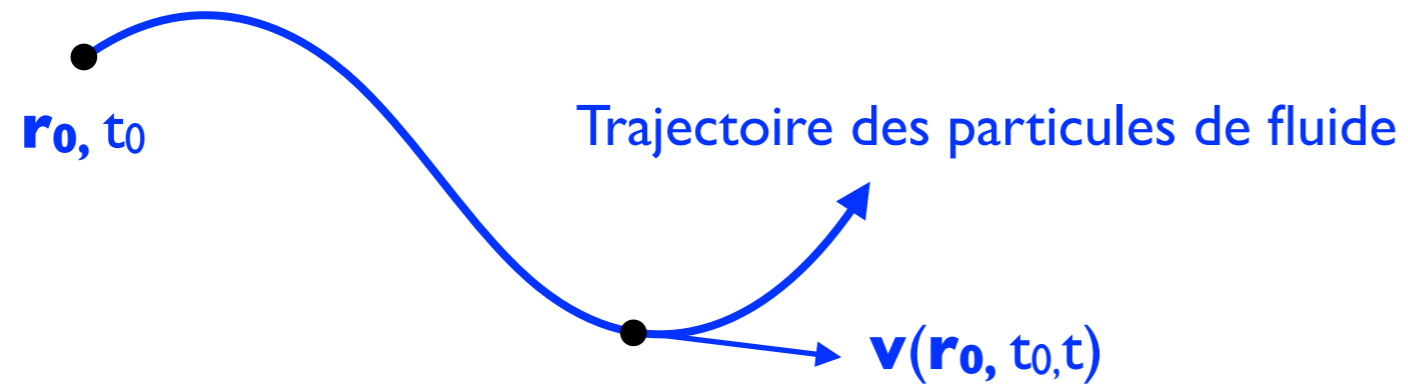


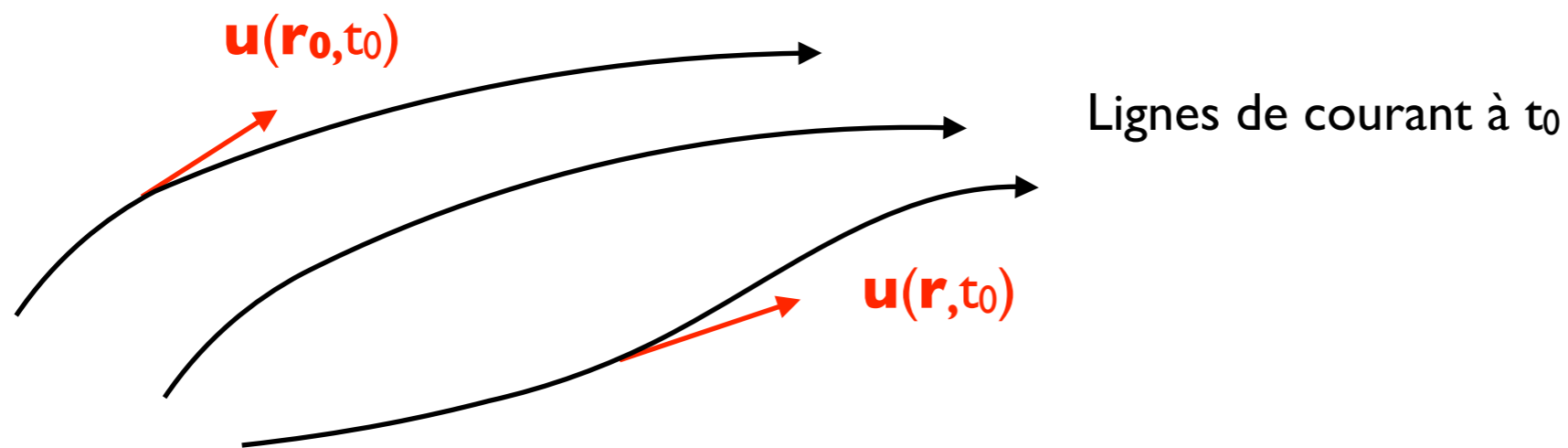
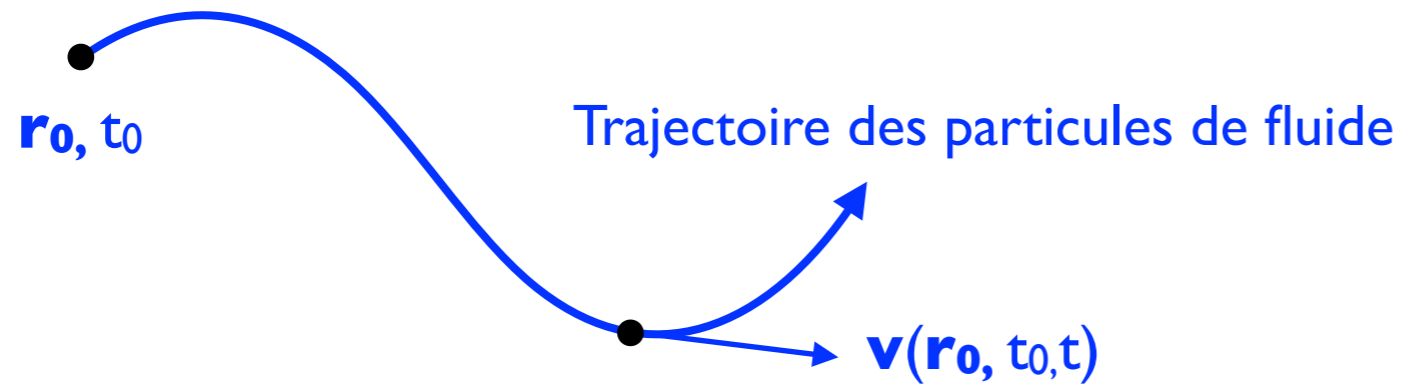
Description des écoulements

Description lagrangienne

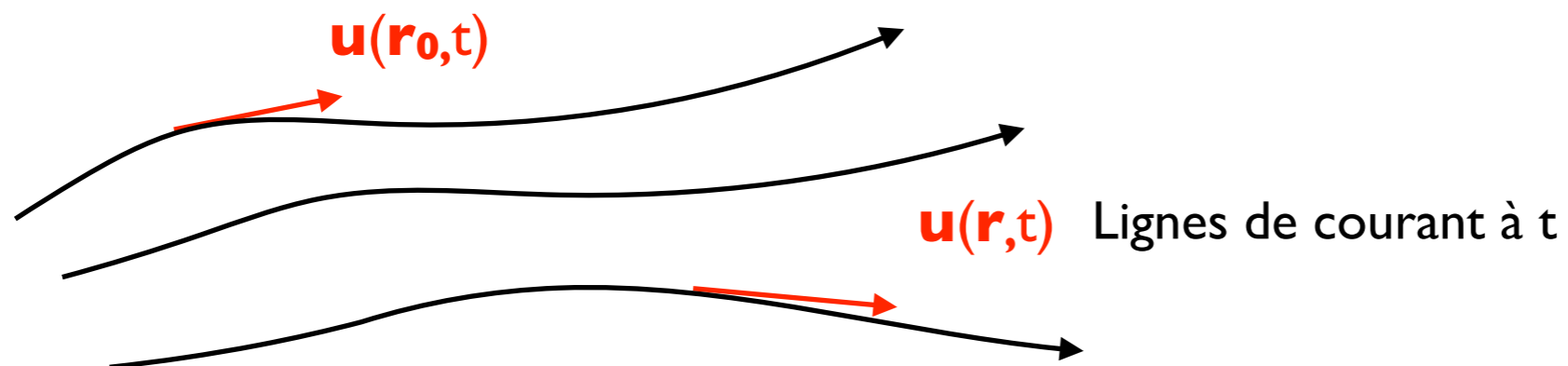


Description des écoulements

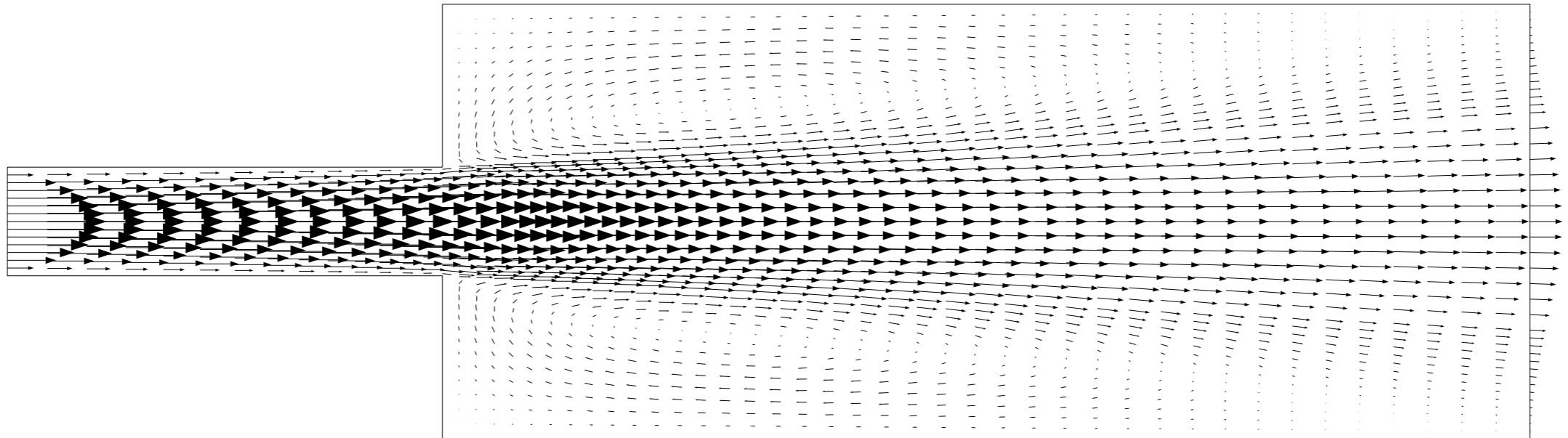
Description lagrangienne



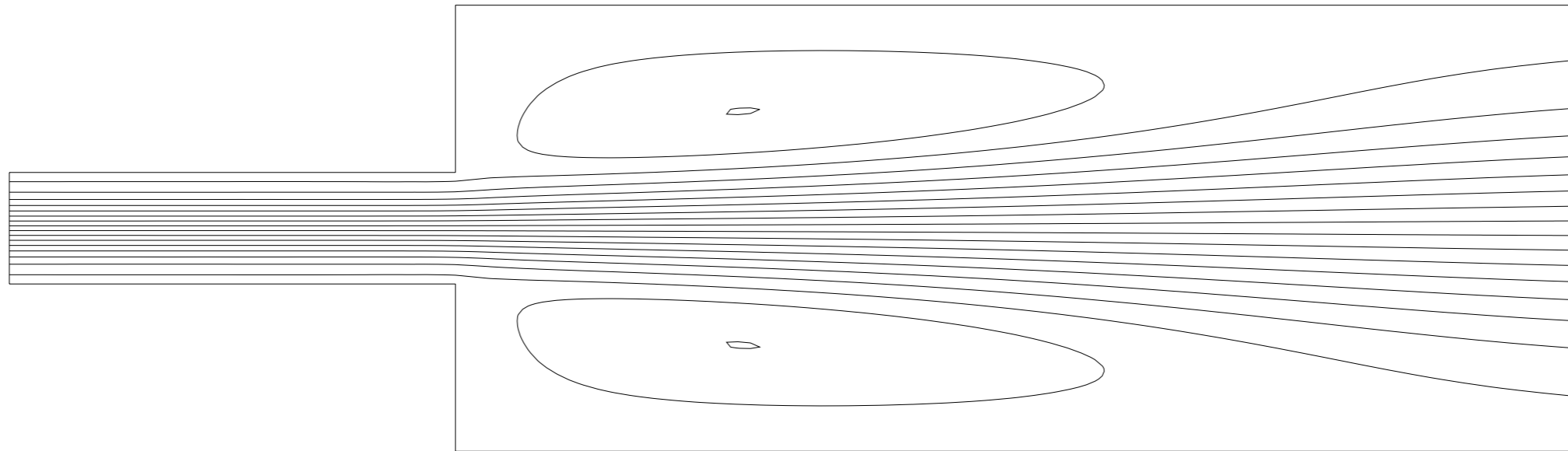
Description eulerienne



Un exemple de champ de vitesse eulérienne

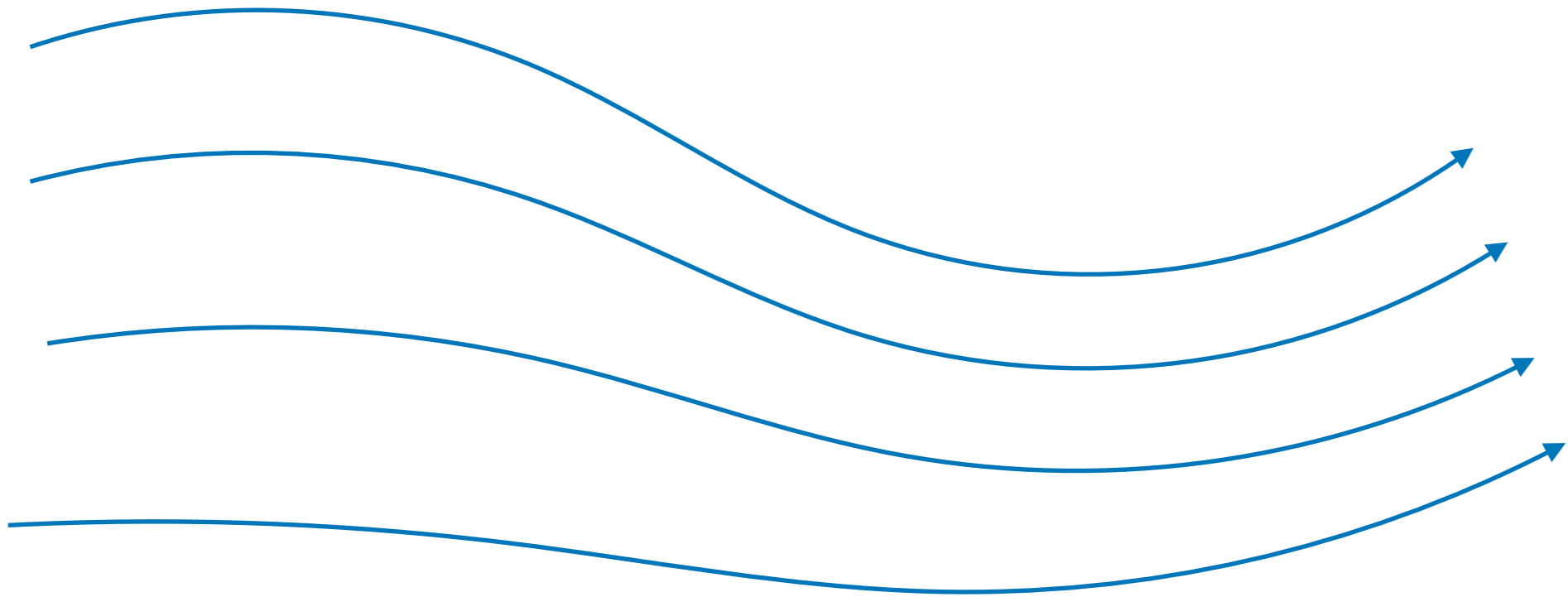


Vecteurs vitesse

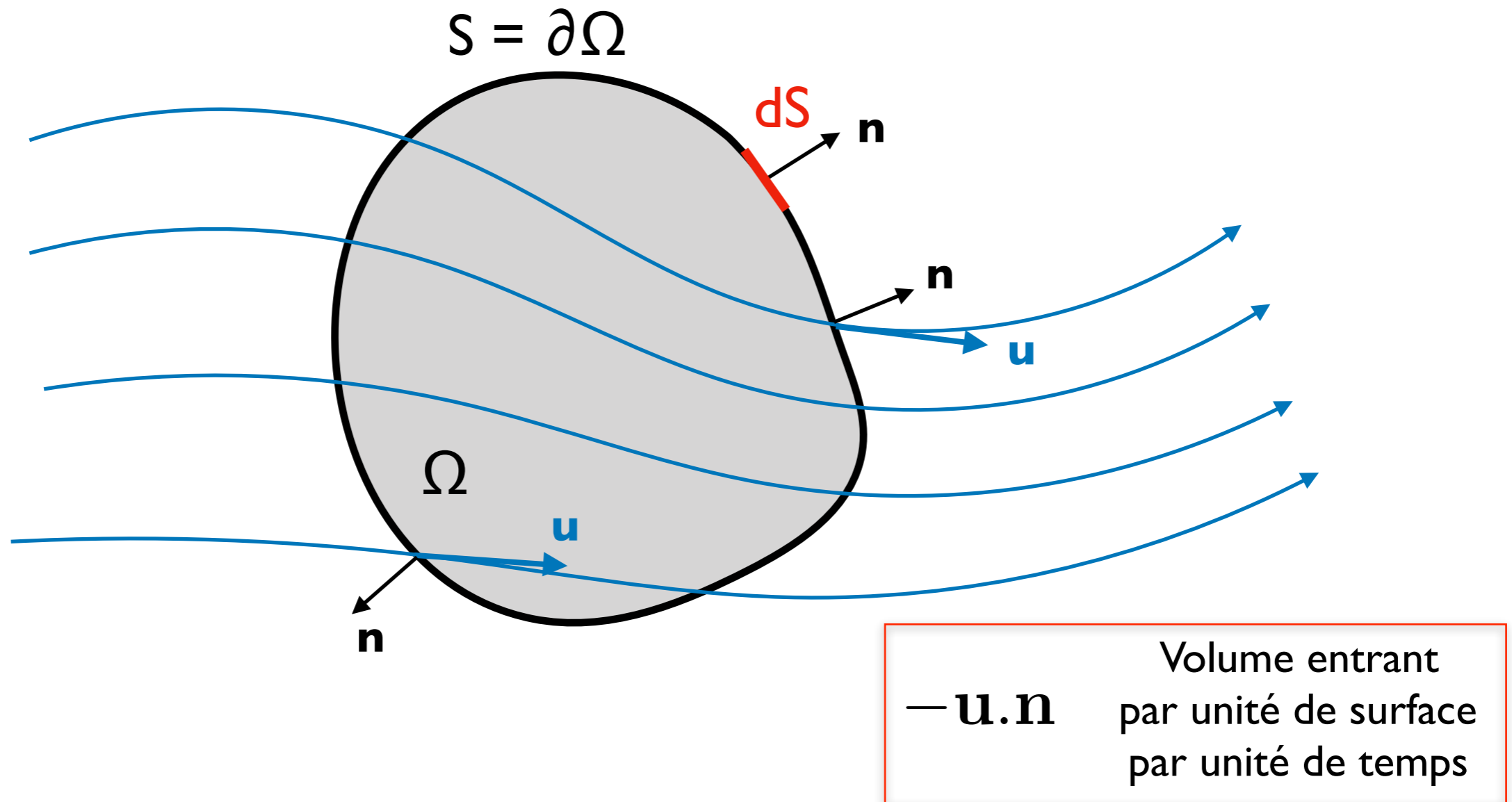


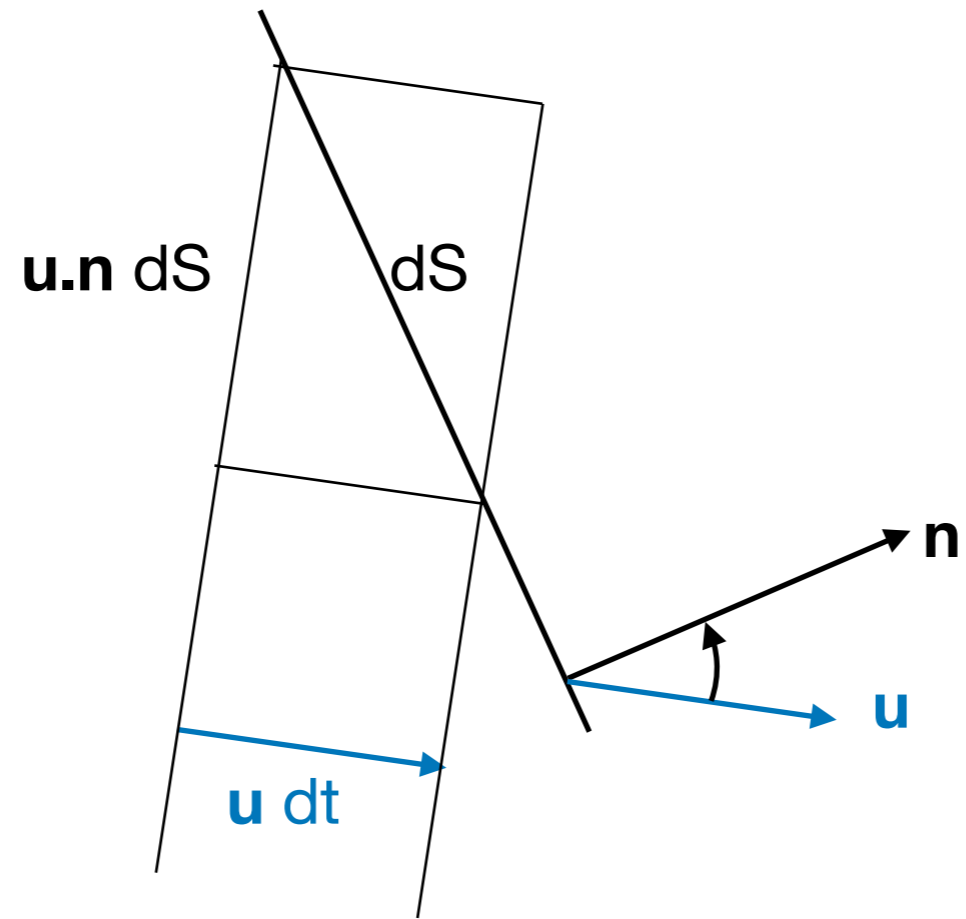
Lignes de courant

Conservation de la masse dans un écoulement

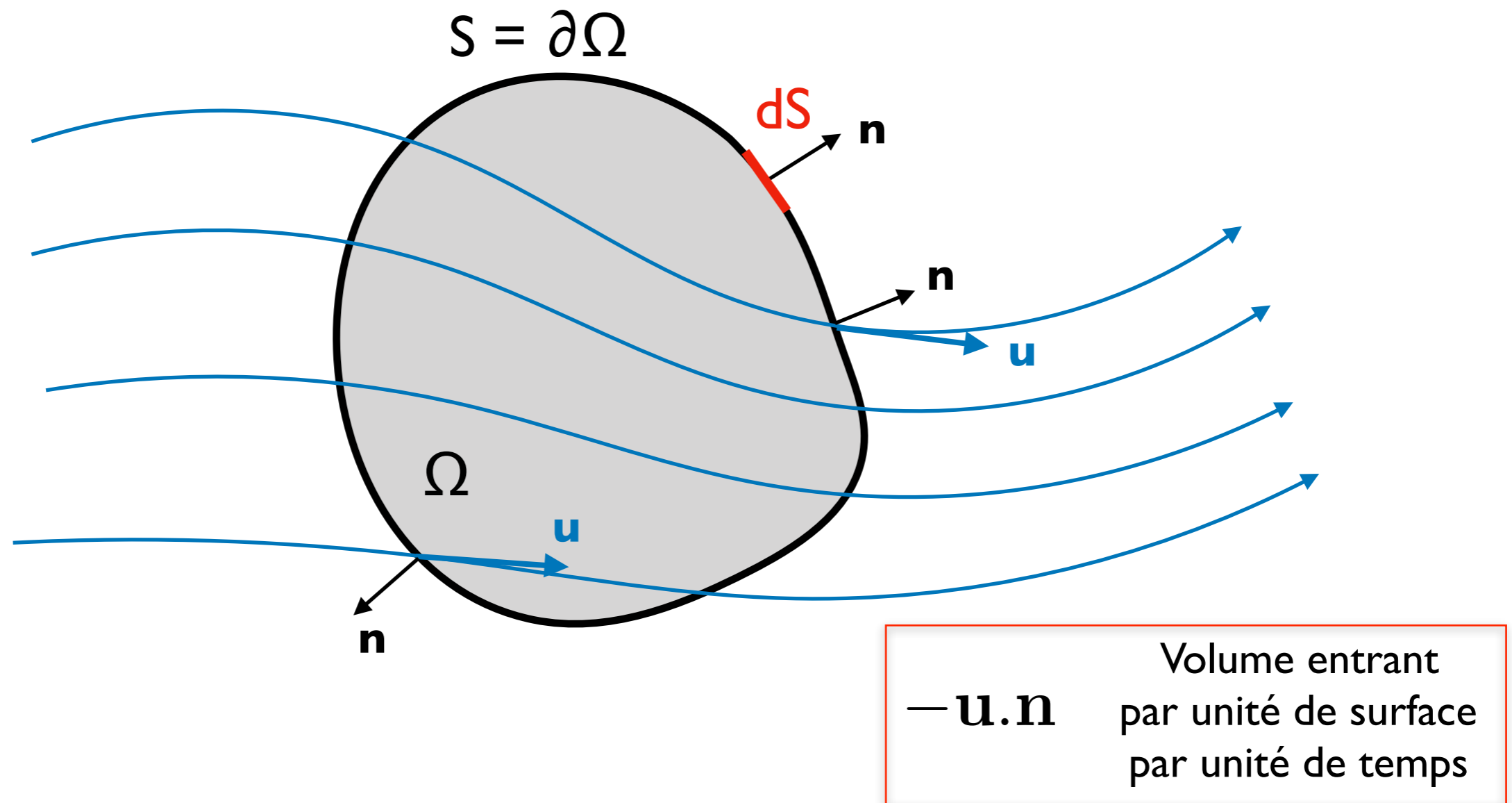


Conservation de la masse dans un écoulement



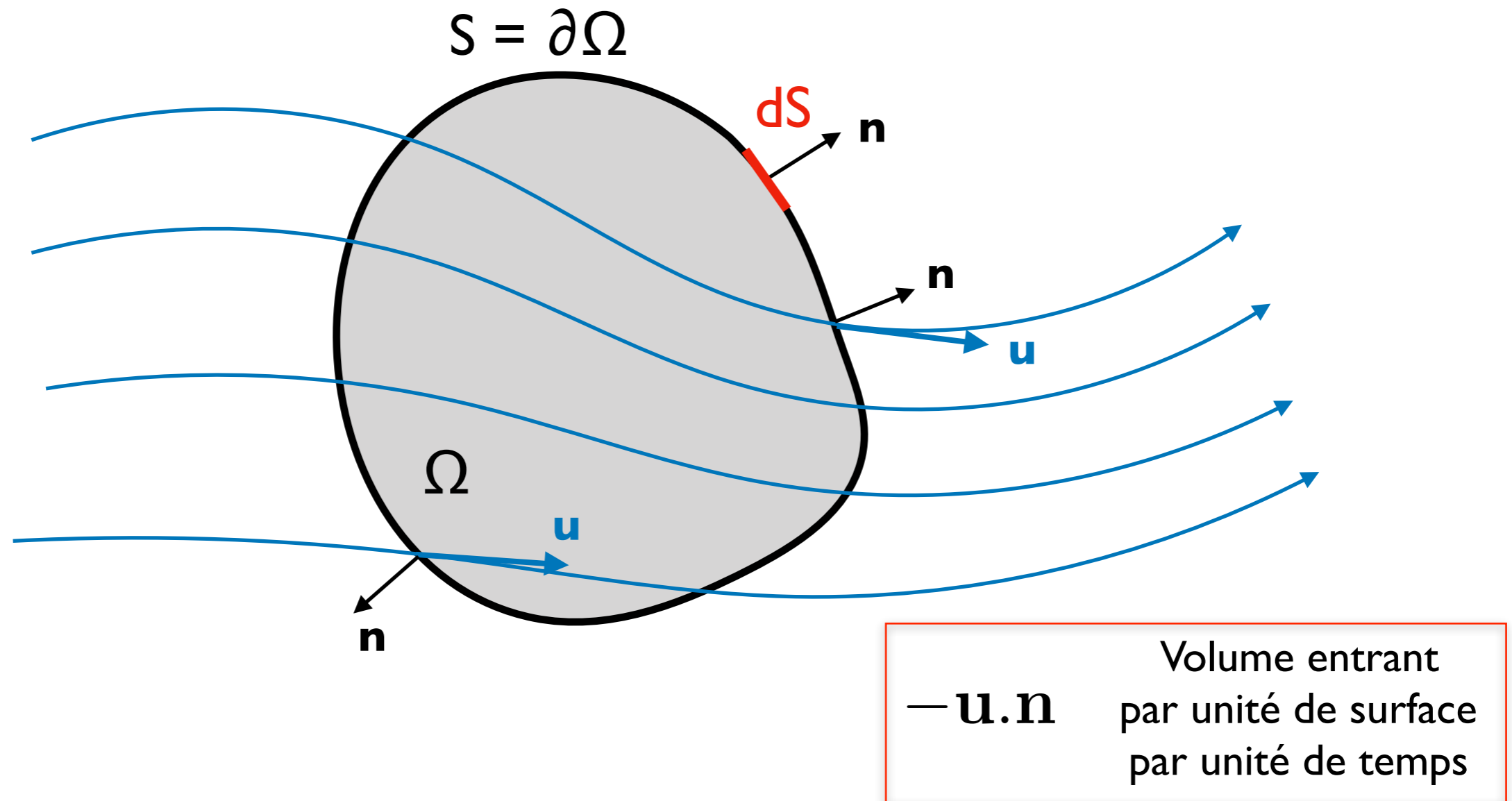


Conservation de la masse dans un écoulement



$$-\int_{\partial\Omega} \rho \mathbf{u} \cdot \mathbf{n} dS + Q$$

Conservation de la masse dans un écoulement




$$\int_{\Omega} \frac{\partial \rho}{\partial t} dV = - \int_{\partial\Omega} \rho \mathbf{u} \cdot \mathbf{n} dS + Q$$

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$\nabla \cdot \equiv$ divergence


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En l'absence de source de masse

$$\frac{\partial \rho}{\partial t} + \rho \nabla \cdot \mathbf{u} + \mathbf{u} \cdot \nabla \rho = 0$$

$\nabla \equiv$ gradient

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En l'absence de source de masse

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$\nabla \equiv$ gradient

Si le fluide est « incompressible », masse volumique constante

$$\nabla \cdot \mathbf{u} = 0$$

Fluide comme “incompressible” ?

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$$\frac{\delta \rho}{\rho} = \frac{1}{\rho} \frac{\partial \rho}{\partial p} \delta p$$

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c : vitesse du son

Fluide comme “incompressible” ?

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c : vitesse du son

En écoulement dominé par l'inertie du fluide: $\delta p \sim \rho u^2$

$$\frac{\delta \rho}{\rho} \sim \frac{u^2}{c^2} = M^2$$

M : Nombre de Mach

Fluide comme “incompressible” ?

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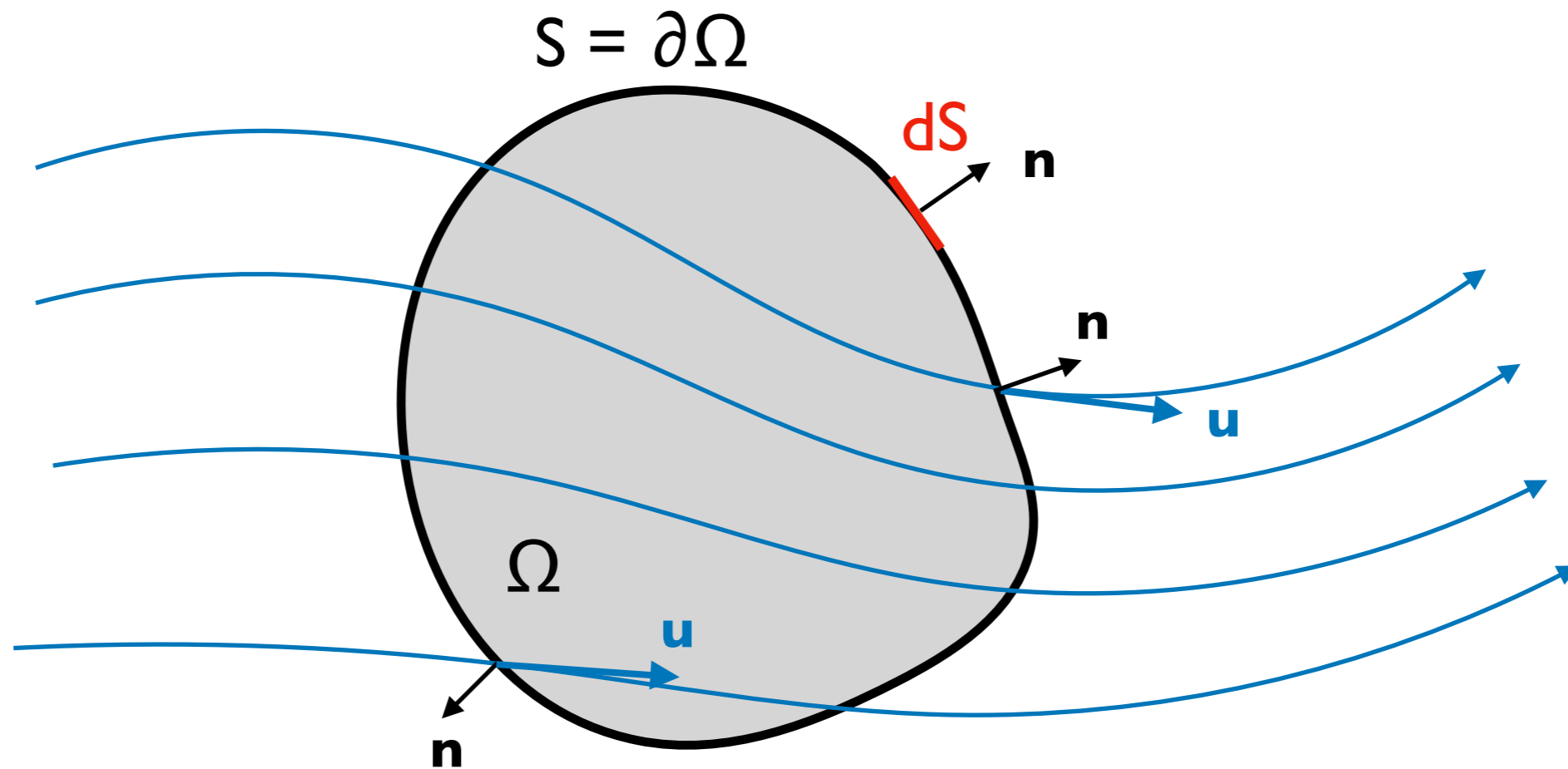
$M \ll 1$ Fluide quasi incompressible



$M \sim 1$ ou $M > 1$

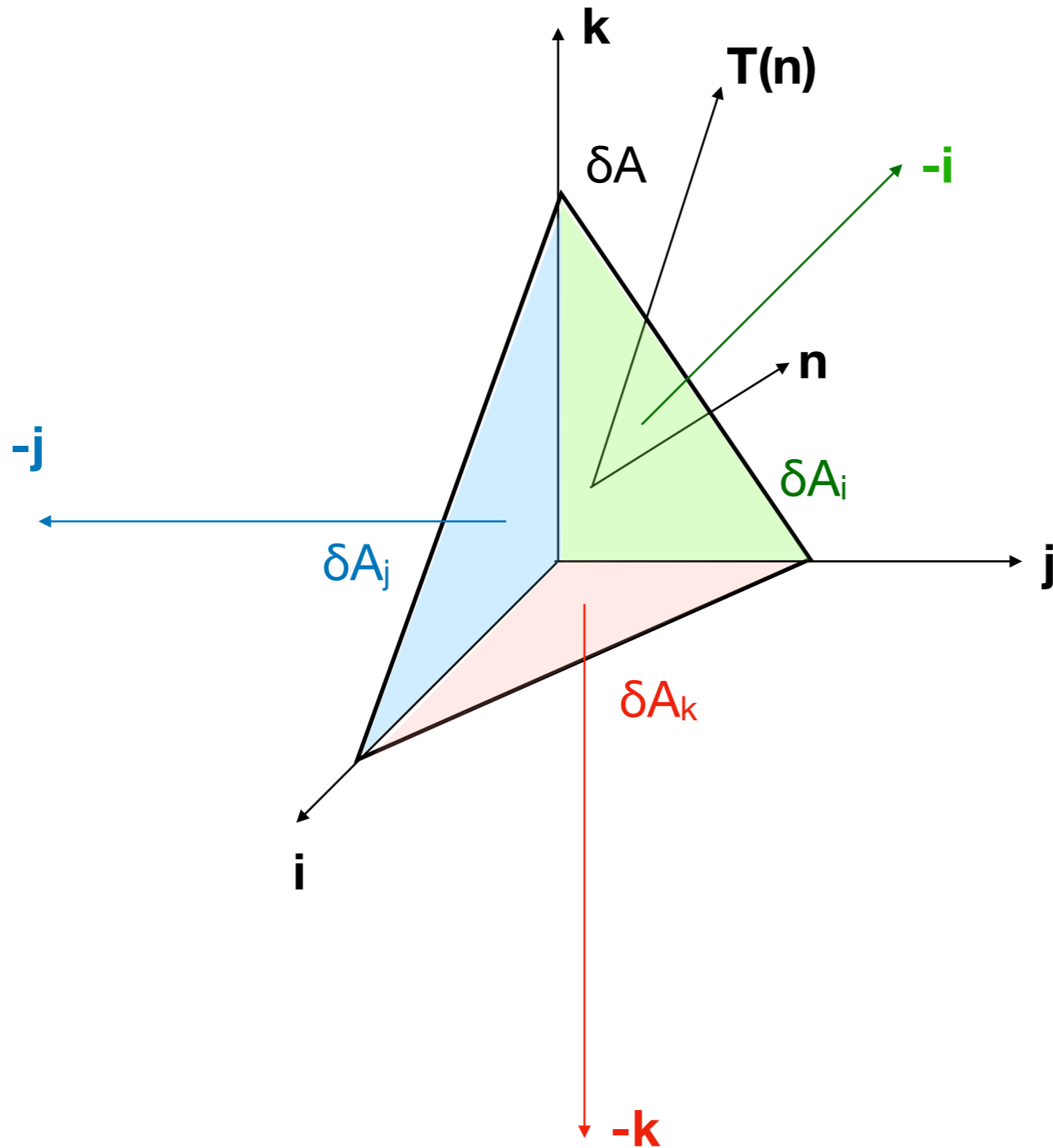
Ondes de choc

Conservation de la quantité de mouvement



$$\int_{\Omega} \frac{\partial \rho \mathbf{u}}{\partial t} dV = \int_{\Omega} \rho \mathbf{f} dV - \int_{\partial\Omega} \underbrace{\rho \mathbf{u}}_{\text{vecteur}} \underbrace{\mathbf{u} \cdot \mathbf{n}}_{\text{scalaire}} dS + \int_{\partial\Omega} \underbrace{\underline{\underline{\sigma}} \cdot \mathbf{n}}_{\text{contraintes}} dS$$

$\mathbf{T}(\mathbf{n})$: vecteur contrainte totale sur la face de normale \mathbf{n}



Forces de surface

$$\mathbf{T}(\mathbf{n})\delta A$$

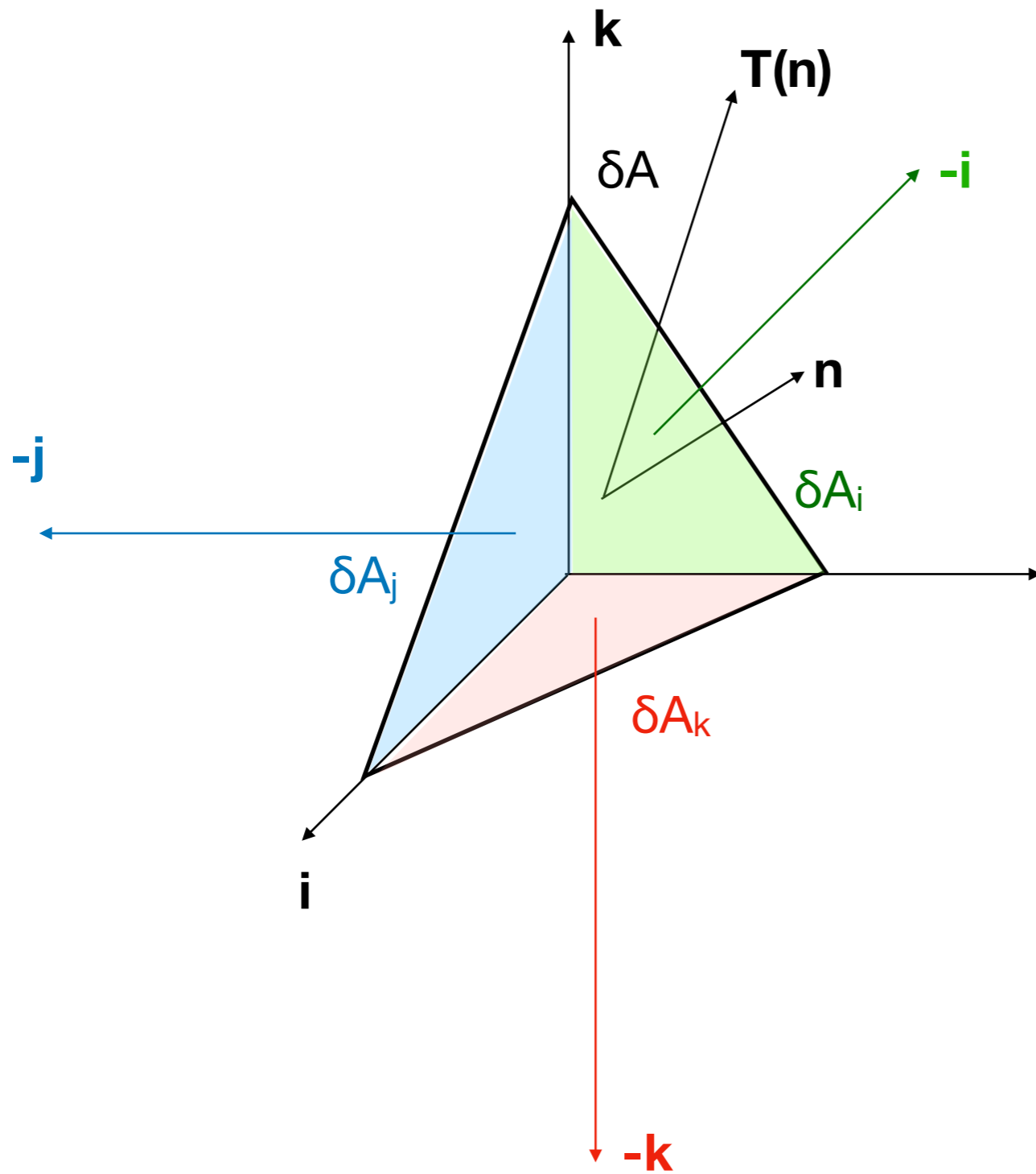
$$\mathbf{T}(-\mathbf{i})\delta A_i$$

$$\mathbf{T}(-\mathbf{j})\delta A_j$$

$$\mathbf{T}(-\mathbf{k})\delta A_k$$

$$\mathbf{T}(-\mathbf{i}) = -\mathbf{T}(\mathbf{i})$$

$$\delta A_i = \delta A \mathbf{i} \cdot \mathbf{n}$$



Forces de surface

$$\mathbf{T}(\mathbf{n})\delta A$$

$$-\mathbf{T}(\mathbf{i}) \mathbf{i} \cdot \mathbf{n} \delta A$$

$$-\mathbf{T}(\mathbf{j}) \mathbf{j} \cdot \mathbf{n} \delta A$$

$$-\mathbf{T}(\mathbf{k}) \mathbf{k} \cdot \mathbf{n} \delta A$$

$$\mathbf{F}_{\text{surface}} = \sum \mathbf{T} \delta A$$

pfd sur l'élément de volume :

$$\rho \delta V \mathbf{a} = \rho \mathbf{f} \delta V + \sum \mathbf{T} \delta A$$

$$\rho \mathbf{a} = \rho \mathbf{f} + \sum \mathbf{T} \frac{\delta A}{\delta V}$$

$$\frac{\delta A}{\delta V} \sim \frac{1}{L} \rightarrow \infty \quad L \rightarrow 0$$

$$\sum \mathbf{T} = 0$$

$$\mathbf{T}(\mathbf{n}) = \mathbf{T}(\mathbf{i}) \mathbf{i} \cdot \mathbf{n} + \mathbf{T}(\mathbf{j}) \mathbf{j} \cdot \mathbf{n} + \mathbf{T}(\mathbf{k}) \mathbf{k} \cdot \mathbf{n}$$

$$\mathbf{T}(\mathbf{n}) = \mathbf{T}(\mathbf{i}) n_x + \mathbf{T}(\mathbf{j}) n_y + \mathbf{T}(\mathbf{k}) n_z$$

Composante x $T_x(\mathbf{n}) = T_x(\mathbf{i}) n_x + T_x(\mathbf{j}) n_y + T_x(\mathbf{k}) n_z$

$$T_x(\mathbf{n}) = \sigma_{xx} n_x + \sigma_{xy} n_y + \sigma_{xz} n_z$$

$$\sigma = \begin{pmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{pmatrix}$$

contraintes normales

contraintes tangentielles

Tenseur des contraintes

$$\begin{pmatrix} T_x \\ T_y \\ T_z \end{pmatrix} = \begin{pmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{pmatrix} \begin{pmatrix} n_x \\ n_y \\ n_z \end{pmatrix}$$

Vecteur contrainte
(force/unité de
surface)

Tenseur des
contraintes

Normale à la
surface considérée

$$\mathbf{T} = \boldsymbol{\sigma} \cdot \mathbf{n}$$

Conservation de la quantité de mouvement

$$\int_{\Omega} \frac{\partial \rho \mathbf{u}}{\partial t} dV = - \int_{\partial \Omega} \rho \mathbf{u} \mathbf{u} \cdot \mathbf{n} dS + \int_{\Omega} \rho \mathbf{f} dV + \int_{\partial \Omega} \boldsymbol{\sigma} \cdot \mathbf{n} dS$$

Théorème de la divergence:

$$\int_{\Omega} \frac{\partial \rho \mathbf{u}}{\partial t} dV + \int_{\Omega} \nabla \cdot \rho \mathbf{u} \mathbf{u} dV = \int_{\Omega} \rho \mathbf{f} dV + \int_{\Omega} \nabla \cdot \boldsymbol{\sigma} dV$$

$\rho \mathbf{u} \mathbf{u}$: Flux de quantité de mouvement,

↑
produit tensoriel \longrightarrow tenseur de composantes $\rho u_i u_j$

Sa divergence :
(somme sur j)

$$\frac{\partial}{\partial x_j} (\rho u_i u_j) = u_i \frac{\partial \rho u_j}{\partial x_j} + \rho u_j \frac{\partial u_i}{\partial x_j}$$

Divergence des contraintes

$$\nabla \cdot \sigma = \sum_j \frac{\partial \sigma_{ij}}{\partial x_j}$$

Conservation de la quantité de mouvement

Pour un volume élémentaire de fluide :

$$\rho \frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \frac{\partial \rho}{\partial t} + \mathbf{u} \nabla \cdot \rho \mathbf{u} + \rho \mathbf{u} \cdot \nabla \mathbf{u} = \rho \mathbf{f} + \nabla \cdot \sigma$$

$$\rho \frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \underbrace{\left(\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \mathbf{u} \right)}_{= 0} + \rho \mathbf{u} \cdot \nabla \mathbf{u} = \rho \mathbf{f} + \nabla \cdot \sigma$$

Conservation de la masse

$$\rho \left(\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) = \rho \mathbf{f} + \nabla \cdot \sigma$$

$$m \mathbf{a} = \mathbf{F}$$

Accélération d'un élément de fluide

$$m\mathbf{a} = \mathbf{F}$$

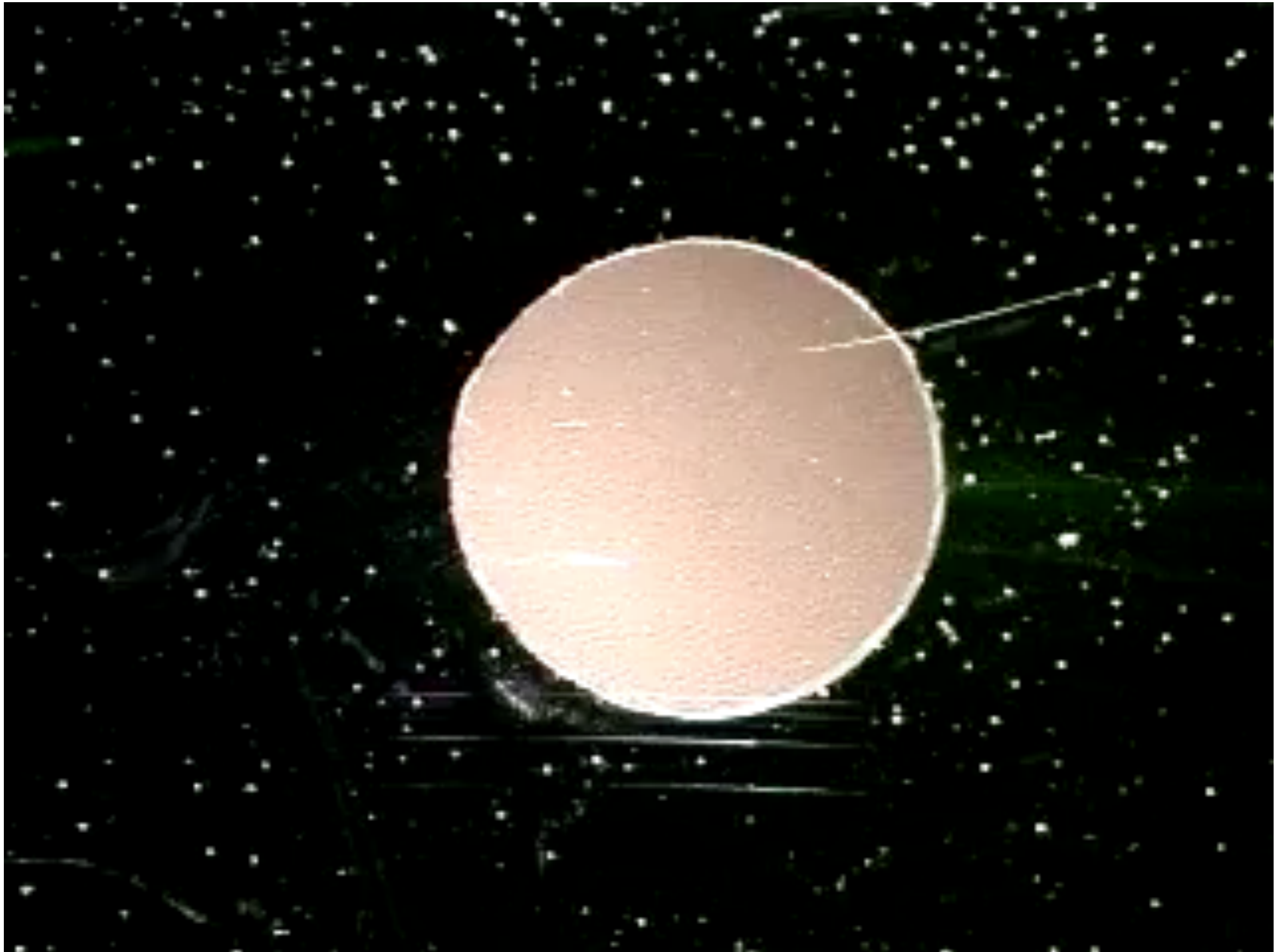
$$\rho \left(\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) = \rho \mathbf{f} + \nabla \cdot \boldsymbol{\sigma}$$

$$\mathbf{a} = \boxed{\frac{\partial \mathbf{u}}{\partial t}} + \boxed{\mathbf{u} \cdot \nabla \mathbf{u}}$$

instationnarité

accélération convective

un écoulement stationnaire où $\mathbf{u} \cdot \nabla \mathbf{u} \neq 0$



Écriture de l'accélération convective

Pour la composante i :

$$u_j \frac{\partial u_i}{\partial x_j} = \sum_{j=1,3} u_j \frac{\partial u_i}{\partial x_j}$$

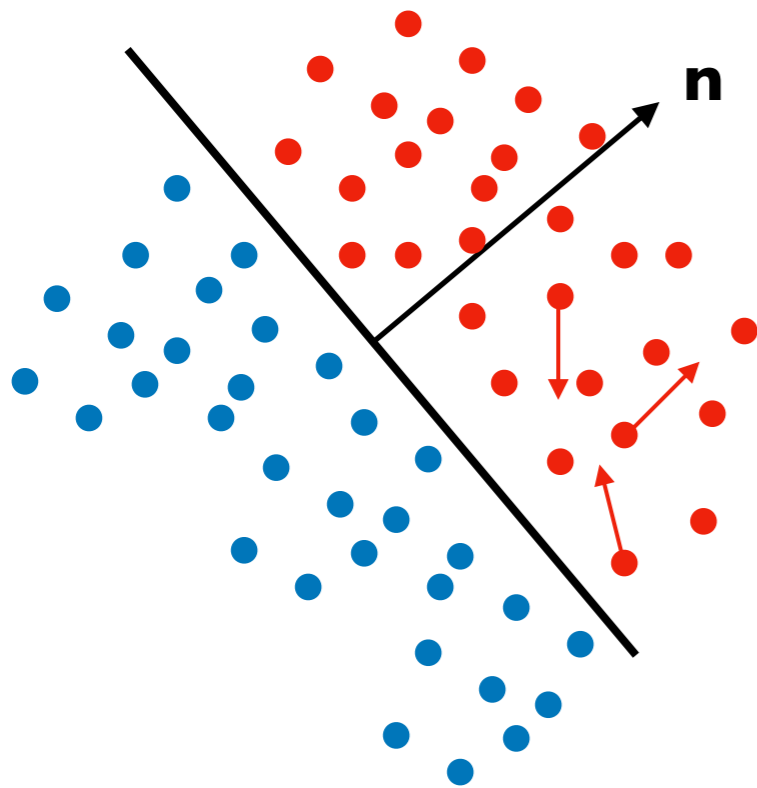
Pour la composante x :

$$u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} + u_z \frac{\partial u_x}{\partial z}$$

Variation spatiale de u_x projetée sur la vitesse (u_x, u_y, u_z)

Les contraintes dans un fluide

Dans un fluide à l'équilibre, sans écoulement macroscopique



La résultante des interactions entre atomes ou molécules est une **pression isotrope**

$$\sigma = \begin{pmatrix} -p & 0 & 0 \\ 0 & -p & 0 \\ 0 & 0 & -p \end{pmatrix}$$

$$\sigma_{ij} = -p \delta_{ij}$$

$$\nabla \cdot \sigma = -\nabla p = \begin{pmatrix} -\frac{\partial p}{\partial x} \\ -\frac{\partial p}{\partial y} \\ -\frac{\partial p}{\partial z} \end{pmatrix}$$

Dans un fluide à l'équilibre, sans écoulement macroscopique

$$\rho \left(\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) = \rho \mathbf{f} + \nabla \cdot \sigma$$

$$0 = \rho \mathbf{g} - \nabla p$$

$$p = p_0 - \rho g z$$