of damage
Power-law distributed size/energy

Fiber Bundle Models (FBM): the approach

Material simplified to:

N parallel brittle fibers

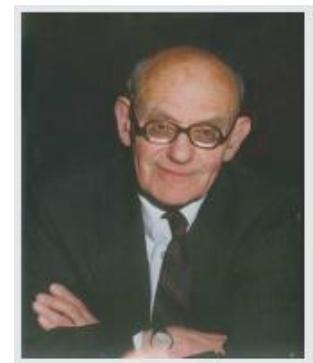
Same stiffness $\kappa = 1$

Random failure threshold

Prescribed rules for load redistribution



F.T. Pierce, 1926



H.E. Daniels, 1945

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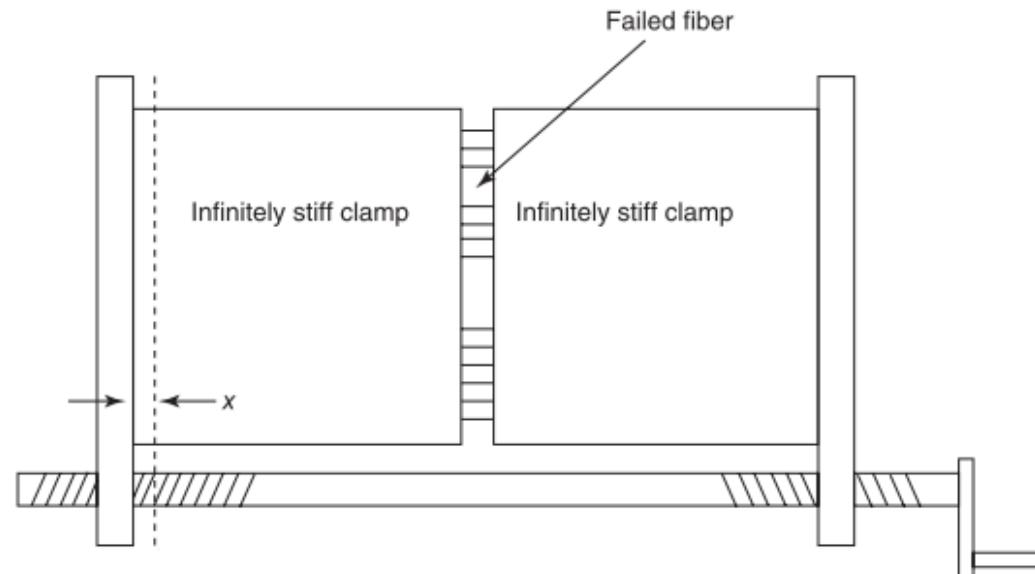
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Prescribed rules for load redistribution

Equal load Sharing (ELS)

all intact fibers share same fraction



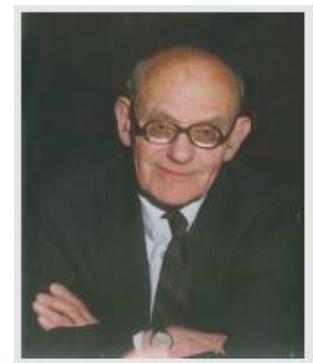
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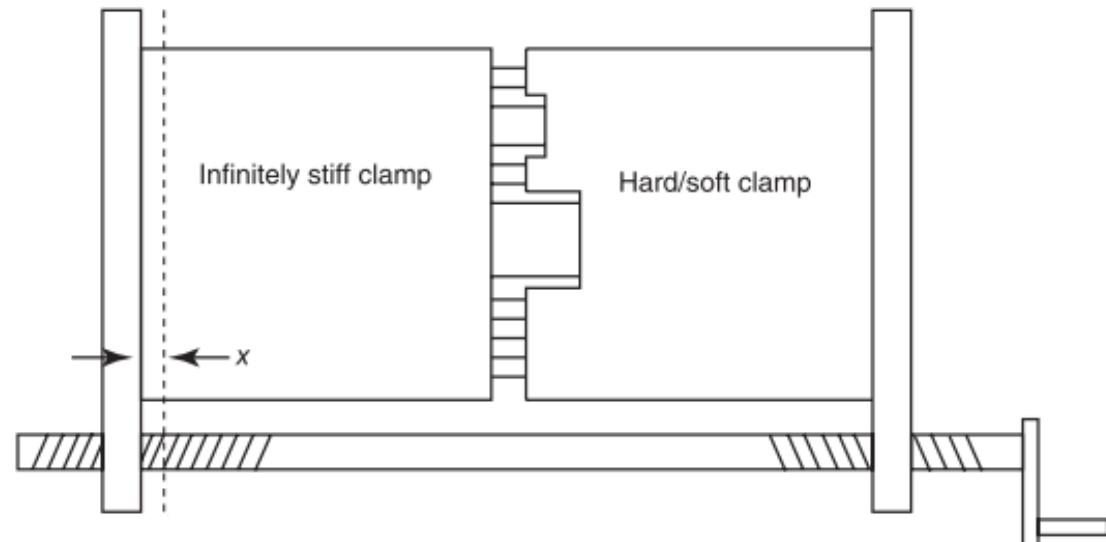
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Local load Sharing (LLS)

Load of failed fiber redistributed
to intact nearest-neighbors only



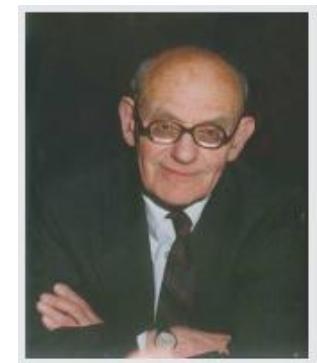
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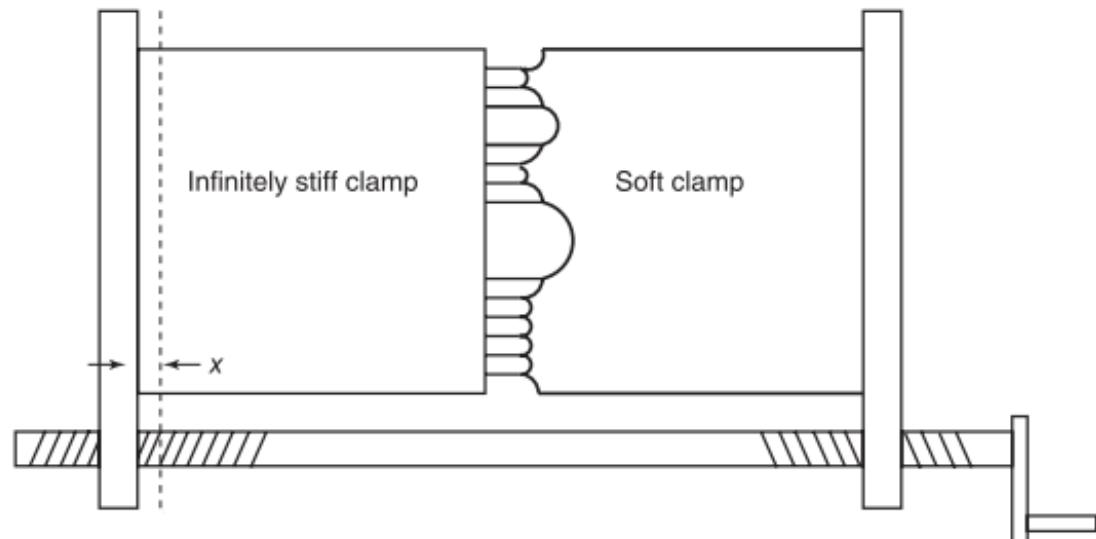
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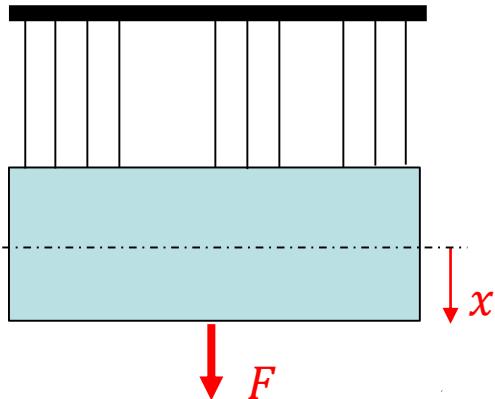
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Intermediate load Sharing (ILS)

Load transfer decreases with distance from failed fiber

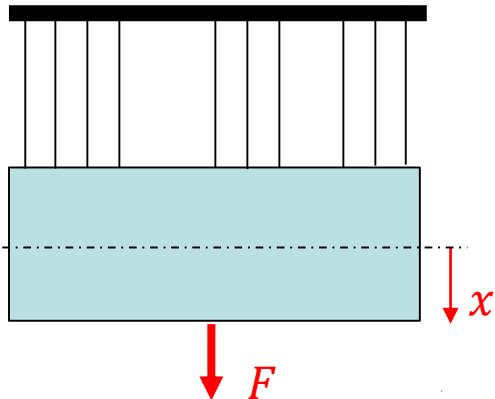
ELS -- FBM: continuum (average) behavior



- $N \rightarrow \infty$ parallel brittle fibers
- Overall stretching force F , => stress $\sigma = F/N$
- Same stiffness $\kappa = 1$
- Same fiber extension : x
- Random critical loads x_i with distribution $p(x)$
[cumulative $P(x)$]

Fully tractable analytically

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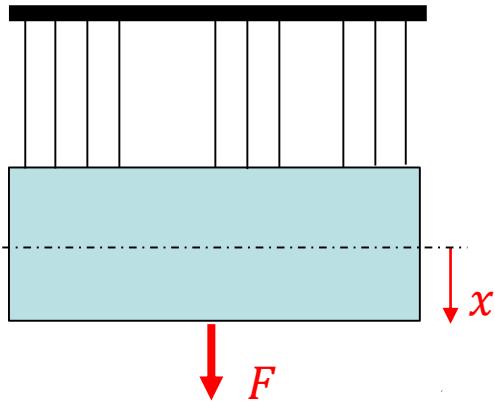
Fully tractable analytically

Displacement-driven “experiment”, at displacement x :

Number of intact fibers: $n(x) = N(1 - P(x))$

→ Density: $\rho = n/N : \rho(x) = 1 - P(x)$

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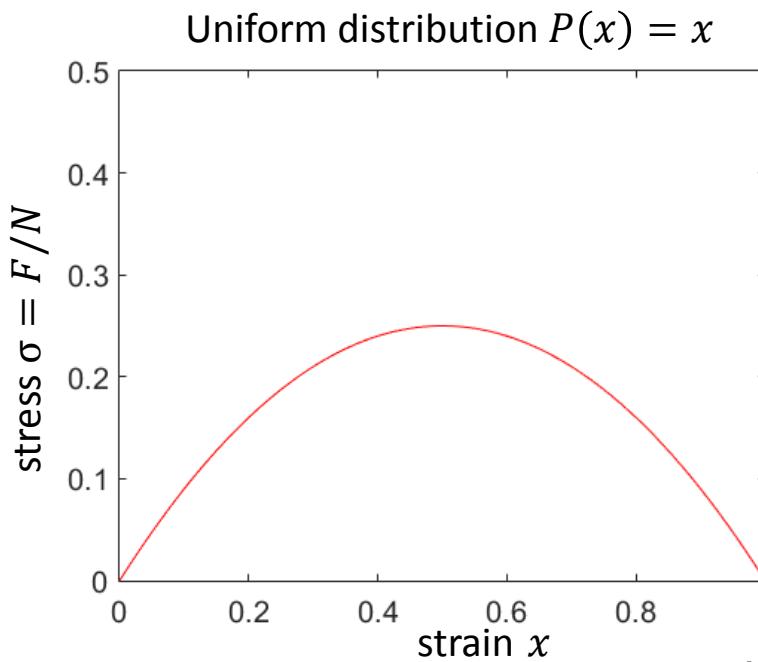
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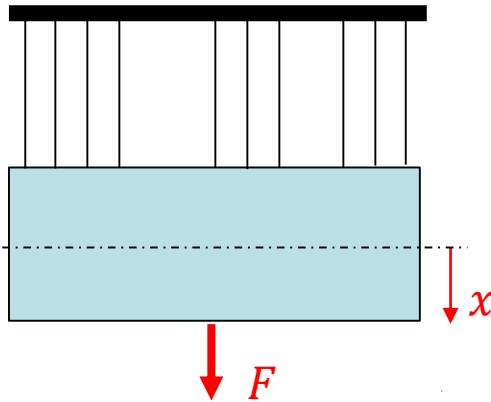
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Stretching force $F(x) = xn(x)$

→ Applied stress $\sigma(x) = x(1 - P(x))$



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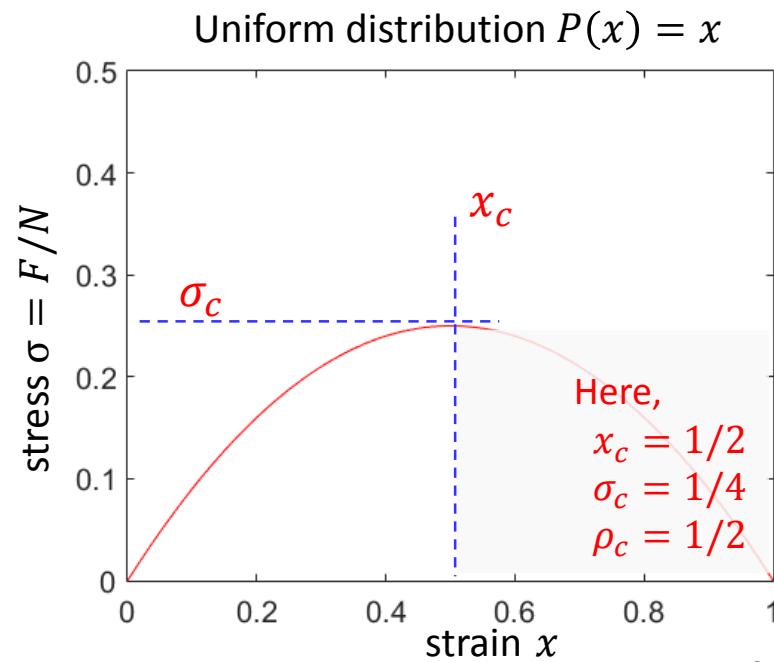
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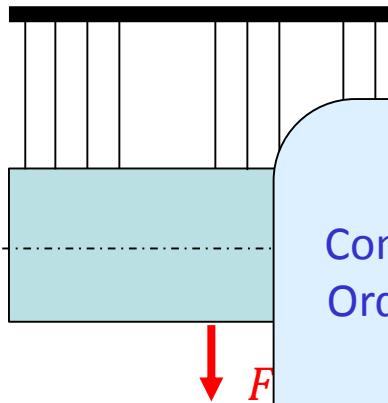
Failure at the maximum point:

→ Strength $\sigma_c = \sigma(x_c)$, so that $\sigma'(x_c) = 0$

→ Critical damage: $\rho_c = \rho(x_c)$



ELS -- FBM: continuum (average) behavior



Critical behavior at failure

Control parameter : σ

Order parameter : $\rho - \rho_c$

$$\rho - \rho_c \sim (\sigma_c - \sigma)^{1/2}$$

$$\frac{d\rho}{d\sigma} \sim (\sigma_c - \sigma)^{-1/2}$$

Universal,
independent of $P(x)$

Fully tractable analysis
Displacement-driven

stress $\sigma = F/N$

distribution $p(x)$
cumulative $P(x)$

Uniform distribution $P(x) = x$

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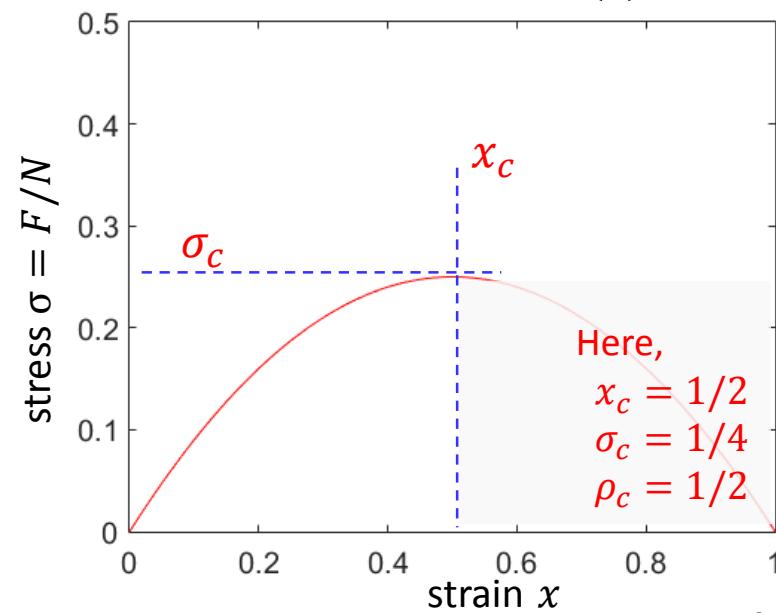
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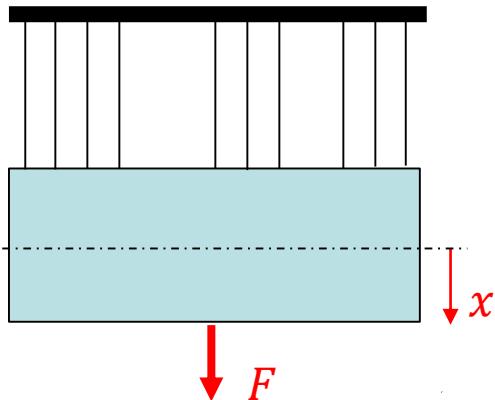
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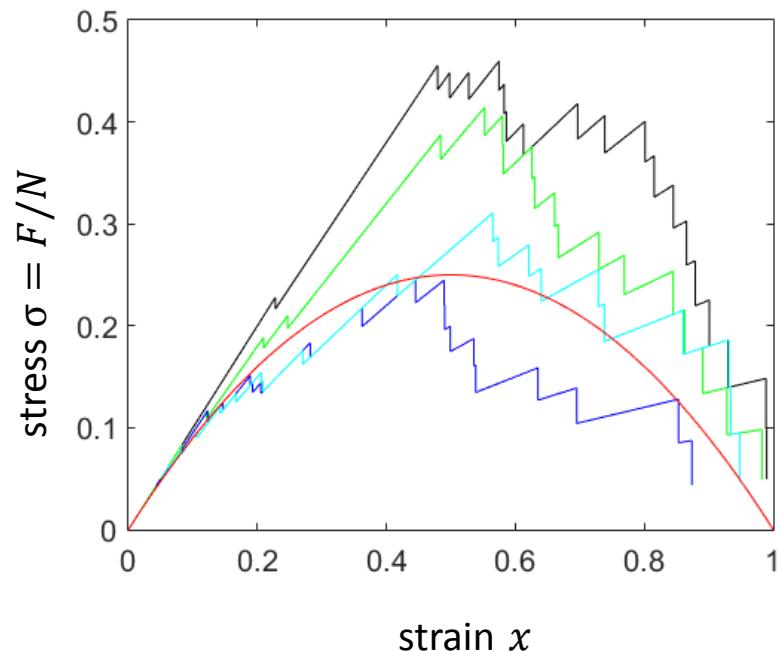


ELS -- FBM: size effect and fluctuations



- Finite N parallel brittle fibers
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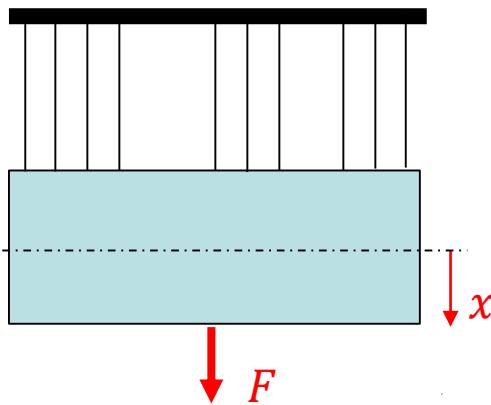
Uniform distribution $P(x) = x, N = 20$



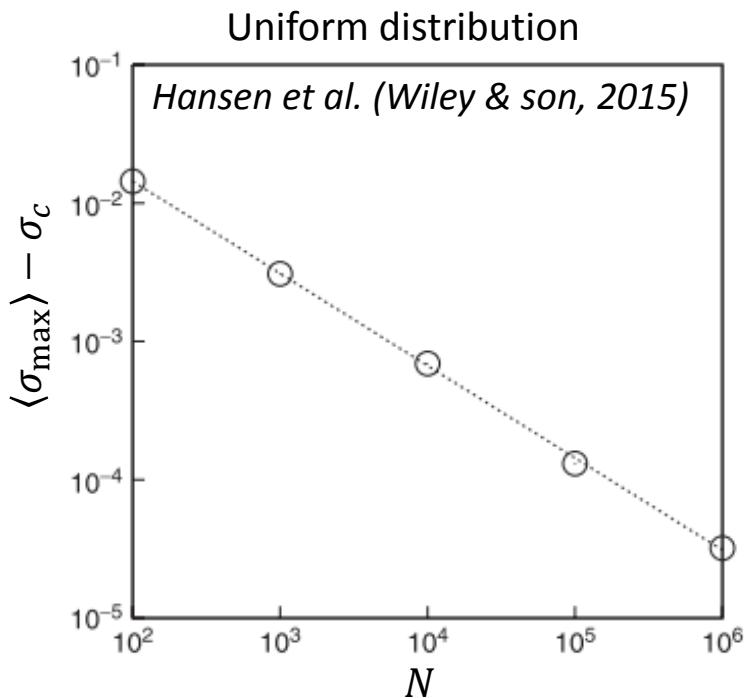
$pdf(\sigma|x, N)$ known analytically (roughly Gaussian)
Daniels, Prc. R. Soc. London A, 1945

- $\langle \sigma_N \rangle(x) = x(1 - P(x))$
- $\langle (\sigma_N - \langle \sigma_N \rangle)^2 \rangle(x) = x^2 P(x)(1 - P(x))/N$

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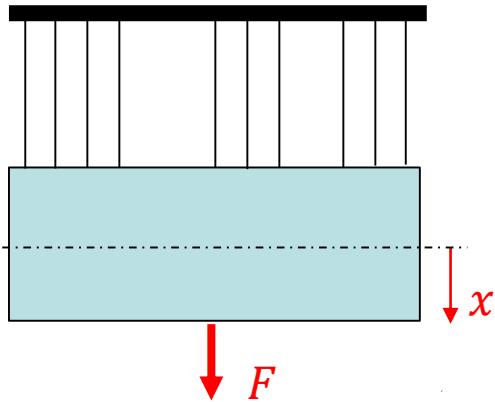
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(Tiny) size effect on strength

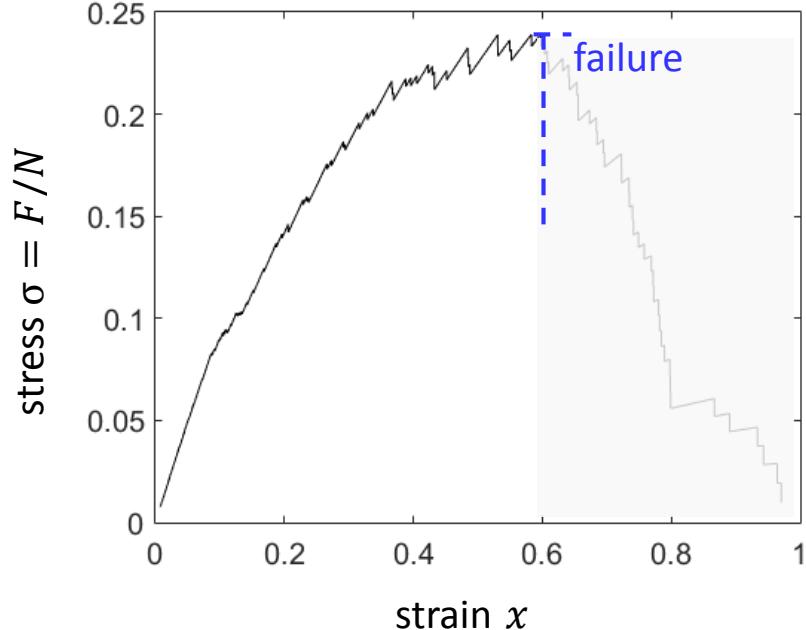
$$\langle \sigma_{\max|N} \rangle = \sigma_c + K/N^{2/3}$$

ELS -- FBM: avalanches precursors



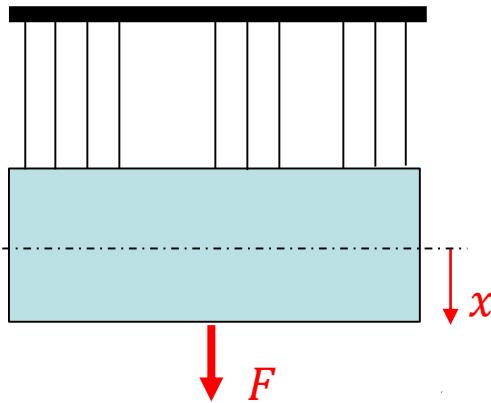
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Uniform distribution $P(x) = x$. $N = 100$



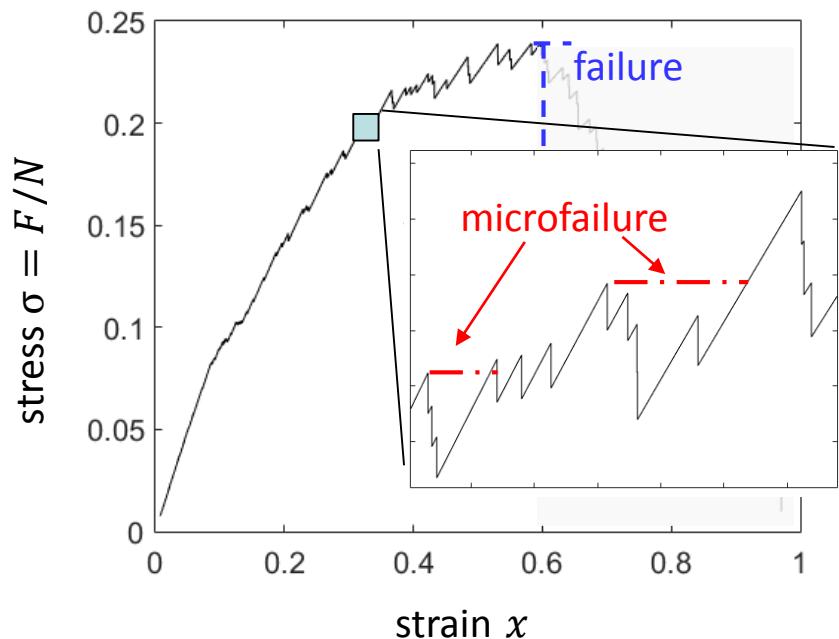
Displacement imposed experiment
→ monotonic $\sigma(x)$

ELS -- FBM: avalanches precursors



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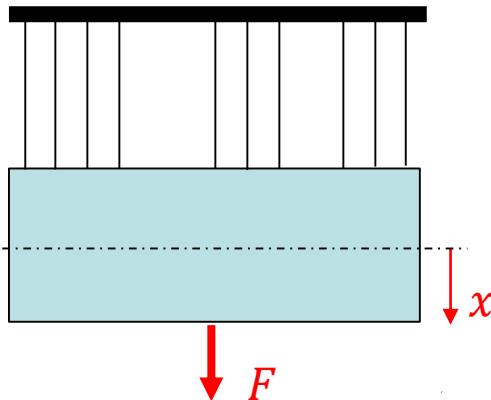
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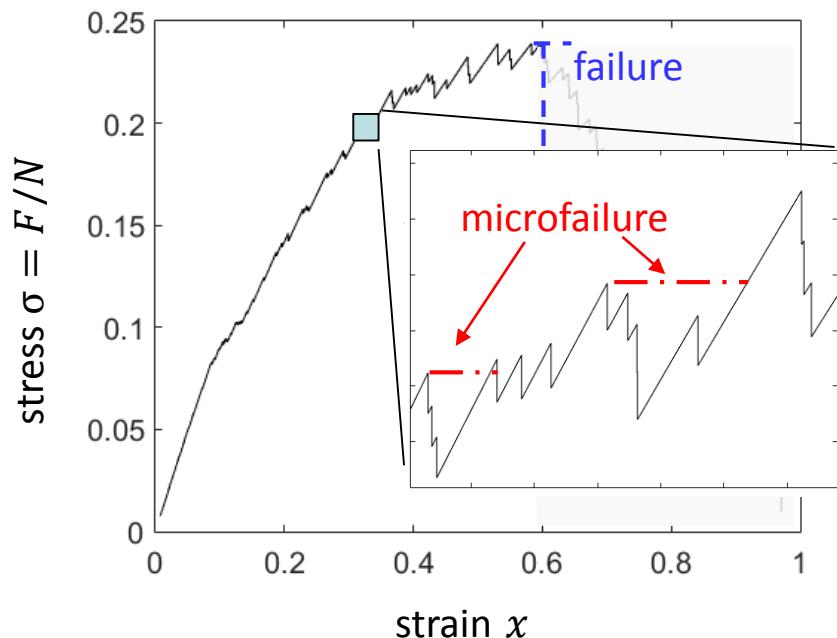
Avalanche size S = number of fibers
involved in microfailure

ELS -- FBM: avalanches precursors



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Size distribution fully computable analytically
Hansen & Hemmer 1992, 1994

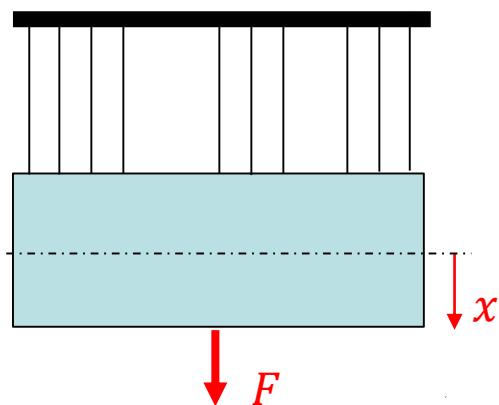
at failure: $P(S|\sigma_c) \sim S^{-3/2}$

before failure: $P(S|\sigma) \sim S^{-3/2} \exp(-S(\sigma - \sigma_c))$

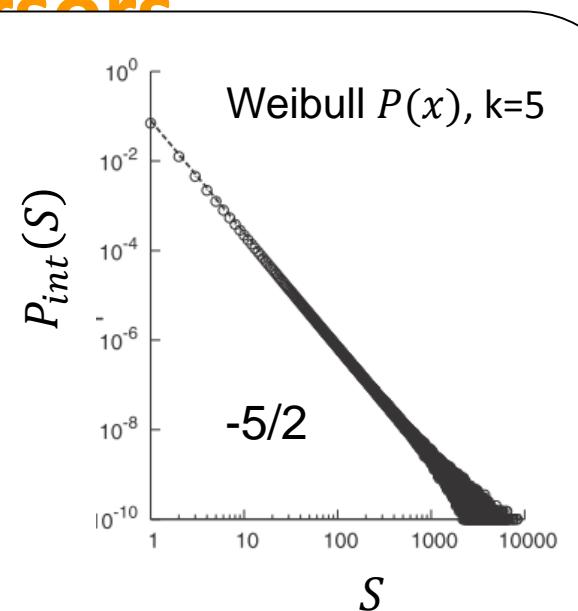
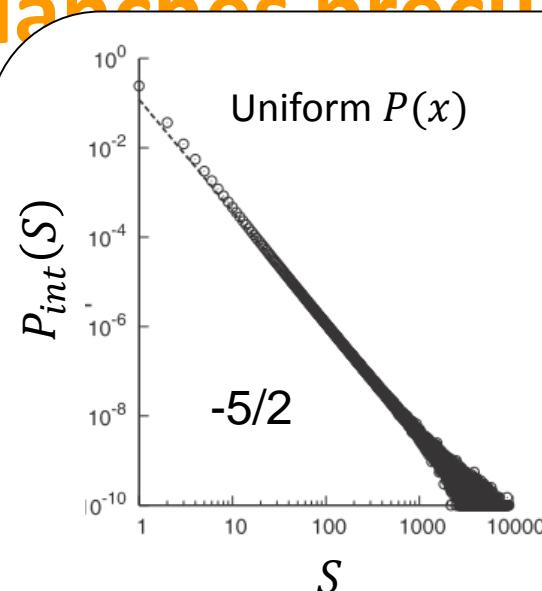
integrated $P_{int}(S) \sim S^{-5/2}$

Interpretable via random walk

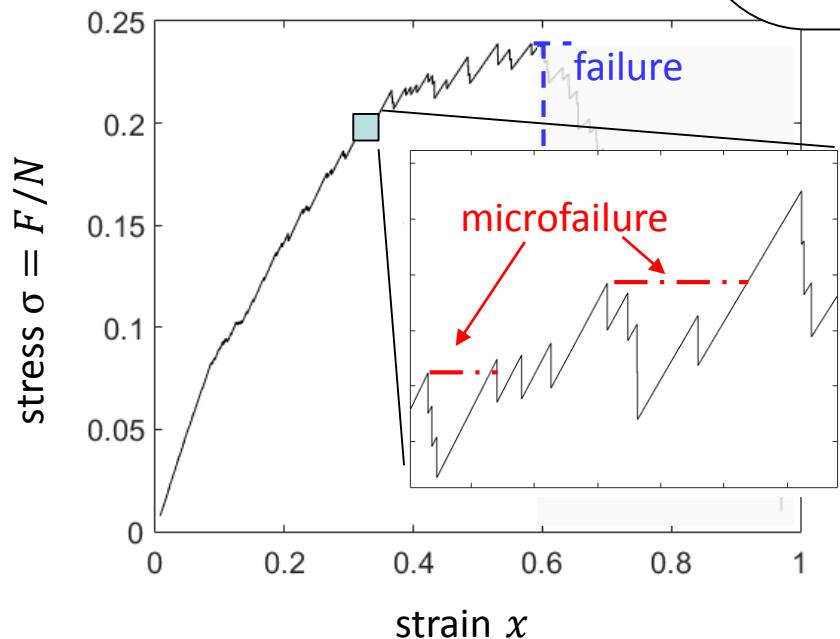
ELS -- FBM: avalanches precursors



Uniform distribution $P(x) = x \cdot N$



20000 sample, $N=10^6$, from Pradhan et al. 2010



Avalanche size S = number of fibers involved in microfailure

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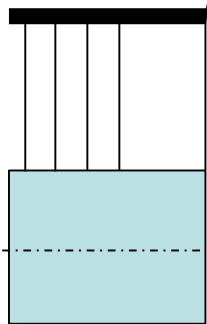
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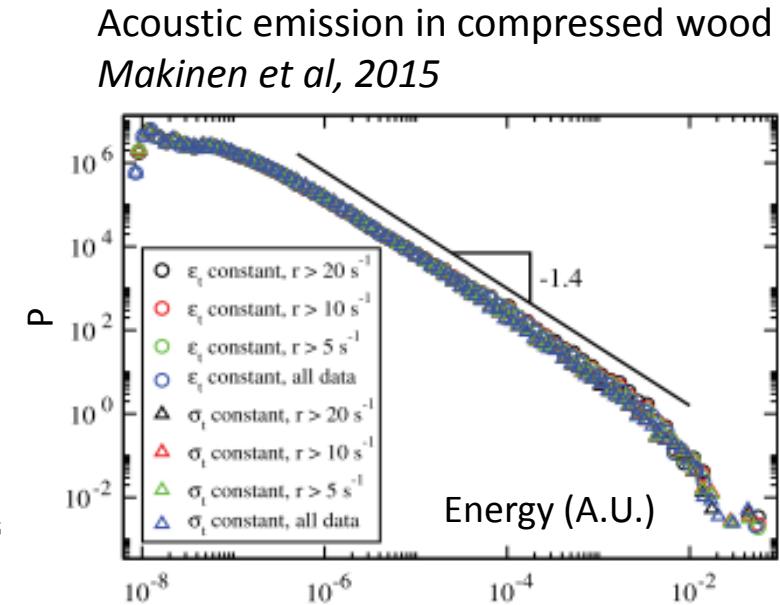
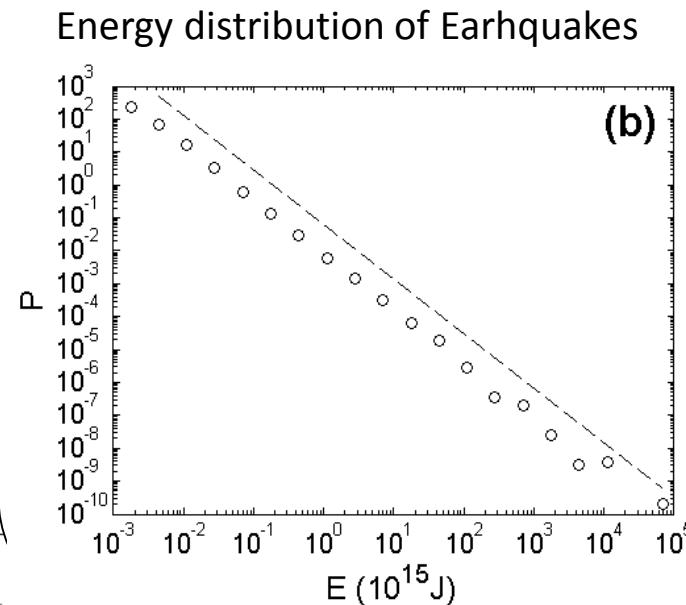
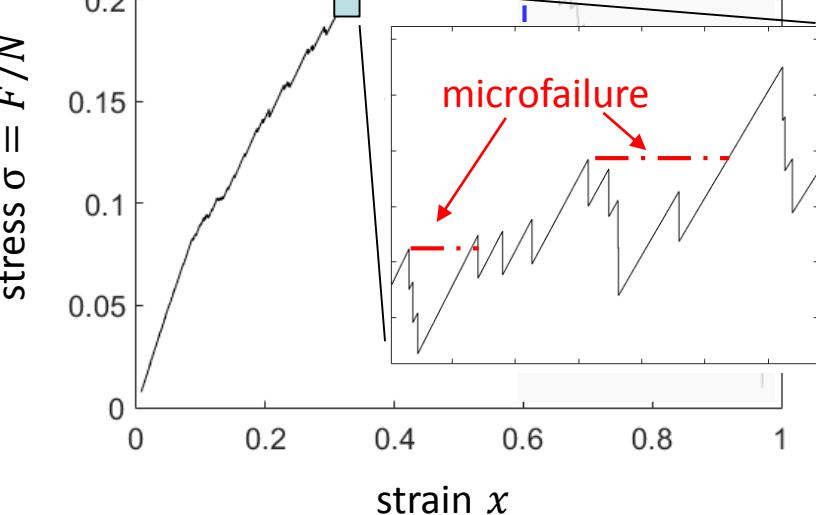
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Interpretable via random walk

Qualitatively compatible with experiments



Uniform distribution



involved in microfailure

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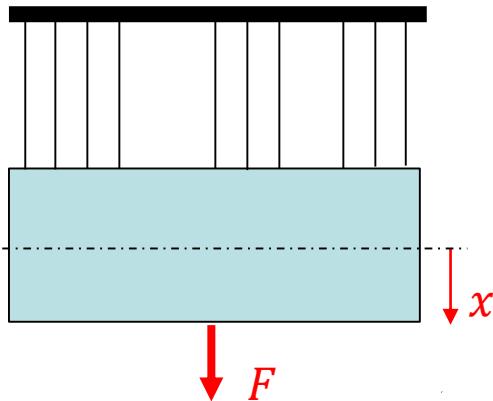
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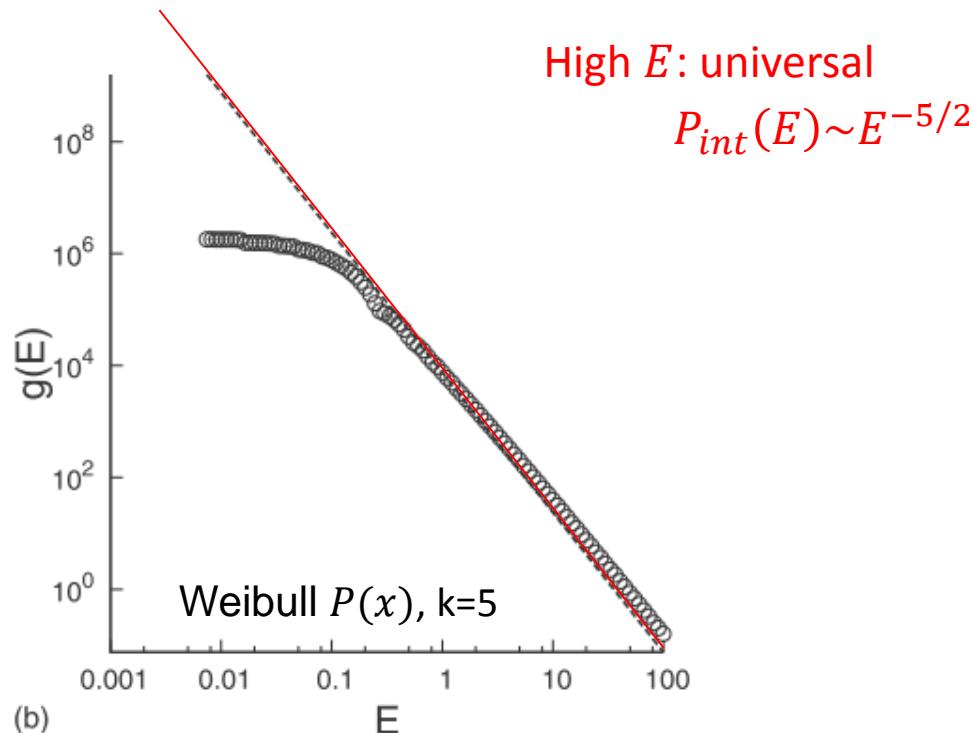
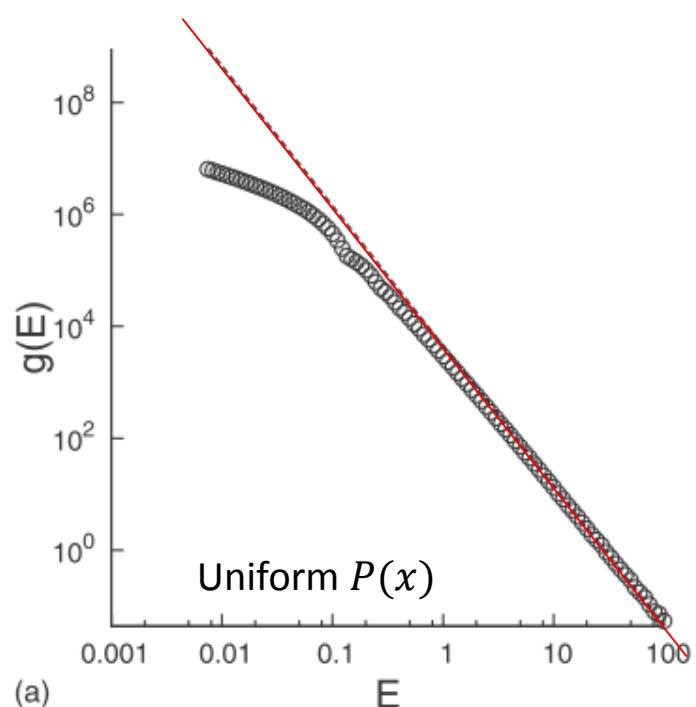
ELS -- FBM: more on avalanches precursors



Experimental observable,
energy release by avalanche

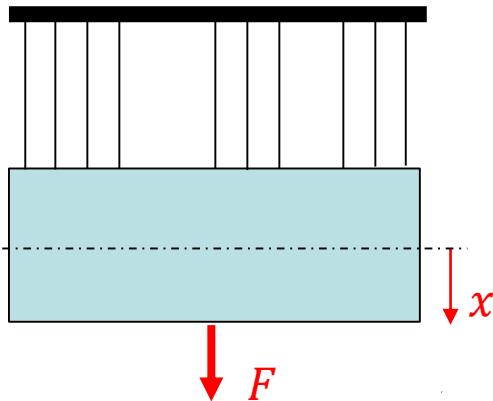
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Energy distribution fully determined analytically
Pradhan et al, Rev. Mod. Phys. 2010



20000 sample, $N=10^6$, from Pradhan et al. 2010

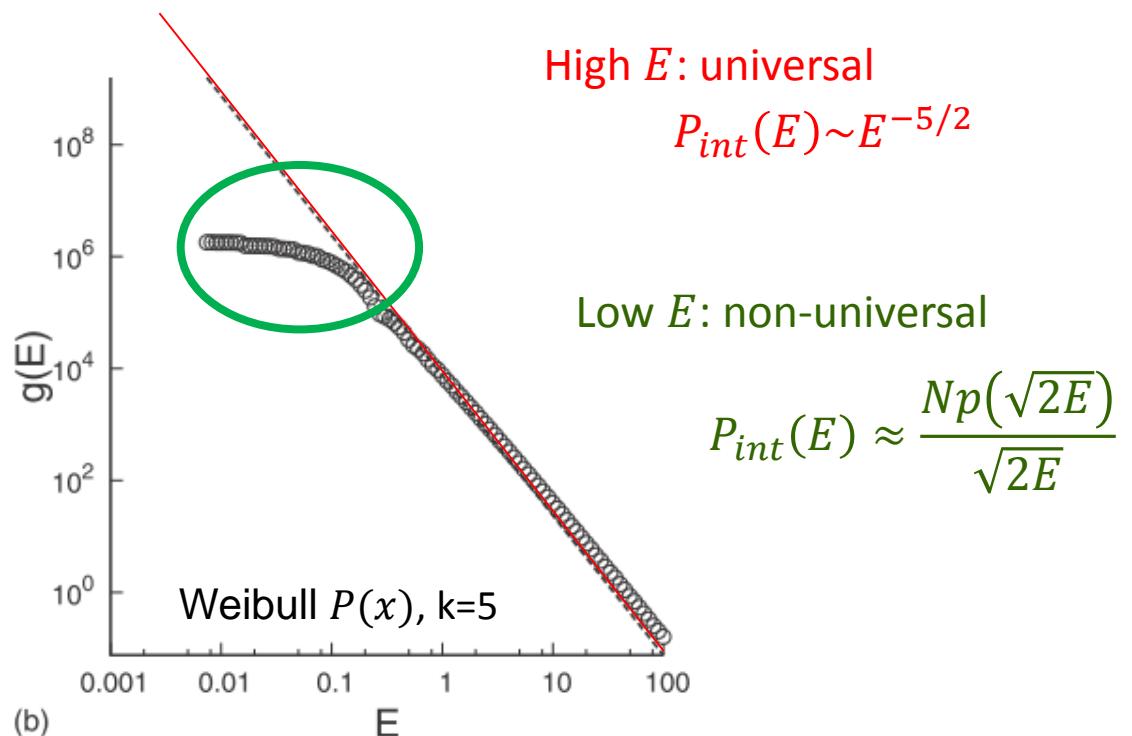
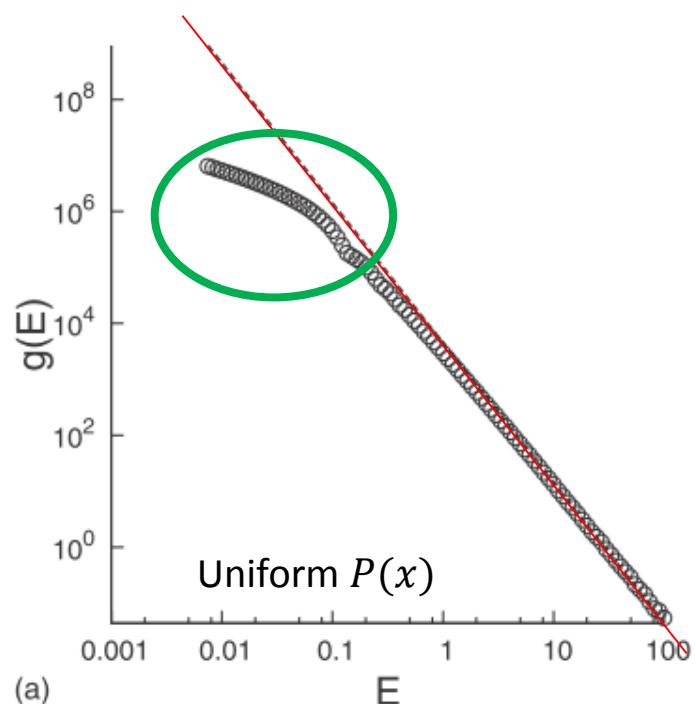
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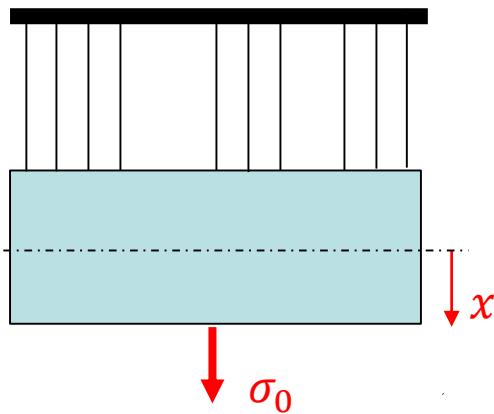
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ELS -- FBM: thermal noise & creep

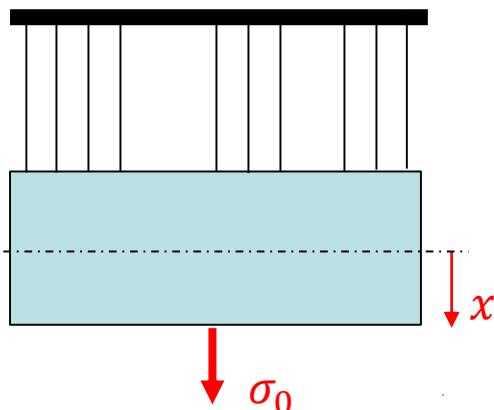
N Mallick, PhD, ENS Lyon, 2010, M. Stojanova, PhD, ENS Lyon, 2015



- N parallel brittle fibers
- Overall constant stress $\sigma_0 = F_0/N < \sigma_c$
- Same stiffness $\kappa = 1$
- Same fiber extension : x
- Random critical loads x_i , pdf Gaussian pdf , variance T_d
- Thermal fluctuations via a new noise term $\eta(t)$, variance T

ELS -- FBM: thermal noise & creep

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→ Analytical determination of failure rate
during creep due the constant stress loading

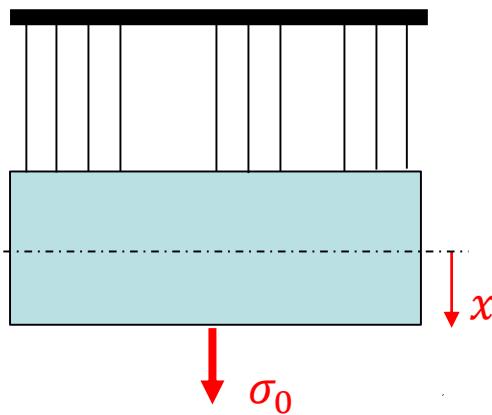
Omori law
$$\frac{dn}{dt} \approx \frac{A\sqrt{T/T_d}}{t^p}$$

... with temperature/stress
dependent Omori exponent

$$p \approx 1 + \frac{T}{T_d} - K(\sigma_c - \sigma_0) \frac{\sqrt{T}}{2T_d}$$

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- Overall constant stress $\sigma_0 = F_0/N < \sigma_c$
- Same stiffness $\kappa = 1$
- Same fiber extension : x
- Random critical loads x_i , pdf Gaussian pdf , variance T_d
- Thermal fluctuations via a new noise term $\eta(t)$, variance T

→ Analytical determination of failure rate during creep due the constant stress loading

Omori law

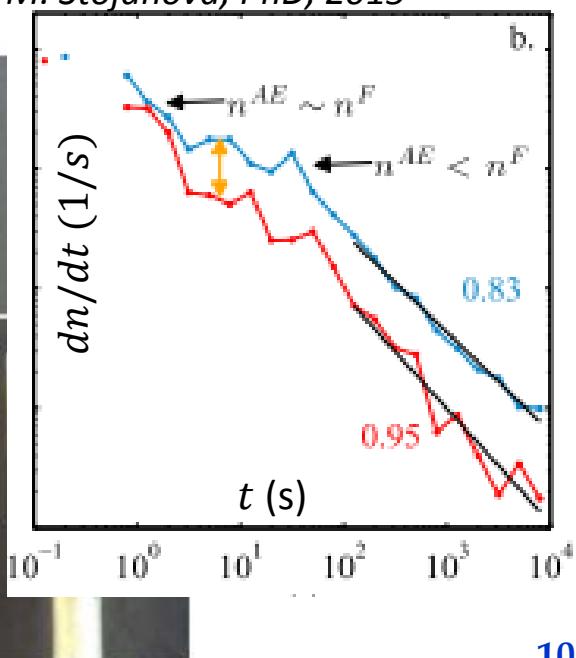
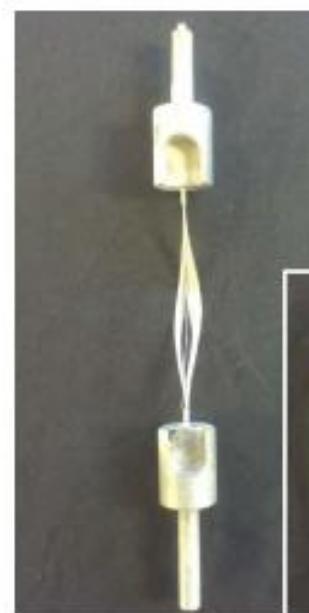
$$\frac{dn}{dt} \approx \frac{A\sqrt{T/T_d}}{t^p}$$

... with temperature/stress dependent Omori exponent

$$p \approx 1 + \frac{T}{T_d} - K(\sigma_c - \sigma_0) \frac{\sqrt{T}}{2T_d}$$

Used to interpret creep experiments in e-glass bundle instrumented in acoustic

From M. Stojanova, PhD, 2015



Fiber Bundle Models (FBM): the approach

Material simplified to:

N parallel brittle fibers

Same stiffness $\kappa = 1$

Random failure threshold



F.T. Pierce, 1926

H.E. Daniels, 1945

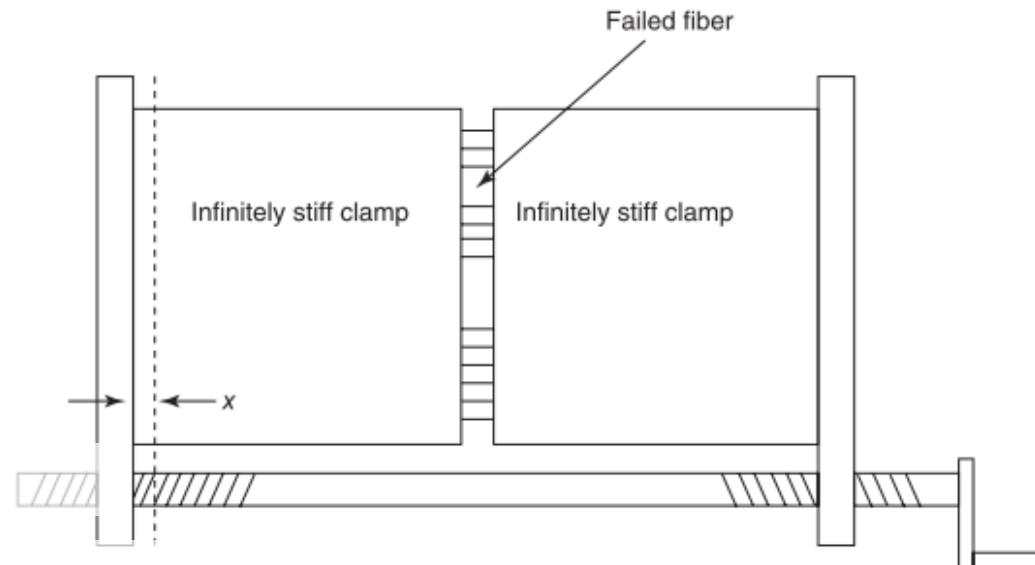
Prescribed rules for load redistribution

Equal load Sharing (ELS)

all intact fibers share same fraction

Local load Sharing (LLS)

Load of failed fiber redistributed to intact nearest-neighbors only



Intermediate load Sharing (ILS)

Load transfer decreases distance from failed fiber

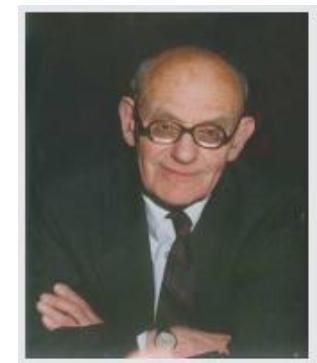
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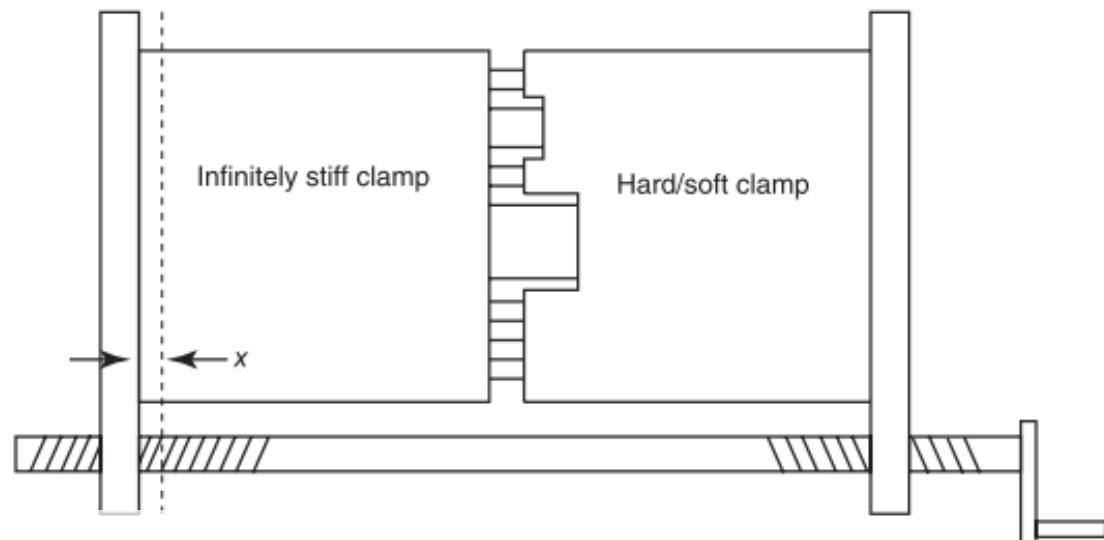
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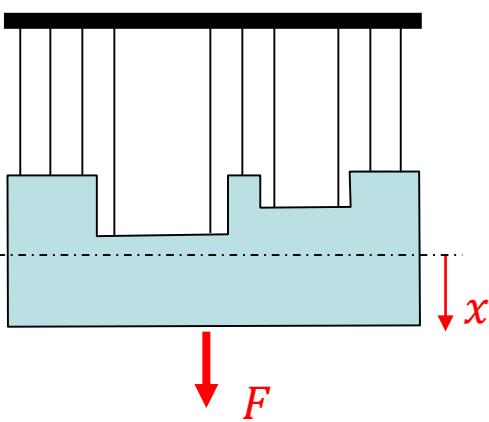
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LLS -- FBM: 1D models

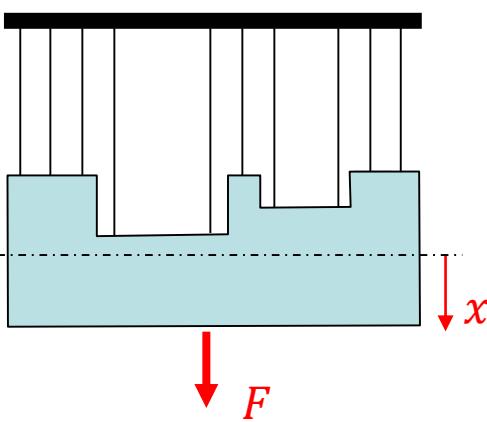


- N parallel brittle fibers
- Overall stretching force F , => stress $\sigma = F/N$
- Same stiffness $\kappa = 1$
- Random critical loads x_i^c , pdf $p(x^c)$, cumulative $P(x^c)$
- Fiber extension : $x_i = \sigma(1 + k_i/2)$
 k_i =nb. of failed nearest-neighbor fibers



Full analytical solutions not available anymore

LLS -- FBM: 1D models



- N parallel brittle fibers
- Overall stretching force F , => stress $\sigma = F/N$
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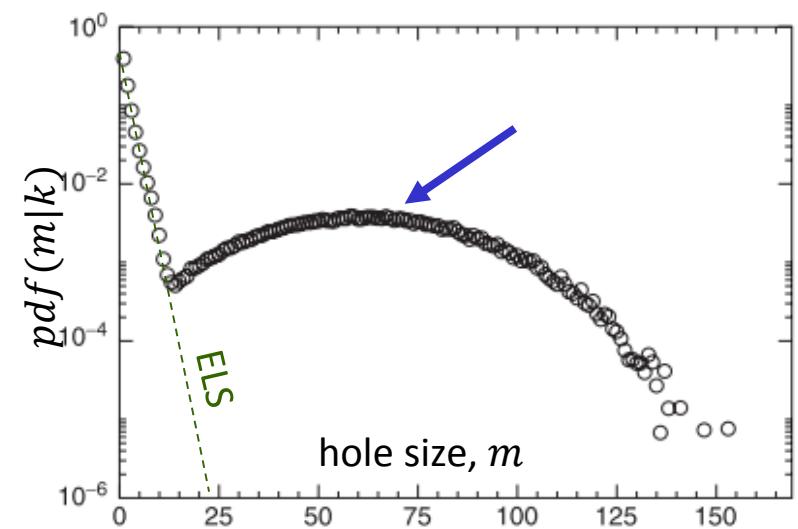
Pdf of hole size after k breaking

Uniform: $P(x) = x$ $N = 1000$, $k = 200$

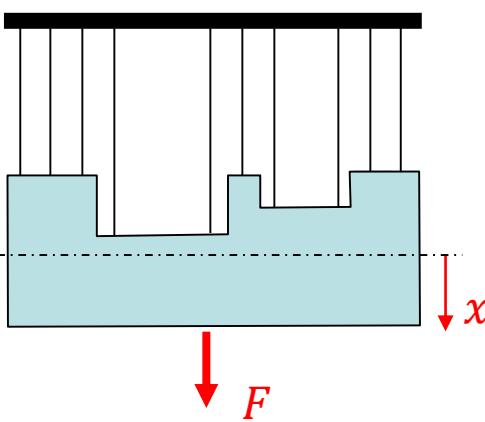
Hansen et al. (Wiley & son, 2015)



Localization captured



LLS -- FBM: 1D models



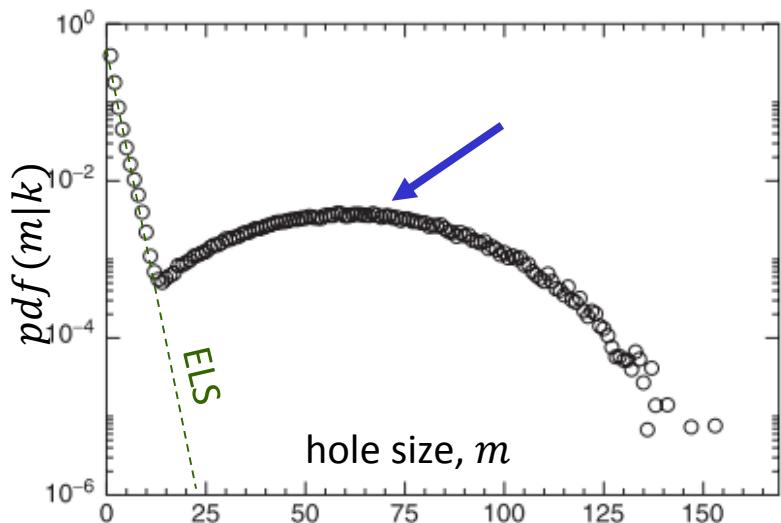
- N parallel brittle fibers
- Overall stretching force F , => stress $\sigma = F/N$
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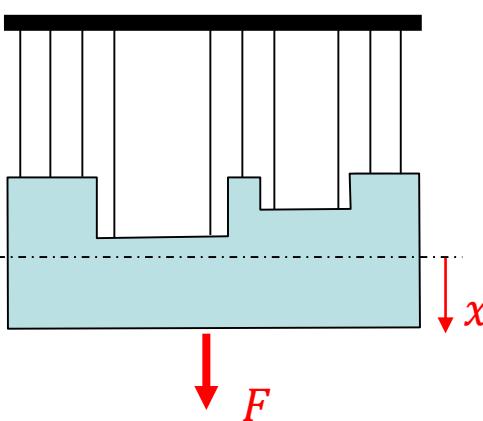
Uniform: $P(x) = x$ $N = 1000$, $k = 200$
Hansen et al. (Wiley & son, 2015)



Localization captured
highly dependent of $P(x)$...
... importance: x_{min}^c and $P(x) \approx x_{min}^c$

- $x_{min}^c = 0, P(x) = x^\beta, \beta \rightarrow \infty$
infinite disorder, no localization, ELS
- $x_{min}^c = 2/3$, uniform above,
fully localized, single crack growth

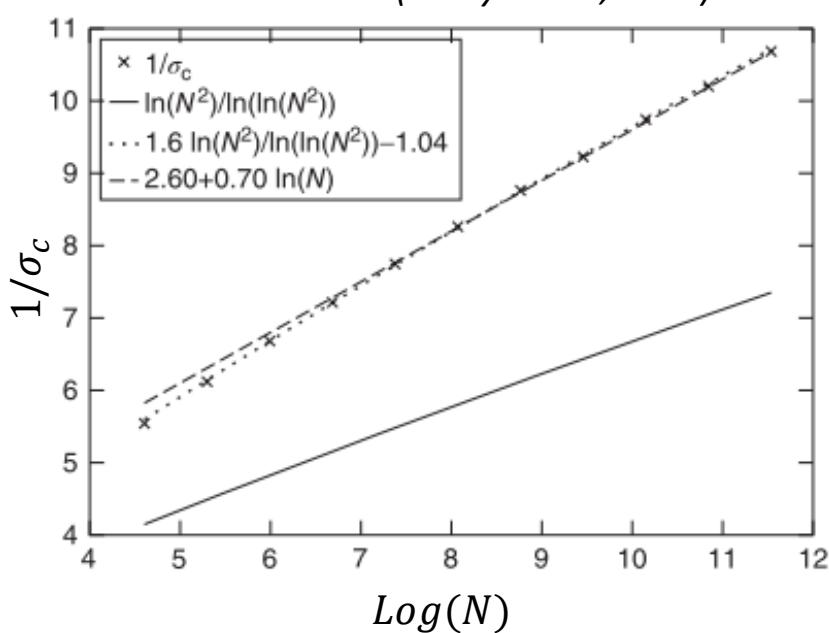
LLS -- FBM: 1D models, size effect on strength



- N parallel brittle fibers
- Overall stretching force F , => stress $\sigma = F/N$
- Same stiffness $\kappa = 1$
- Fiber extension : $x_i = \sigma(1 + k_i/2)$
 k_i =nb. of failed nearest-neighbor fibers
- Random critical loads x_i^c with distribution $p(x^c)$
[cumulative $P(x^c)$]



Size effect can be reproduced
But depend of $P(x)$, x_{min}^c and $P(x \approx x_{min}^c)$

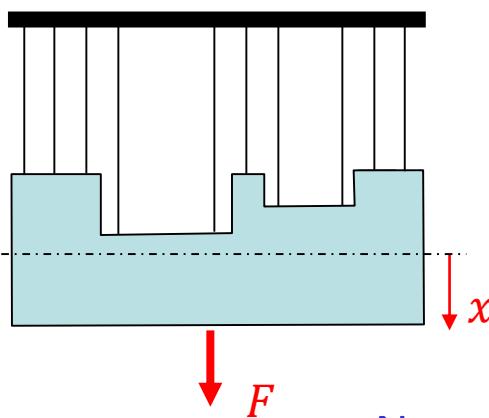


Case of uniform distribution, $P(x) = x$

Numerics, simple estimates: $\sigma_c \approx 1/\log(N)$
Zhang & Ding, Phys. Lett. A 1994, PRB &995

More refined: $\sigma_c \approx \log(\log(N^2))/\log(N^2)$
Hansen et al (Wiley & son, 2015)

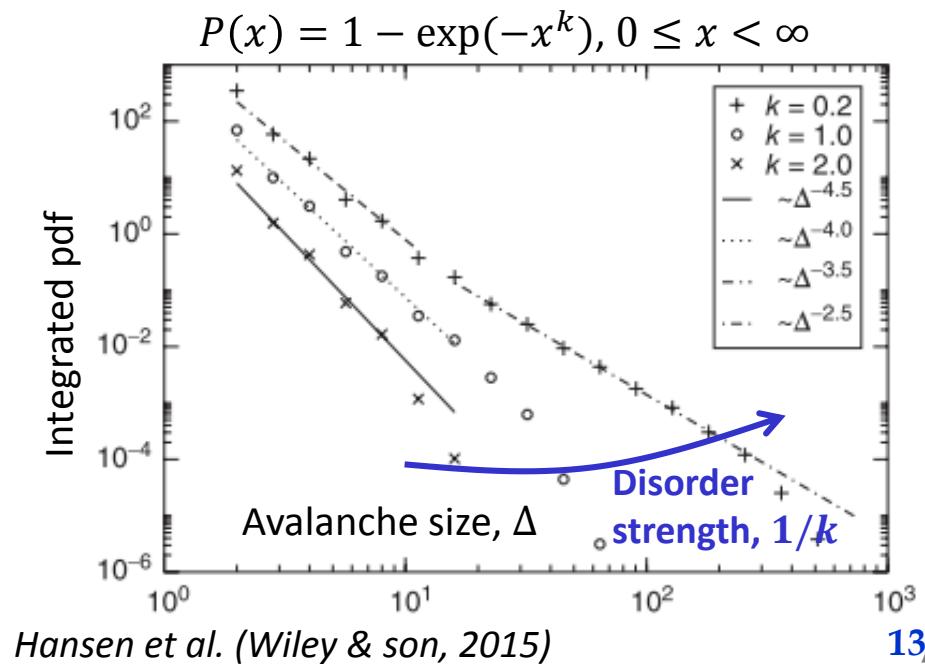
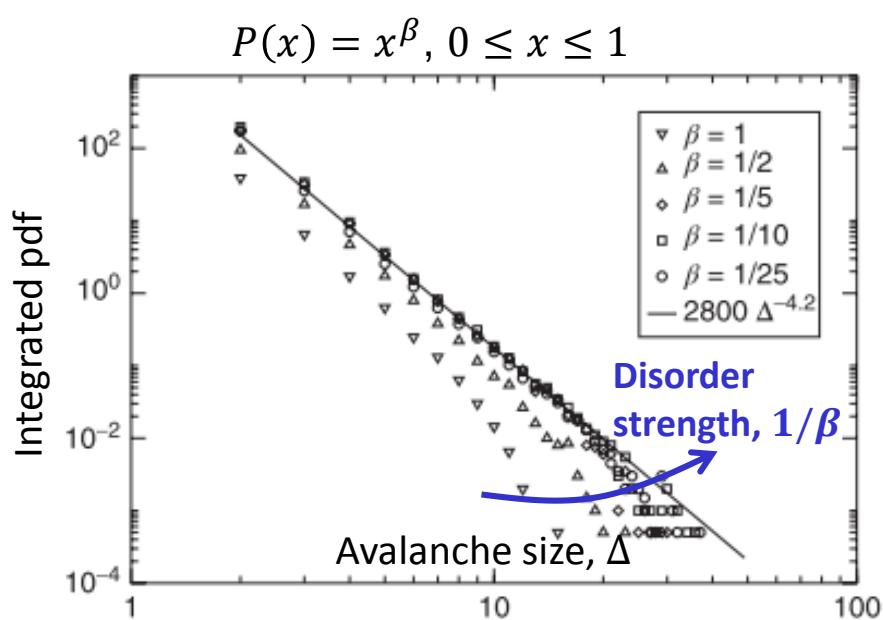
LLS -- FBM: 1D models, avalanche distribution



- N parallel brittle fibers
- Overall stretching force F , => stress $\sigma = F/N$
- Same stiffness $\kappa = 1$
- Fiber extension : $x_i = \sigma(1 + k_i/2)$
 k_i =nb. of failed nearest-neighbor fibers
- Random critical loads x_i^c with distribution $p(x^c)$
[cumulative $P(x^c)$]

Non-universal size-distributions,
Depend on critical load distribution, $P(x)$

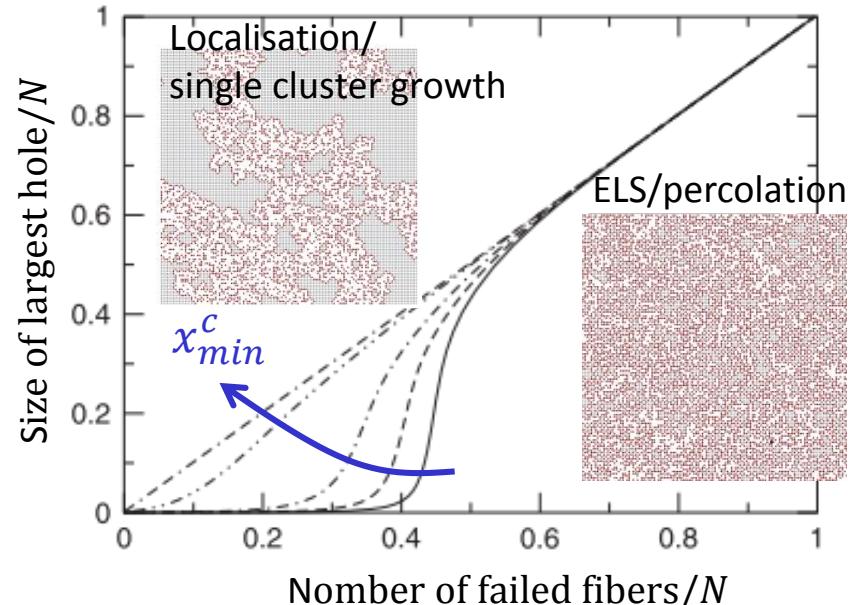
Zhang & Ding Phys. Lett. A 1994, Pradhan et al. RMP, 2010



LLS – FBM in higher dimensions

Localization less important in 2d

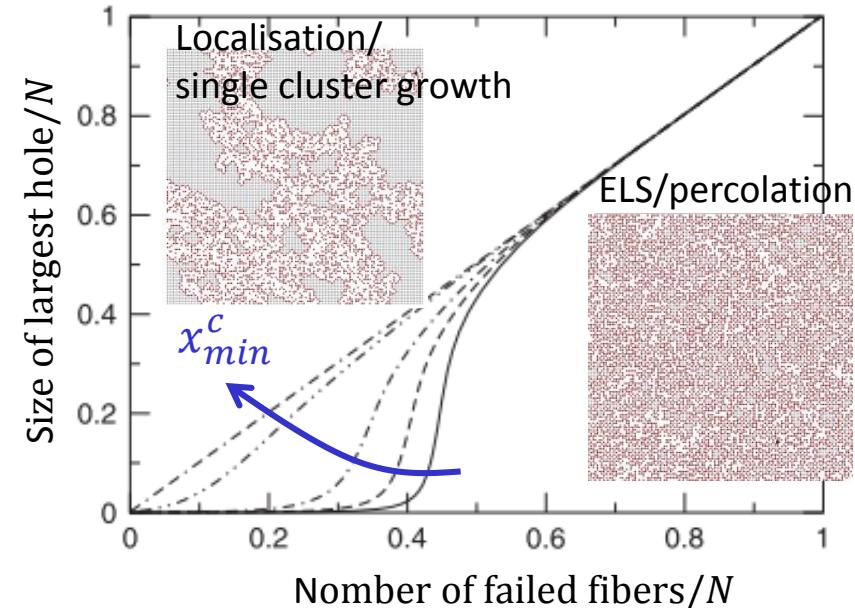
→ finite x_{min}^c now required to activate localization



LLS – FBM in higher dimensions

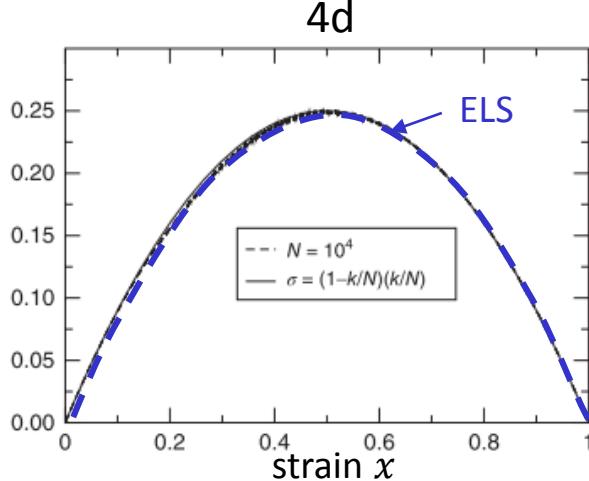
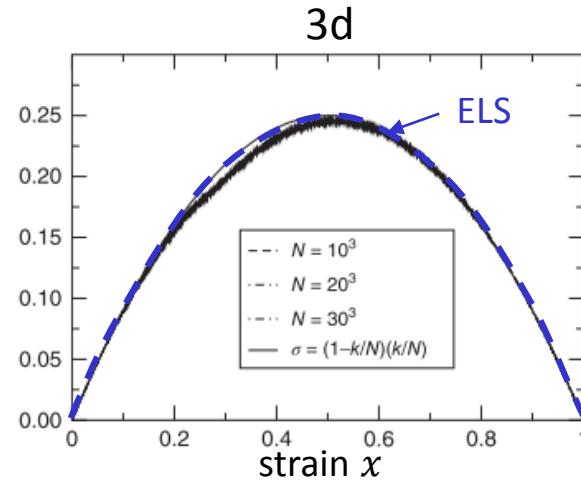
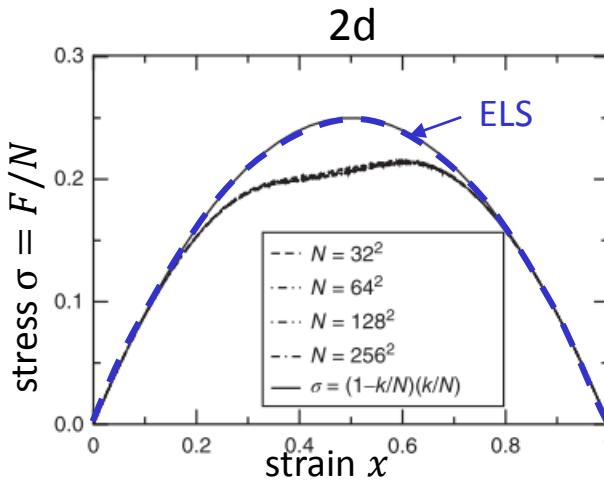
Localization less important in 2d

→ finite x_{min}^c now required to activate localization



Stress-strain curve in LLS for uniform distribution, $P(x^c) = x^c$, over $[0,1]$

From Hansen et al. (Wiley & son, 2015)



When dimensionality increases, LLS-FBM looks more and more to ELS-FBM !

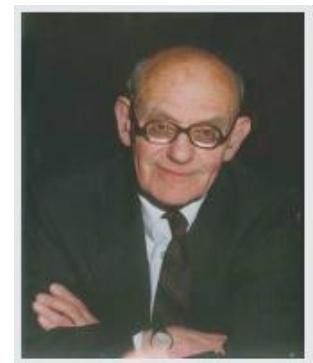
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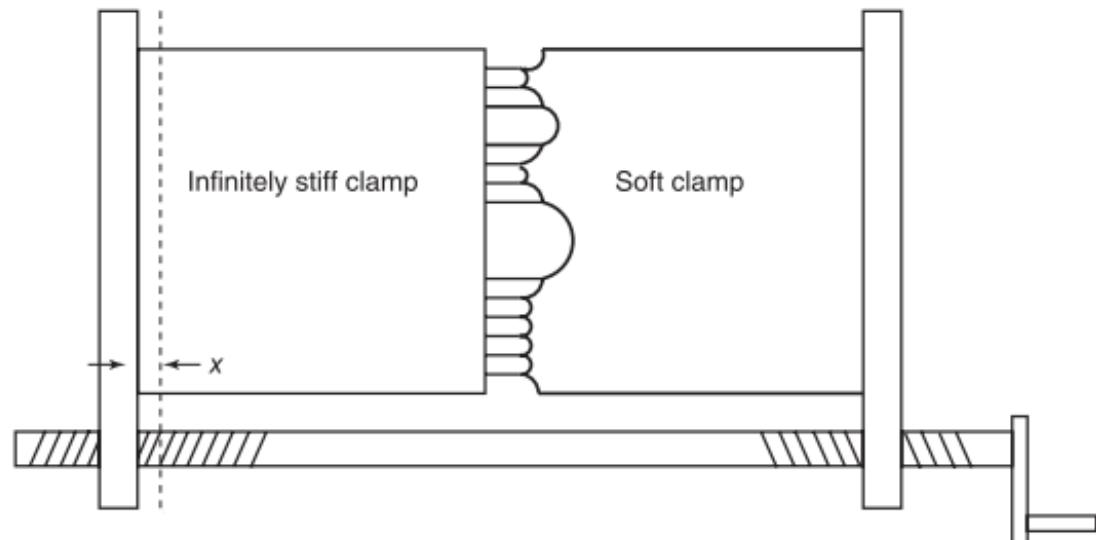
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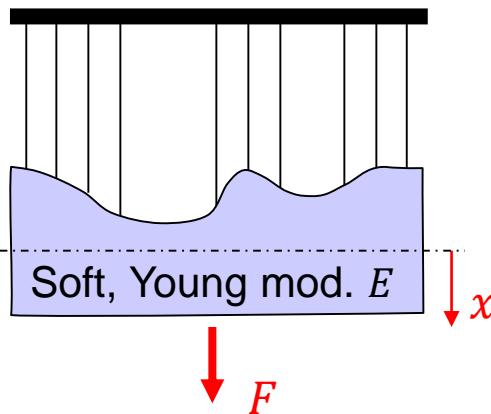


Intermediate load Sharing (ILS)

Load transfer decreases distance from failed fiber

An example of FLS -- FBM: Soft-clamp model

Stormo, Gjerden, Hansen PRE, 2012



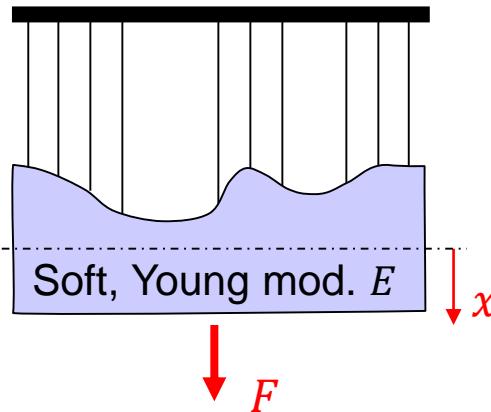
- N parallel brittle fibers, Overall force F , => stress $\sigma = F/N$
- Same stiffness $\kappa = 1$
- Random critical loads x_i^c , pdf $p(x^c)$, cumulative $P(x^c)$
- Forces between fibers redistributed via the elastic clamp

$$\therefore \sigma_i = \kappa(x_i - x), x_i = \sum_j G_{ij} \sigma_j,$$

G_{ij} = green function for 2D elastic infinite half space

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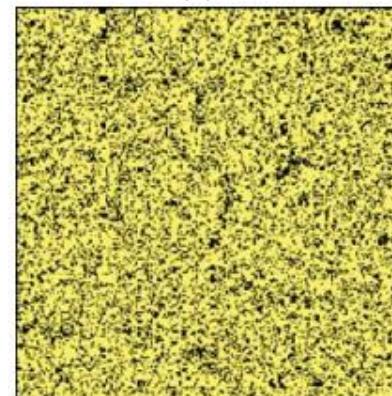
G_{ij} = green function for 2D elastic infinite half space

Control parameter for interaction: $e = E/N$

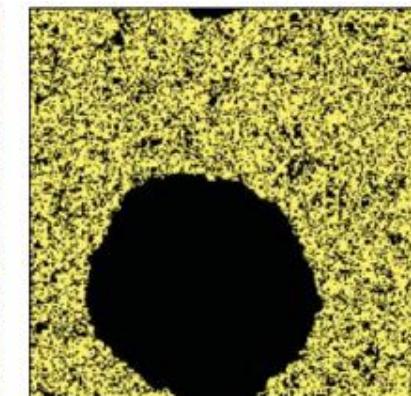
→ Increasing size \equiv softer clamp

Transition from LLS (small e)
to ELS (large e)

$$e_{stiff} = 2^6$$



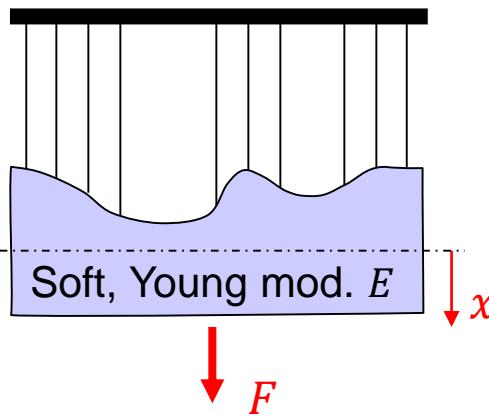
$$e_{soft} = 2^{-17}$$



From Hansen et al. (Wiley & son, 2015)

An example of FLS -- FBM: Soft-clamp model

Stormo, Gjerden, Hansen PRE, 2012



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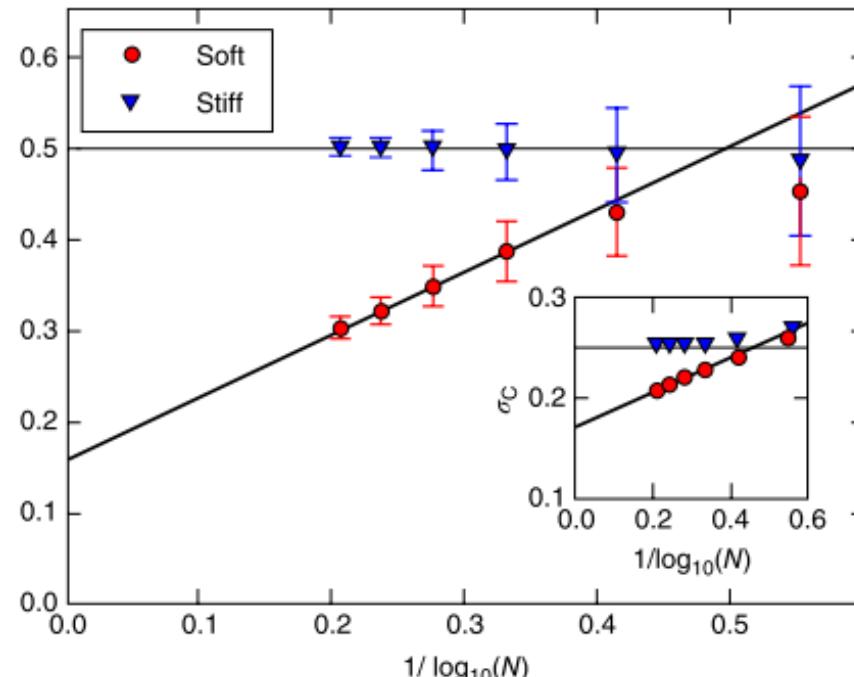
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Transition from LLS (small e)
to ELS (large e)

Size effect on strength at small e ,
absence of size effect at large e



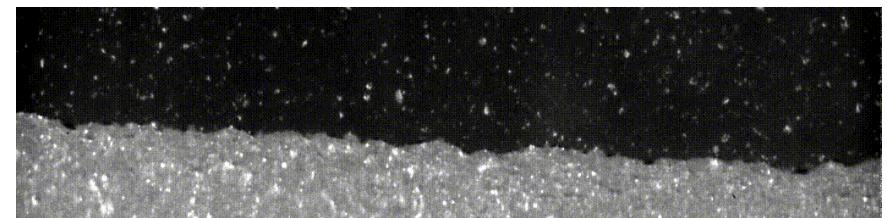
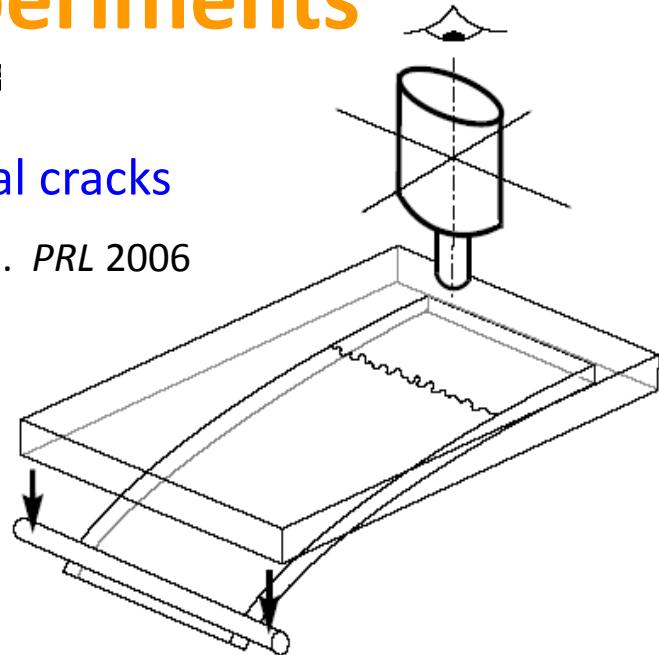
From Stormo et al. PRE, 2012

FBM: Soft-clamp model & experiments

Gjerden, Stormo, Hansen PRL, 2013

Interfacial cracks

Maloy et al. *PRL* 2006

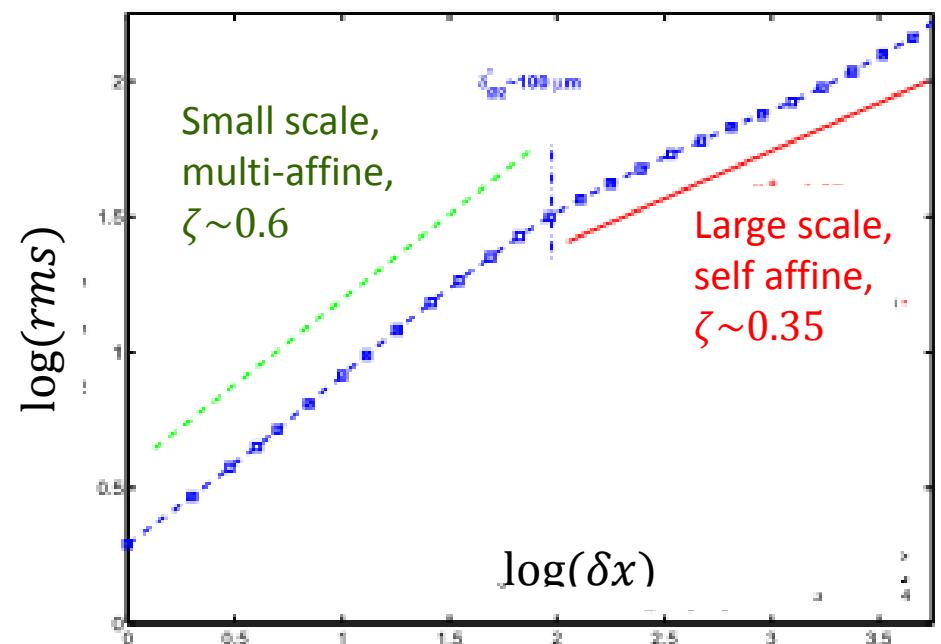
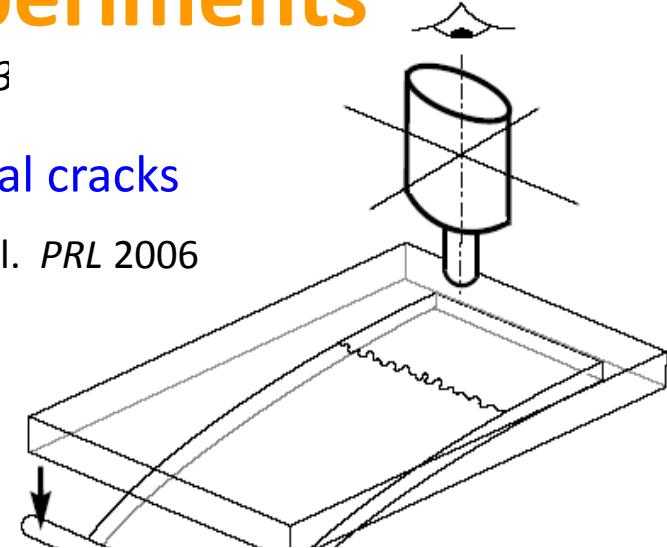


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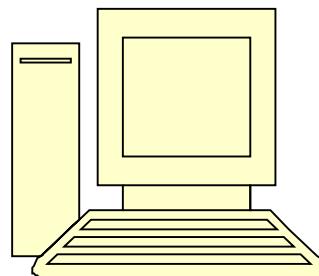
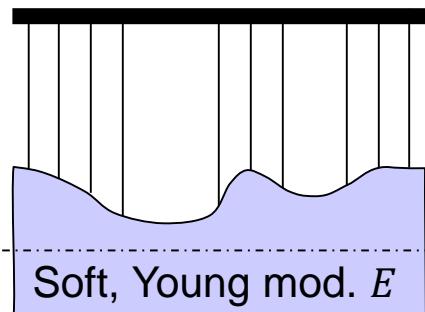
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Maloy et al. PRL 2006



FBM: Soft-clamp model & experiments

Gjerden, Stormo, Hansen PRL, 2013



Large N (soft e)

Self-affine (single) growing front



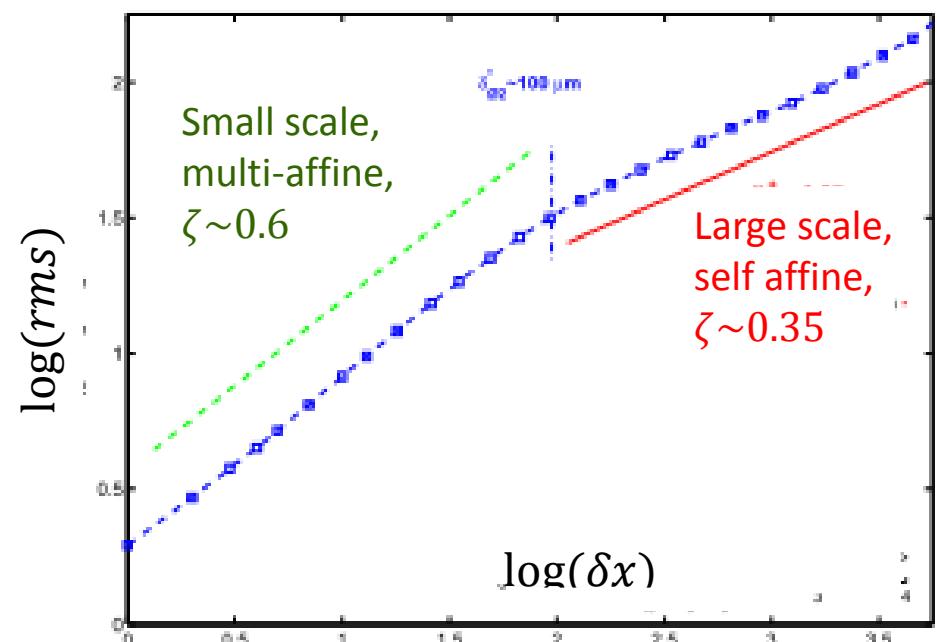
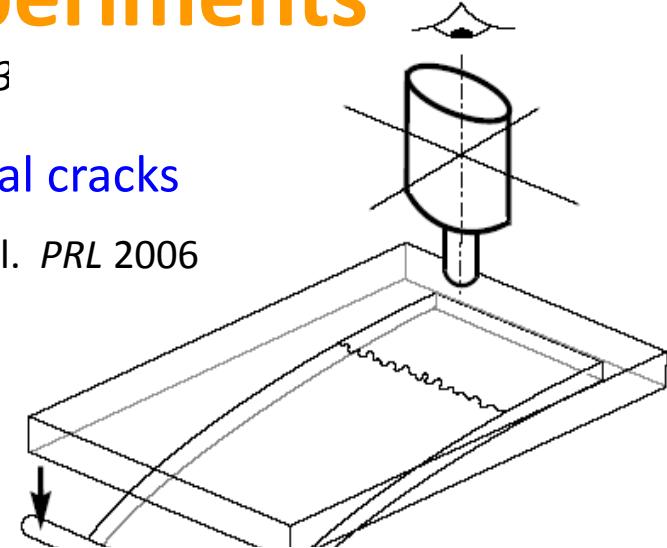
Small N (stiff e)

Fractal percolated clusters



Interfacial cracks

Maloy et al. PRL 2006



→ In (experimental) fracture: ELS/percolation at small scales,
LLS/single crack growth at large scales

FBM: few take-home messages

- FBMs address fracture problems via models of increasing complexity/description ability depending of the redistribution rules
- Simplest one: Equal-load-Sharing FBM :
 - fully tractable analytically, fracture \leftrightarrow critical phenomena
 - capture qualitatively gradual damaging before failure, scale-free precursor avalanches, response in creep,
 - ail capturing localization and size effects
- Local-load-Sharing FBM
 - Not tractable numerically anymore
 - Capture localization and size effects
 - No universality, very dependent on threshold distribution (and its minimum)
 - As dimension increases, looks more and more to ELS
- Soft-clamp FBM
 - LLS at large scales, ELS at small scales
 - Explain 2 scaling regimes in fracture depending on length-scales

Thank you for your attention

WILEY-VCH

Alex Hansen, Per C. Hemmer, Srutarshi Pradhan

The Fiber Bundle Model

Modeling Failure in Materials



To know more

REVIEWS OF MODERN PHYSICS, VOLUME 82, JANUARY–MARCH 2010

Failure processes in elastic fiber bundles

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NO-7491 Trondheim, Norway
and SINTEF Petroleum Research, NO-7465 Trondheim, Norway*

Alex Hansen†

*Department of Physics, Norwegian University of Science and Technology,
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Computational Science, Saha Institute of Nuclear Physics, 1/AF Bidhan Nagar,
Kolkata 700064, India*

(Published 1 March 2010)

The fiber bundle model describes a collection of elastic fibers under load. The fibers fail successively and, for each failure, the load distribution among the surviving fibers changes. Even though very simple, this model captures the essentials of failure processes in a large number of materials and settings. A review of the fiber bundle model is presented with different load redistribution mechanisms from the point of view of statistics and statistical physics rather than materials science, with a focus on concepts such as criticality, universality, and fluctuations. The fiber bundle model is discussed as a tool for understanding phenomena such as creep and fatigue and how it is used to describe the behavior of fiber-reinforced composites as well as modeling, e.g., network failure, traffic jams, and earthquake dynamics.