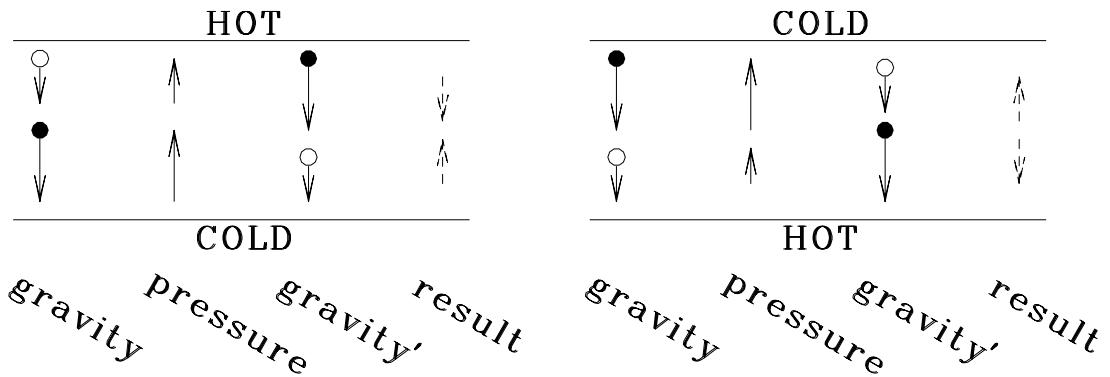


# **Hydrodynamics**

## **Class 9**

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# Rayleigh-Bénard Convection



# Rayleigh-Bénard Convection

Boussinesq Approximation

Calculation and subtraction of the basic state

Non-dimensionalisation

Boundary Conditions

Linear stability analysis

# Boussinesq Approximation

$\mu$  (viscosity  $\sim$  diffusivity of momentum),  $\kappa$  (diffusivity of temperature),  
 $\rho$  (density) constant except in buoyancy force.

Valid for  $T_0 - T_1$  not too large.

$$\begin{aligned}\rho(T) &= \rho_0 [1 - \alpha(T - T_0)] \\ \nabla \cdot \mathbf{U} &= 0\end{aligned}$$

Governing equations:

$$\begin{aligned}\rho_0 [\partial_t + (\mathbf{U} \cdot \nabla)] \mathbf{U} &= \mu \Delta \mathbf{U} - \nabla P - g \rho(T) \hat{\mathbf{e}}_z \\ [\partial_t + (\mathbf{U} \cdot \nabla)] T &= \kappa \Delta T\end{aligned}$$

↑                      ↑                      ↑  
advection        diffusion        buoyancy

Boundary conditions:

$$\begin{aligned}\mathbf{U} &= 0 && \text{at } z = 0, d \\ T &= T_{0,1} && \text{at } z = 0, d\end{aligned}$$

# Calculation and subtraction of base state

Conductive solution:  $(U^*, T^*, P^*)$

Motionless:  $U^* = 0$

uniform temperature gradient:  $T^* = T_0 - (T_0 - T_1) \frac{z}{d}$

density:  $\rho(T^*) = \rho_0 \left[ 1 + \alpha(T_0 - T_1) \frac{z}{d} \right]$

Hydrostatic pressure counterbalances buoyancy force:

$$\begin{aligned} P^* &= -g \int dz \rho(T^*) \\ &= P_0 - g\rho_0 \left[ z + \alpha(T_0 - T_1) \frac{z^2}{2d} \right] \end{aligned}$$

Write:

$$T = T^* + \hat{T} \quad P = P^* + \hat{P}$$

Buoyancy:

$$\begin{aligned}\rho(T^* + \hat{T}) &= \rho_0(1 - \alpha(T^* + \hat{T} - T_0)) \\ &= \rho_0(1 - \alpha(T^* - T_0)) - \rho_0\alpha\hat{T} \\ &= \rho(T^*) - \rho_0\alpha\hat{T} \\ -\nabla P - g\rho(T)\hat{\mathbf{e}}_z &= -\nabla P^* - g\rho(T^*) - \nabla\hat{P} + g\rho_0\alpha\hat{T}\hat{\mathbf{e}}_z \\ &= -\nabla\hat{P} + g\rho_0\alpha\hat{T}\hat{\mathbf{e}}_z\end{aligned}$$

Advection of temperature:

$$\begin{aligned}(U \cdot \nabla)T &= (U \cdot \nabla)T^* + (U \cdot \nabla)\hat{T} \\ &= (U \cdot \nabla) \left( T_0 - (T_0 - T_1) \frac{z}{d} \right) + (U \cdot \nabla)\hat{T} \\ &= -\frac{T_0 - T_1}{d} U \cdot \hat{\mathbf{e}}_z + (U \cdot \nabla)\hat{T}\end{aligned}$$

## Governing equations:

$$\begin{aligned}\rho_0 [\partial_t + (\mathbf{U} \cdot \nabla)] \mathbf{U} &= -\nabla \hat{P} + g \rho_0 \alpha \hat{T} \hat{\mathbf{e}}_z + \mu \Delta \mathbf{U} \\ \nabla \cdot \mathbf{U} &= 0 \\ [\partial_t + (\mathbf{U} \cdot \nabla)] \hat{T} &= \frac{T_0 - T_1}{d} \mathbf{U} \cdot \hat{\mathbf{e}}_z + \kappa \Delta \hat{T}\end{aligned}$$

## Homogeneous boundary conditions:

$$\begin{aligned}\mathbf{U} &= 0 \text{ at } z = 0, d \\ \hat{T} &= 0 \text{ at } z = 0, d\end{aligned}$$

# Non-dimensionalization

Scales:

$$z = d\bar{z}, \quad t = \frac{d^2}{\kappa}\bar{t}, \quad U = \frac{\kappa}{d}\bar{U}, \quad \hat{T} = \frac{\mu\kappa}{d^3 g \rho_0 \alpha} \bar{T}, \quad \hat{P} = \frac{\mu\kappa}{d^2} \bar{P}$$

Equations :

$$\begin{aligned} \frac{\kappa^2 \rho_0}{d^3} [\partial_{\bar{t}} + (\bar{U} \cdot \bar{\nabla})] \bar{U} &= -\frac{\mu\kappa}{d^3} \bar{\nabla} \bar{P} + \frac{\mu\kappa}{d^3} \bar{T} \hat{\mathbf{e}}_z + \frac{\mu\kappa}{d^3} \bar{\Delta} \bar{U} \\ \frac{\kappa}{d^2} \bar{\nabla} \cdot \bar{U} &= 0 \\ \frac{\mu\kappa^2}{d^5 g \rho_0 \alpha} [\partial_{\bar{t}} + (\bar{U} \cdot \bar{\nabla})] \bar{T} &= \frac{\kappa}{d} \frac{T_0 - T_1}{d} \bar{U} \cdot \hat{\mathbf{e}}_z + \frac{\mu\kappa^2}{d^5 g \rho_0 \alpha} \bar{\Delta} \bar{T} \end{aligned}$$

Dividing through, we obtain:

$$\begin{aligned} [\partial_{\bar{t}} + (\bar{U} \cdot \bar{\nabla})] \bar{U} &= \frac{\mu}{\rho_0 \kappa} [-\bar{\nabla} \bar{P} + \bar{T} \hat{\mathbf{e}}_z + \bar{\Delta} \bar{U}] \\ [\partial_{\bar{t}} + (\bar{U} \cdot \bar{\nabla})] \bar{T} &= \frac{(T_0 - T_1) d^3 g \rho_0 \alpha}{\kappa \mu} \bar{U} \cdot \hat{\mathbf{e}}_z + \bar{\Delta} \bar{T} \end{aligned}$$

## Non-dimensional parameters:

the Prandtl number:

$$Pr \equiv \frac{\mu}{\rho_0 \kappa}$$

momentum diffusivity / thermal diffusivity

the Rayleigh number:

$$Ra \equiv \frac{(T_0 - T_1) d^3 g \rho_0 \alpha}{\kappa \mu}$$

non-dimensional measure of thermal gradient

# Boundary conditions

Horizontal direction: periodicity  $2\pi/q$

Vertical direction: at  $z = 0, 1$

$$T = 0|_{z=0,1} \quad \text{perfectly conducting plates}$$

$$w = 0|_{z=0,1} \quad \text{impenetrable plates}$$

Rigid boundaries at  $z = 0, 1$ :

$$u|_{z=0,1} = v|_{z=0,1} = 0 \quad \text{zero tangential velocity}$$

Incompressibility

$$\partial_x u + \partial_y v + \partial_z w = 0$$

$$\implies \partial_z w = -(\partial_x u + \partial_y v)$$

$$u|_{z=0,1} = v|_{z=0,1} = 0 \implies \partial_x u|_{z=0,1} = \partial_y v|_{z=0,1} = 0$$

$$\implies \partial_z w|_{z=0,1} = 0$$

Free surfaces at  $z = 0, 1$  to simplify calculations:

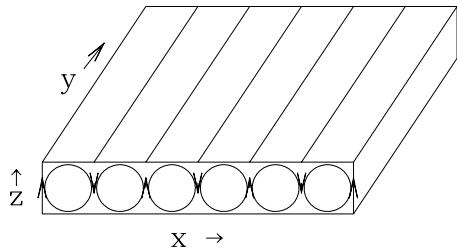
$$[\partial_z u + \partial_x w]_{z=0,1} = [\partial_z v + \partial_y w]_{z=0,1} = 0$$

zero tangential stress

$$\begin{aligned} w|_{z=0,1} = 0 &\implies \partial_x w|_{z=0,1} = \partial_y w|_{z=0,1} = 0 \\ &\implies \partial_z u|_{z=0,1} = \partial_z v|_{z=0,1} = 0 \\ &\implies \partial_x \partial_z u|_{z=0,1} = \partial_y \partial_z v|_{z=0,1} = 0 \\ &\implies \partial_{zz} w|_{z=0,1} = -\partial_z (\partial_x u + \partial_y v)|_{z=0,1} = 0 \end{aligned}$$

Not realistic, but allows trigonometric functions  $\sin(k\pi z)$

## Two-dimensional case



$$U = \nabla \times \psi \hat{e}_y \implies \begin{cases} u = -\partial_z \psi \\ w = \partial_x \psi \end{cases} \implies \nabla \cdot U = 0$$

No-penetration boundary condition:

Horizontal flux:  $0 = w = \partial_x \psi \implies \begin{cases} \psi = \psi_1 & \text{at } z = 1 \\ \psi = \psi_0 & \text{at } z = 0 \end{cases}$

$$\int_{z=0}^1 dz \ u(x, z) = - \int_{z=0}^1 dz \ \partial_z \psi(x, z) = - [\psi(x, z)]_{z=0}^1 = \psi_0 - \psi_1$$

Arbitrary constant  $\implies \psi_0 = 0$

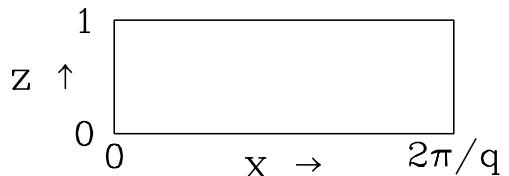
Zero flux  $\implies \psi_1 = 0$

Stress-free:  $0 = \partial_z u = -\partial_{zz}^2 \psi$

Rigid:  $0 = u = \partial_z \psi \quad \text{at } z = 0, 1$

$$T = \psi = \partial_{zz} \psi = 0$$

Two-dimensional case



$$T = \psi = \partial_{zz} \psi = 0$$

Temperature equation:

$$\partial_t T + \color{red}{U \cdot \nabla T} = Ra U \cdot \hat{e}_z + \Delta T$$

$$\begin{aligned}\color{red}{U \cdot \nabla T} &= u \partial_x T + w \partial_z T \\ &= -\partial_z \psi \partial_x T + \partial_x \psi \partial_z T \equiv \color{red}{J[\psi, T]}\end{aligned}$$

$$\partial_t T + \color{red}{J[\psi, T]} = Ra \partial_x \psi + \Delta T$$

## Velocity equation

$$\partial_t U + (\mathbf{U} \cdot \nabla) U = Pr [-\nabla P + T \hat{\mathbf{e}}_z + \Delta U]$$

Take  $\hat{\mathbf{e}}_y \cdot \nabla \times$ :

$$\hat{\mathbf{e}}_y \cdot \nabla \times \partial_t U = \hat{\mathbf{e}}_y \cdot \nabla \times \nabla \times \partial_t \psi \hat{\mathbf{e}}_y = -\partial_t \Delta \psi$$

$$\hat{\mathbf{e}}_y \cdot \nabla \times \nabla P = 0$$

$$\hat{\mathbf{e}}_y \cdot \nabla \times T \hat{\mathbf{e}}_z = -\partial_x T$$

$$\hat{\mathbf{e}}_y \cdot \nabla \times \Delta U = \hat{\mathbf{e}}_y \cdot \nabla \times \Delta \nabla \times \psi \hat{\mathbf{e}}_y = -\Delta^2 \psi$$

$$\partial_t \Delta \psi - \hat{\mathbf{e}}_y \cdot \nabla \times (\mathbf{U} \cdot \nabla) U = Pr [\partial_x T + \Delta^2 \psi]$$

$$\nabla \times \nabla \times f = \nabla \nabla \cdot f - \Delta f$$

$$\hat{e}_y \cdot \nabla \times (U \cdot \nabla) U = \partial_z(U \cdot \nabla)u - \partial_x(U \cdot \nabla)w$$

$$\begin{aligned}
&= \partial_z(u\partial_x u + w\partial_z u) - \partial_x(u\partial_x w + w\partial_z w) \\
&= \partial_z u \partial_x u + \partial_z w \partial_z u - \partial_x u \partial_x w - \partial_x w \partial_z w \\
&+ u \partial_{xz} u + w \partial_{zz} u - u \partial_{xx} w - w \partial_{xz} w \\
&= \partial_z u (\partial_x u + \partial_z w) - \partial_x w (\partial_x u + \partial_z w) \\
&+ u \partial_x (\partial_z u - \partial_x w) + w \partial_z (\partial_z u - \partial_x w) \\
&= (-\partial_z \psi) \partial_x (-\partial_{zz} \psi - \partial_{xx} \psi) \\
&+ (\partial_x \psi) \partial_z (-\partial_{zz} \psi - \partial_{xx} \psi) \\
&= (\partial_z \psi) \partial_x (\Delta \psi) - (\partial_x \psi) \partial_z (\Delta \psi)
\end{aligned}$$

$$= -J[\psi, \Delta \psi]$$

$$\partial_t \Delta \psi + J[\psi, \Delta \psi] = Pr[\partial_x T + \Delta^2 \psi]$$

# Linear stability analysis

Linearized equations:

$$\begin{aligned}\partial_t \Delta \psi &= Pr[\partial_x T + \Delta^2 \psi] \\ \partial_t T &= Ra \partial_x \psi + \Delta T\end{aligned}$$

Solutions:

$$\begin{array}{lcl} \psi(x, z, t) & = & \hat{\psi} \sin qx \sin k\pi z e^{\lambda t} \quad q \in \mathcal{R}, \quad k \in \mathcal{Z}^+, \quad \lambda \in \mathcal{C} \\ T(x, z, t) & = & \hat{T} \cos qx \sin k\pi z e^{\lambda t} \\ \uparrow & & \uparrow \\ \text{functions} & & \text{scalars} \end{array} \qquad \gamma^2 \equiv q^2 + (k\pi)^2$$

$$\begin{aligned}-\lambda \gamma^2 \hat{\psi} &= Pr[-q \hat{T} + \gamma^4 \hat{\psi}] \\ \lambda \hat{T} &= Ra q \hat{\psi} - \gamma^2 \hat{T}\end{aligned}$$

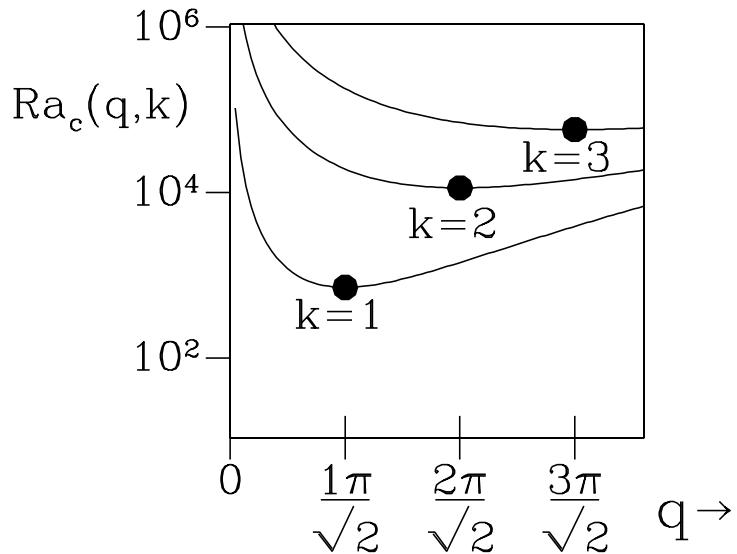
$$\lambda \begin{bmatrix} \hat{\psi} \\ \hat{T} \end{bmatrix} = \begin{bmatrix} -Pr \gamma^2 & Pr q/\gamma^2 \\ Ra q & -\gamma^2 \end{bmatrix} \begin{bmatrix} \hat{\psi} \\ \hat{T} \end{bmatrix}$$

Seek:  $\lambda = 0$

$$Pr \gamma^4 - Pr Ra \frac{q^2}{\gamma^2} = 0$$

$$Ra = \frac{\gamma^6}{q^2} = \frac{(q^2 + (k\pi)^2)^3}{q^2} \equiv Ra_c(q, k)$$

## Convection Threshold



Conductive state unstable at  $(q, k)$  for  $Ra > Ra_c(q, k)$

Conductive state stable if

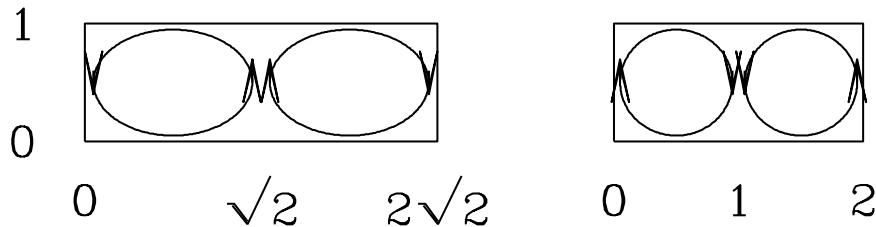
$$\min_{\substack{q \in \mathcal{R} \\ k \in \mathcal{Z}^+}} Ra < Ra_c(q, k)$$

$$\begin{aligned} 0 &= \frac{\partial Ra_c(q, k)}{\partial q} = \frac{q^2 3(q^2 + (k\pi)^2)^2 2q - 2q(q^2 + (k\pi)^2)^3}{q^4} \\ &= \frac{2(q^2 + (k\pi)^2)^2}{q^3} (3q^2 - (q^2 + (k\pi)^2)) \\ \implies q^2 &= \frac{(k\pi)^2}{2} \end{aligned}$$

$$Ra_c \left( q = \frac{k\pi}{\sqrt{2}}, k \right) = \frac{(k\pi)^2/2 + (k\pi)^2)^3}{(k\pi)^2/2} = \frac{27}{4}(k\pi)^4$$

$$Ra_c \equiv Ra_c \left( q = \frac{\pi}{\sqrt{2}}, k = 1 \right) = \frac{27}{4}(\pi)^4 = 657.5$$

# Rigid Boundaries



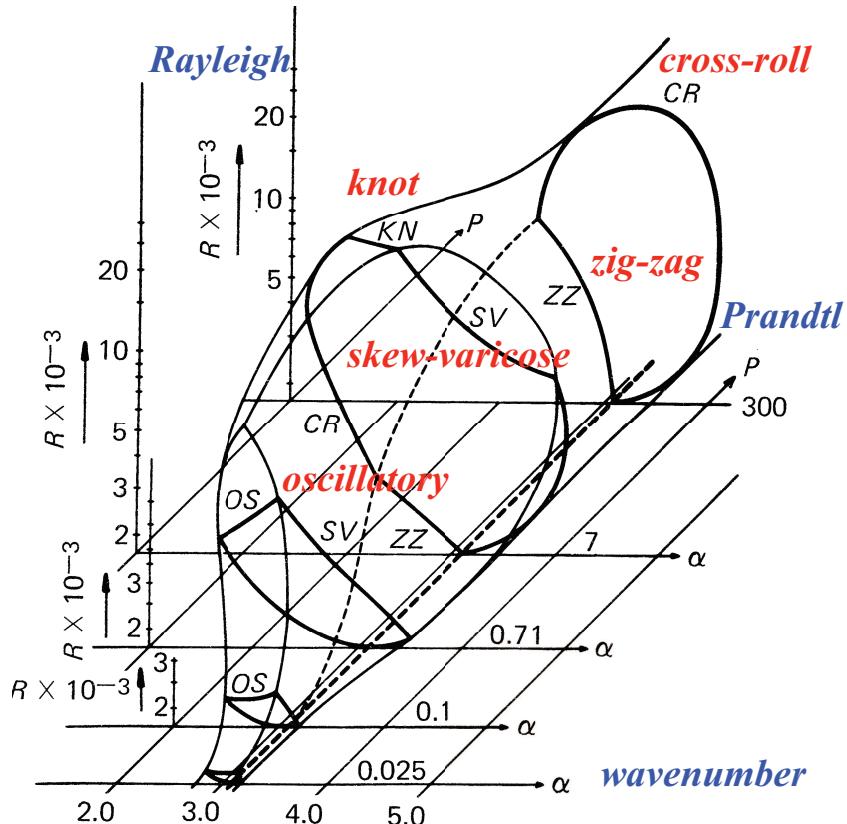
Calculation follows the same principle, but more complicated.

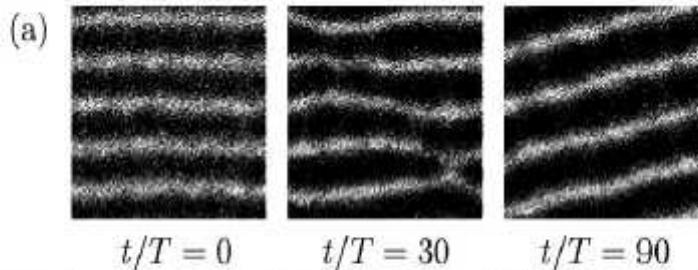
Boundaries damp perturbations  $\Rightarrow$  higher threshold

$q_c \downarrow \Rightarrow \ell_c = \pi/q_c \uparrow \Rightarrow$  rolls  $\approx$  circular

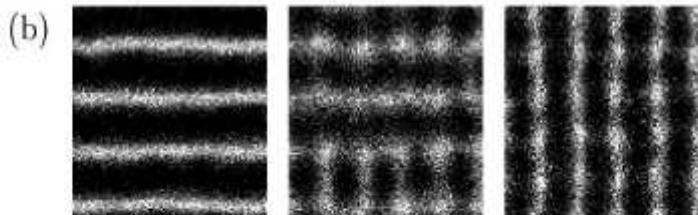
	$Ra_c$	$q_c$	$\ell_c$
stress-free boundaries	$\frac{27}{4}\pi^4 = 657.5$	$\frac{\pi}{\sqrt{2}}$	1.4
rigid boundaries	$\approx 1700$	$\approx \pi$	$\approx 1$

# Instabilities of straight rolls: “Busse balloon”

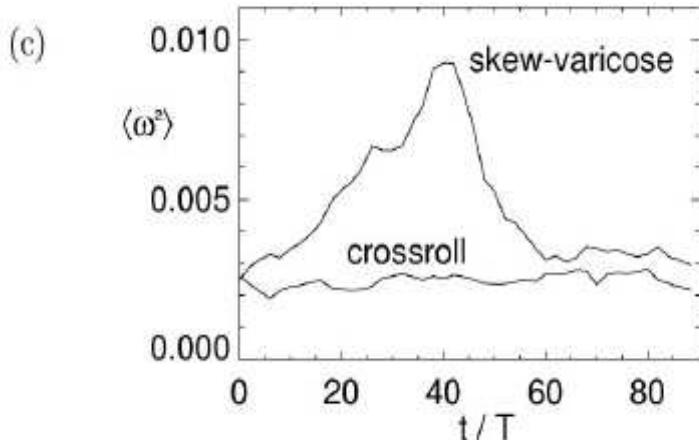




skew-varicose instability



cross-roll instability

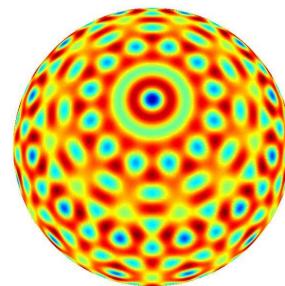


Continuum-type stability balloon in oscillated granulated layers, J. de Bruyn, C. Bizon, M.D. Shattuck, D. Goldman, J.B. Swift & H.L. Swinney, Phys. Rev. Lett. 1998.

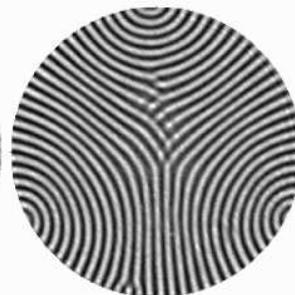
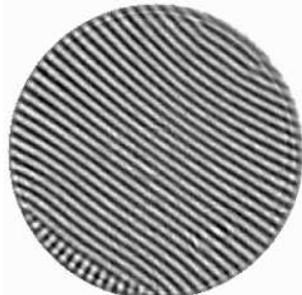
# Complex spatial patterns in convection



Experimental spiral defect chaos  
Egolf, Melnikov, Pesche, Ecke  
Nature **404** (2000)

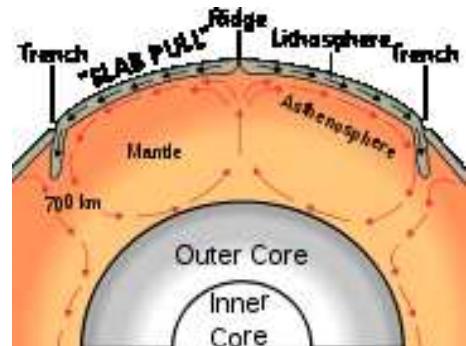
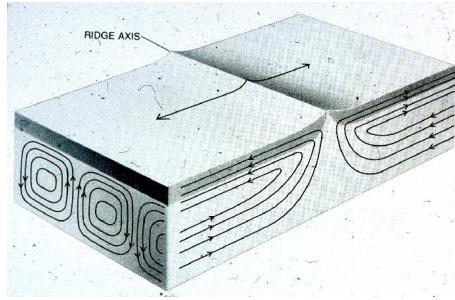


Spherical harmonic  $\ell = 28$   
P. Matthews  
Phys. Rev. E **67** (2003)

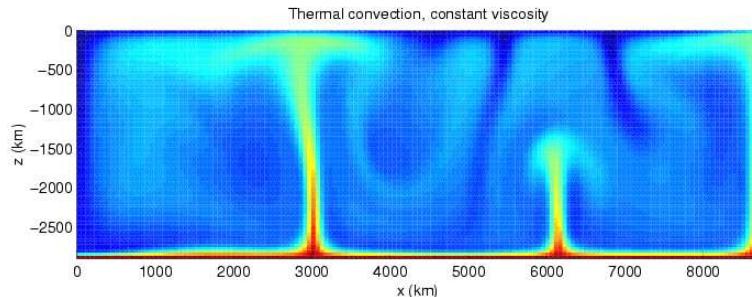


Convection in cylindrical geometry. Bajaj et al. J. Stat. Mech. (2006)

# Geophysics

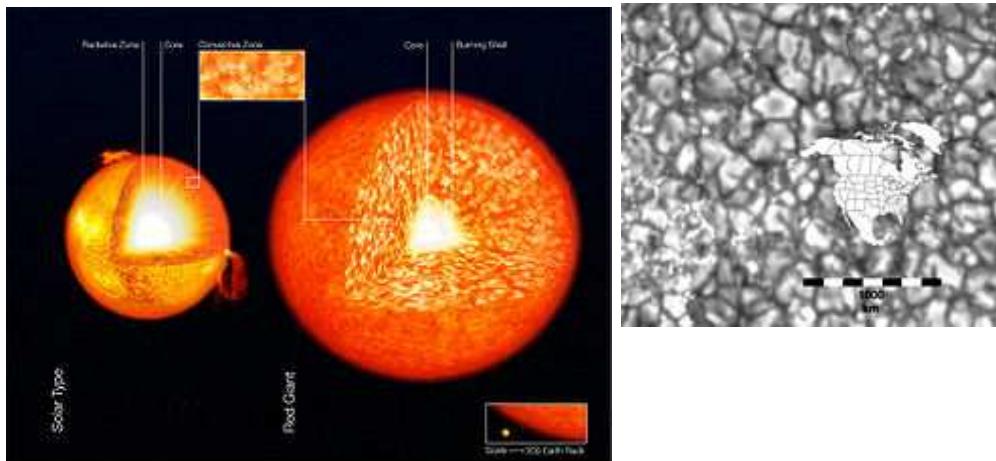


## Convection and plate tectonics



Numerical simulation of convection in earth's mantle, showing plumes and thin boundary layers. By H. Schmeling, Wikimedia Commons.

# Convection cells in the sun

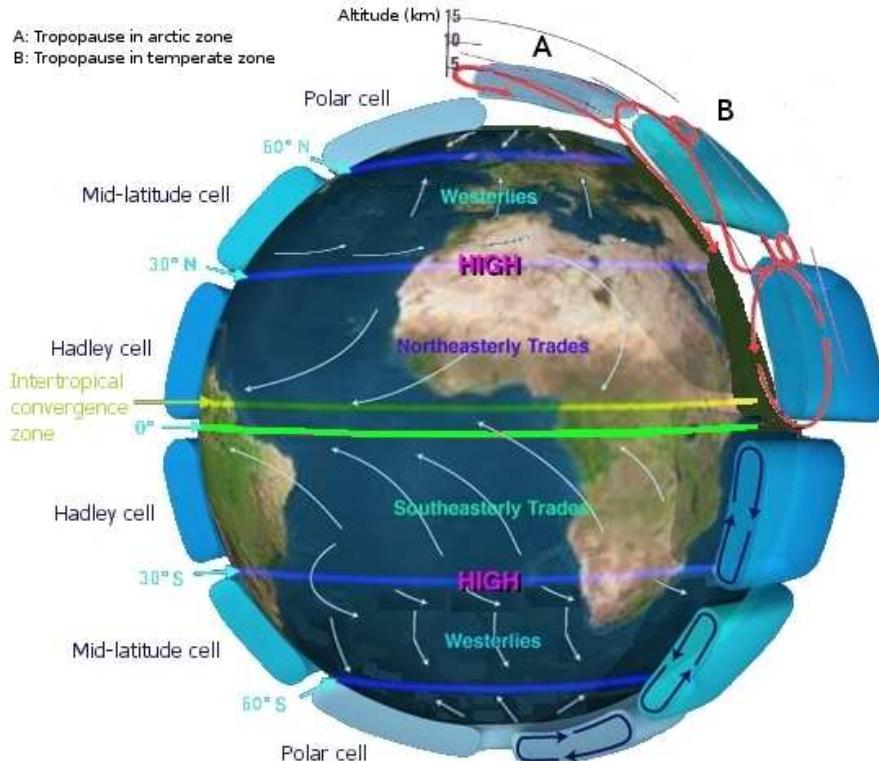


The Structure of Stars

ESO Press Photo 29/07 (5 July 2007)



# Atmospheric circulation



Latitudinal circulation  $\Rightarrow$  Hadley cell, mid-latitude cell, polar cell

## Solutal Convection

Mixture of two species whose density depends on the relative concentration:

$$\rho(C) = \rho_0 [1 - \beta(C - C_0)]$$

Impose concentration  $C_0$  below and  $C_1$  above. Base state has uniform concentration gradient  $C^*$ . Define deviation  $\hat{C}$  from base state  $C^*$ :

$$C^* = C_0 - (C_0 - C_1) \frac{z}{d} \quad C = C^* + \hat{C}$$

Governing equations

$$\begin{aligned}\rho_0 [\partial_t + (U \cdot \nabla)] U &= -\nabla \hat{P} + g\rho_0 \beta \hat{C} \hat{\mathbf{e}}_z + \mu \Delta U \\ \nabla \cdot U &= 0 \\ [\partial_t + (U \cdot \nabla)] \hat{C} &= \frac{C_0 - C_1}{d} U \cdot \hat{\mathbf{e}}_z + \kappa_C \Delta \hat{C}\end{aligned}$$

lead to solutal Rayleigh number and Schmidt number:

$$\begin{aligned}Ra_C \equiv \frac{(C_0 - C_1)d^3 g \beta}{\kappa_C \nu} &\quad \text{non-dimensional measure of concentration gradient} \\ Sc \equiv \frac{\nu}{\kappa_C} &\quad \text{momentum diffusivity / mass diffusivity}\end{aligned}$$

The convection in the earth's mantle is solutal.

# Thermosolutal Convection

$$\rho(T, C) = \rho_0 [1 - \alpha(T - T_0) + \beta(C - C_0)]$$

$$\partial_t \Delta \psi + J[\psi, \Delta \psi] = Pr [\partial_x T + \partial_x C + \Delta^2 \psi]$$

$$\partial_t T + J[\psi, T] = Ra \partial_x \psi + \Delta T$$

$$\partial_t C + J[\psi, C] = Ra_C \partial_x \psi + \frac{Pr}{Sc} \Delta C$$

Linear Stability Analysis: set  $J[., .] = 0$  and substitute

$$\psi(x, z, t) = \hat{\psi} \sin qx \sin k\pi z e^{\lambda t} \quad q \in \mathcal{R}, \quad k \in \mathcal{Z}^+, \quad \lambda \in \mathcal{C}$$

$$C(x, z, t) = \hat{C} \cos qx \sin k\pi z e^{\lambda t}$$

$$T(x, z, t) = \hat{T} \cos qx \sin k\pi z e^{\lambda t}$$

↑

↑

functions

scalars

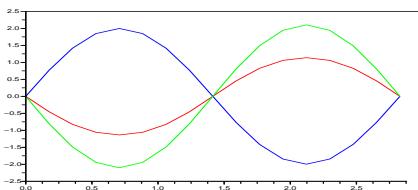
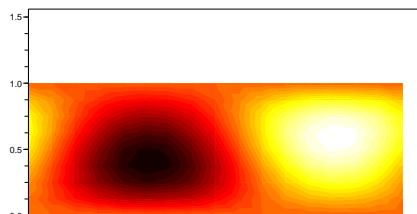
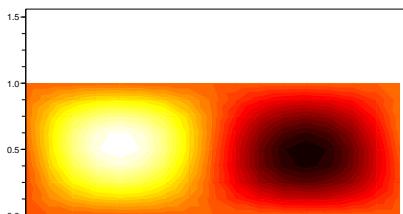
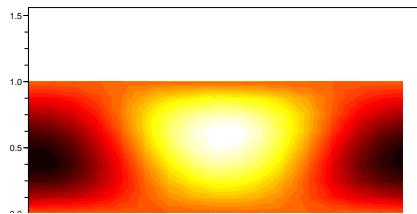
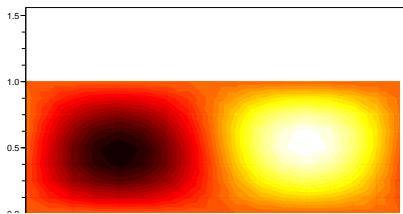
$$\gamma^2 \equiv q^2 + (k\pi)^2$$

$$-\lambda \gamma^2 \hat{\psi} = -q Pr [\hat{T} + \hat{C} + \gamma^4 \hat{\psi}]$$

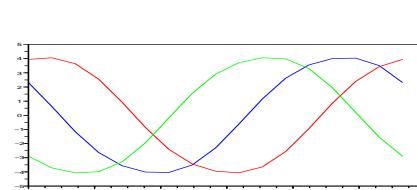
$$\lambda \hat{T} = Ra q \hat{\psi} - \gamma^2 \hat{T}$$

$$\lambda \hat{C} = Ra_C q \hat{\psi} - \frac{Pr}{Sc} \gamma^2 \hat{C}$$

If thermal and solutal convection oppose each other,  $\lambda$  can be complex  
⇒ time-dependent states, like traveling and standing waves:



Standing waves



Travelling waves

# Marangoni Convection: Mechanism

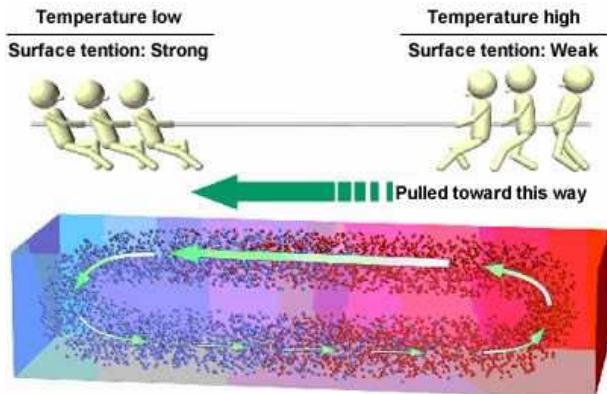
Surface tension varies with temperature. Define Marangoni number.

$$\sigma(T) = \sigma_0[1 + \gamma(T - T_0)] \quad Ma \equiv \frac{(T_0 - T_1)d\sigma_0\gamma}{\kappa\mu}$$

Marangoni boundary condition at upper surface:

$$\frac{\partial u}{\partial z} = -\frac{\partial \sigma}{\partial x} = -\gamma \frac{\partial T}{\partial x} \text{ and } w = 0$$

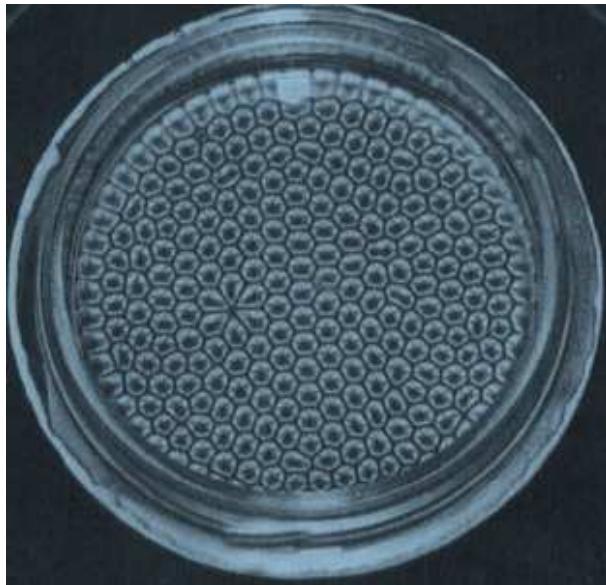
Along free surface, fluid moves towards region with lower surface tension.



Under region with high (low) surface tension, fluid rises (falls).

## Marangoni Convection: Pattern

Experimental visualization of Marangoni convection by L. Koschmieder:



Hexagonal cells are formed in Marangoni convection because of asymmetry between top and bottom (theory of dynamical systems and pattern formation).

# Marangoni Convection: History

Henri Bénard, “Les tourbillons cellulaires dans une nappe liquide transportant de la chaleur par convection en régime permanent”, Annales de Chimie et de Physique, **23** 62–144 (1901).

Bénard (1901) and Rayleigh (1916) thought that the motion was due to  $\rho(T)$ . Block (1956) and Pearson (1958) showed that Bénard’s cells were due to  $\sigma(T)$ . Bénard’s experiment showed hexagonal cells. In fact, buoyancy-driven ( $\rho(T)$ ) convection usually forms rolls, not hexagons. But we still call buoyancy-driven convection “Rayleigh-Bénard convection”, even though Bénard did not see it.

