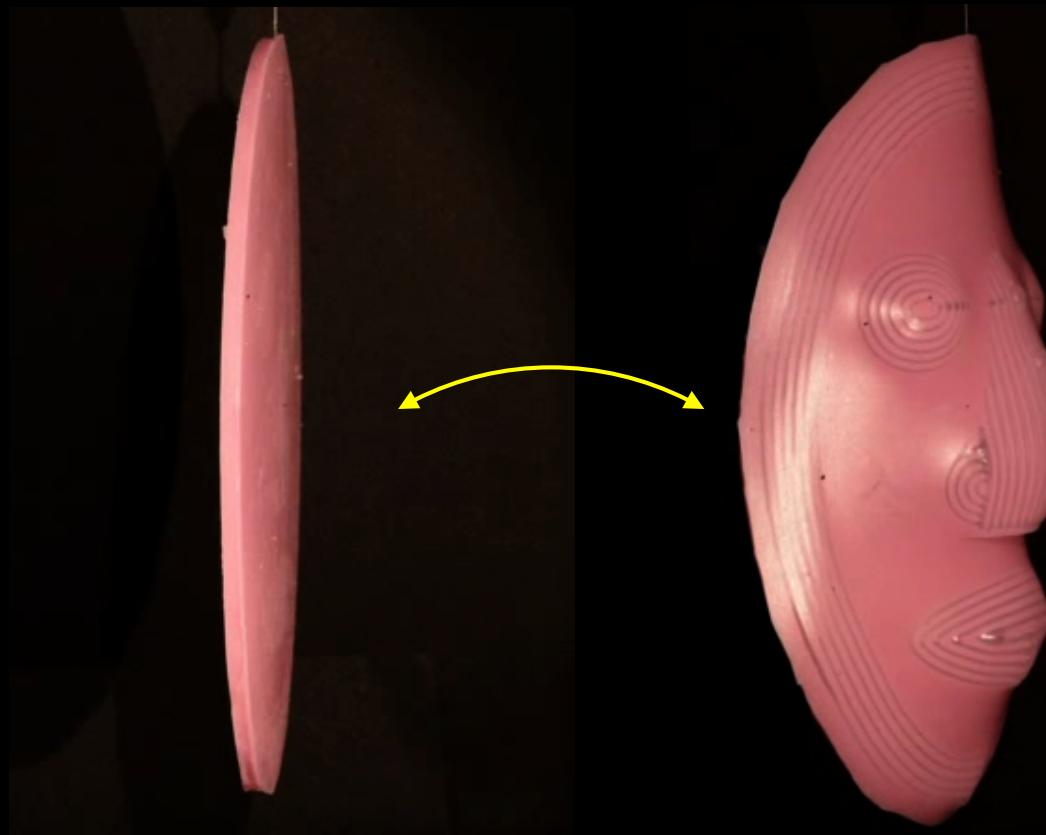


# Mises en forme

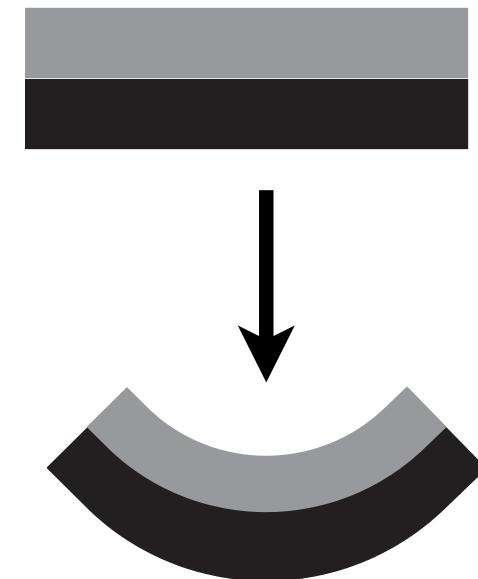
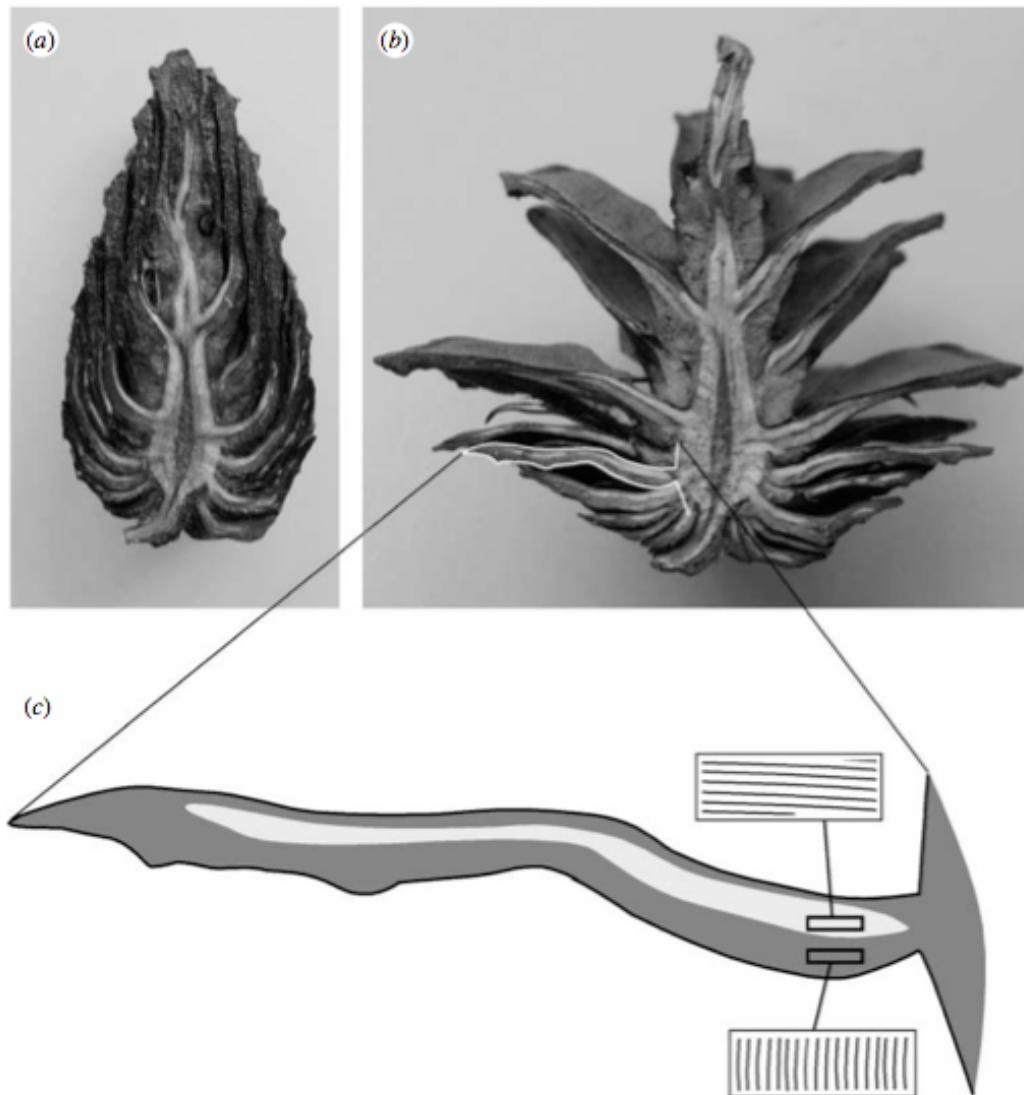


José Bico, MecaWet Group PMMH ESPCI

# Drying pine cones



# Bilayer scales

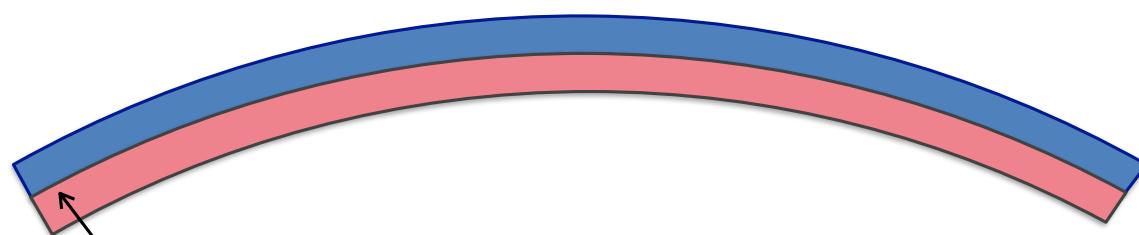
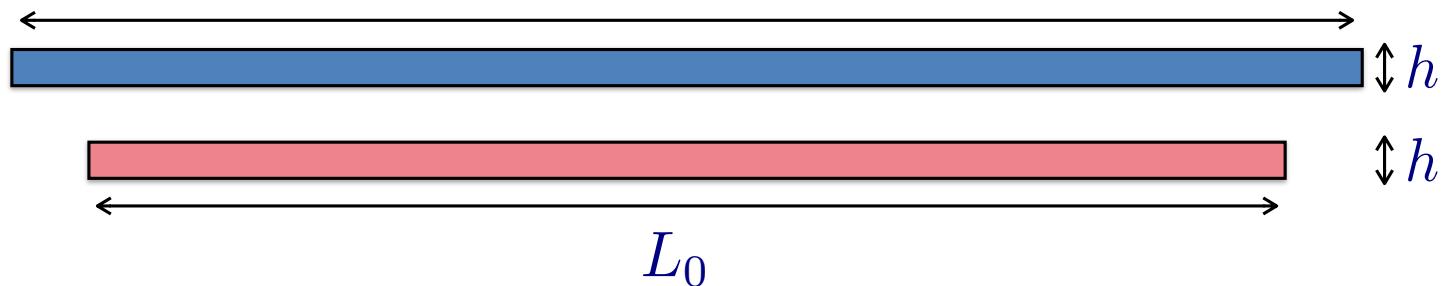


Dowson & Vincent, *Nature* (1997)

Reyssat & Mahadevan, *J.R.Soc Interface* (2008)

# Bilayers

$$(1 + \alpha)L_0$$



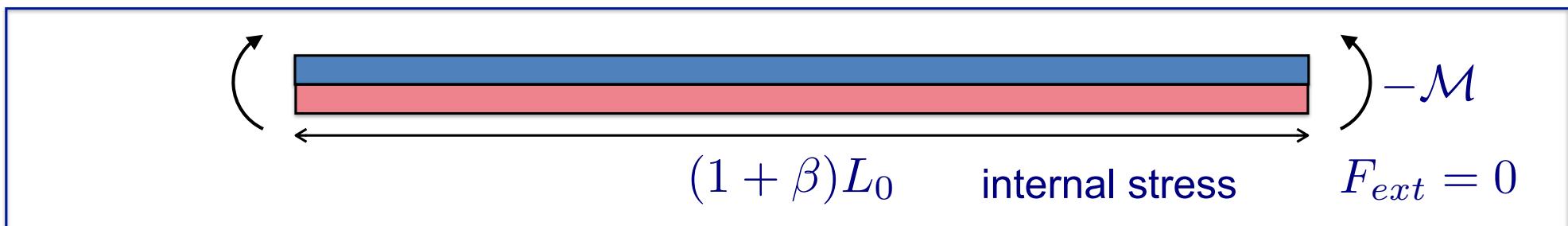
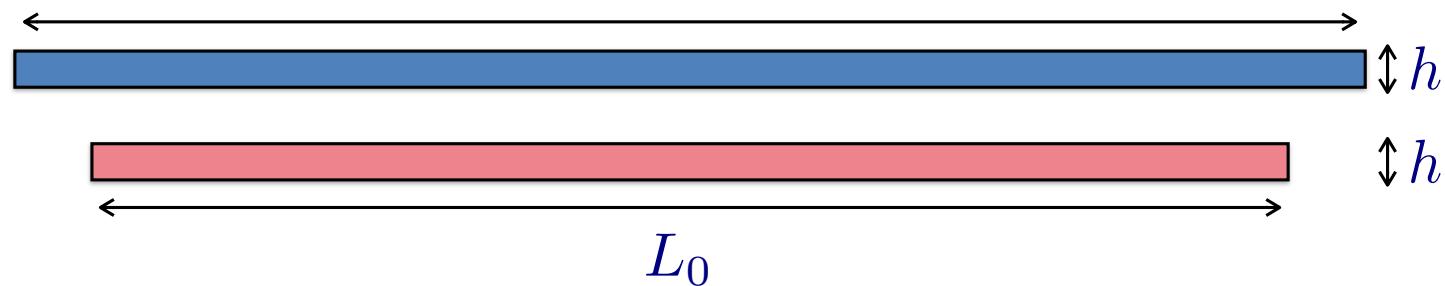
$R ?$

$$F_{ext} = 0$$

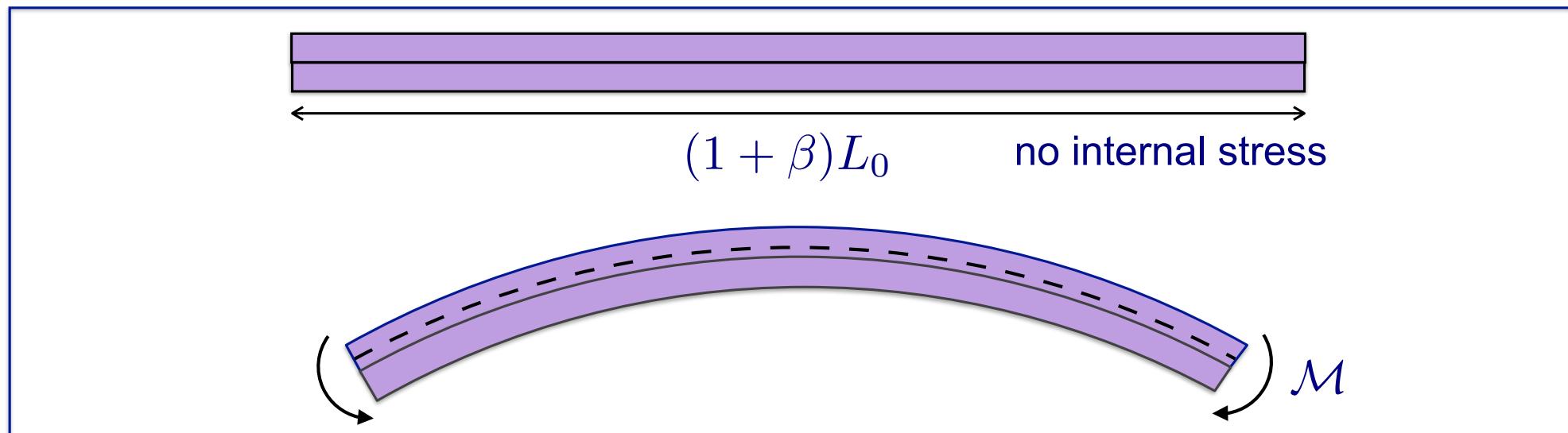
$$\mathcal{M}_{ext} = 0$$

# Superposition

$$(1 + \alpha)L_0$$

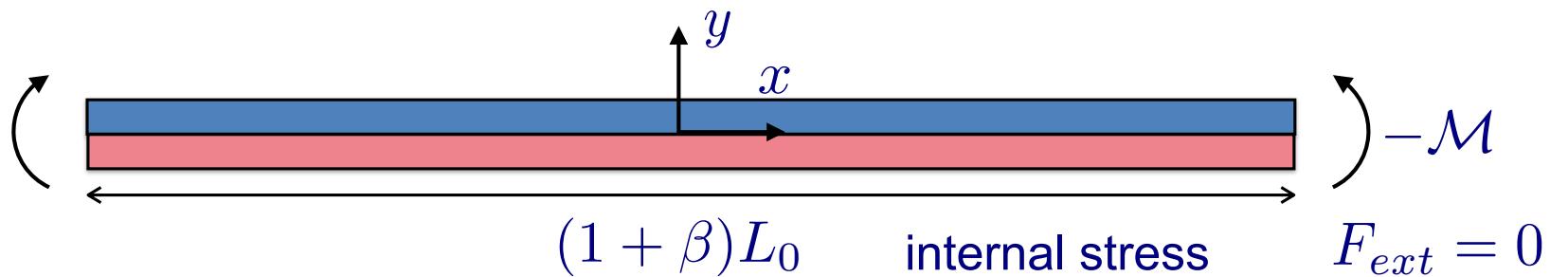
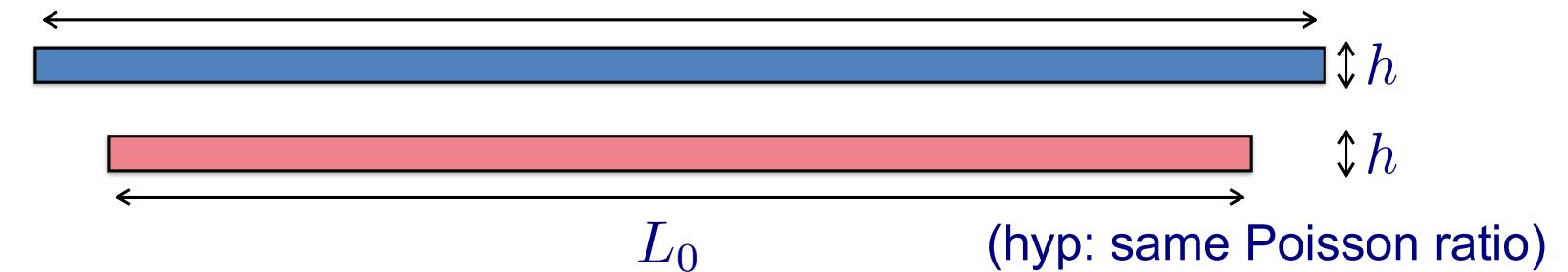


+



# Superposition

$$(1 + \alpha)L_0$$



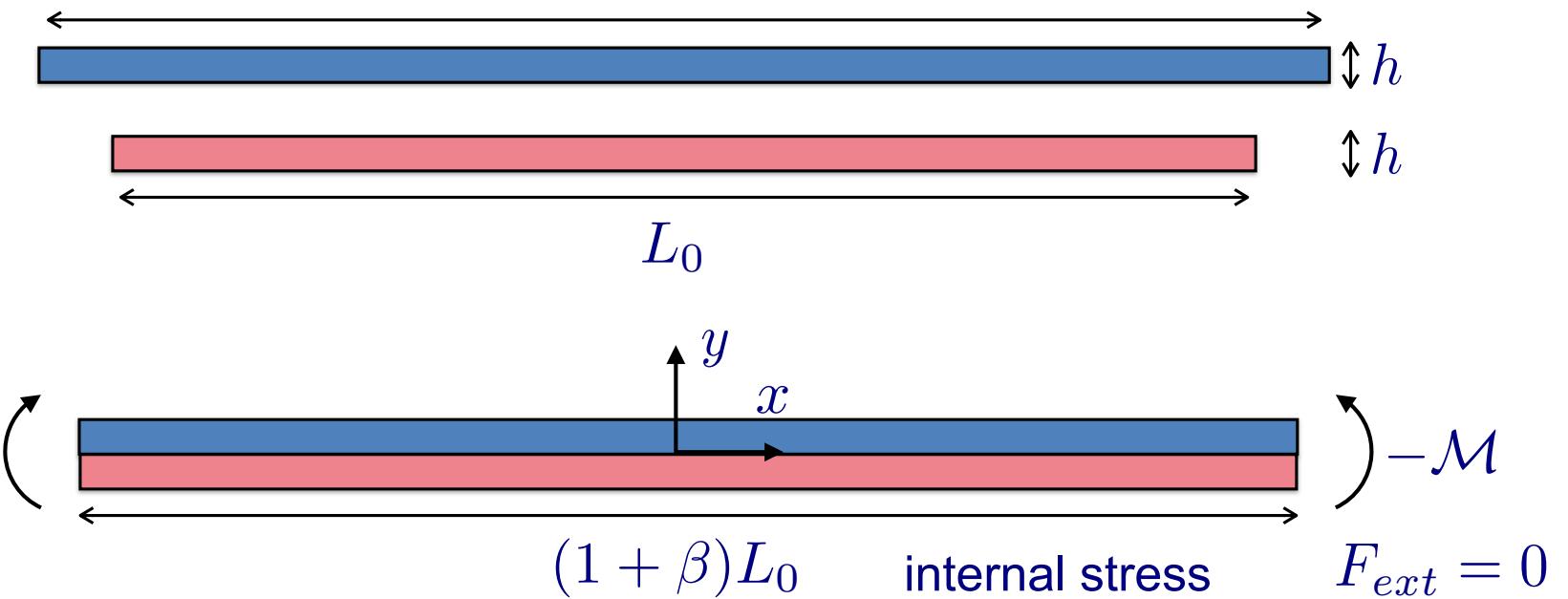
$$-h \leq y \leq 0 \quad \varepsilon_{xx} = \beta \quad \sigma_{xx} = \beta E$$

$$0 \leq y \leq h \quad \varepsilon_{xx} = \frac{(1 + \beta)L_0 - (1 + \alpha)L_0}{(1 + \beta)L_0} \simeq (\beta - \alpha)$$

$$\sigma_{xx} = (\beta - \alpha)E$$

# Superposition

$$(1 + \alpha)L_0$$



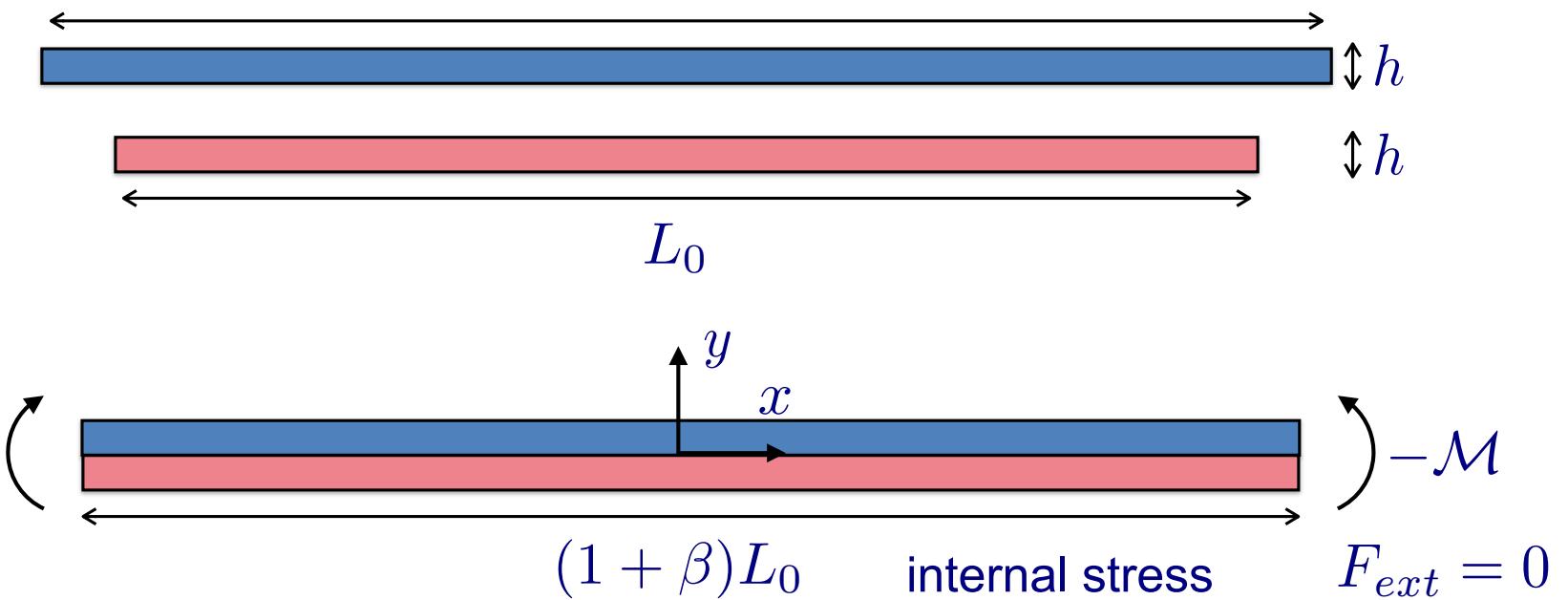
$$F_{ext} = 0 \Rightarrow \int_{-h}^h \sigma_{xx}(y) dy = 0$$

$$E(\beta - \alpha)h + E\beta h = 0$$

$$\boxed{\beta = \alpha/2}$$

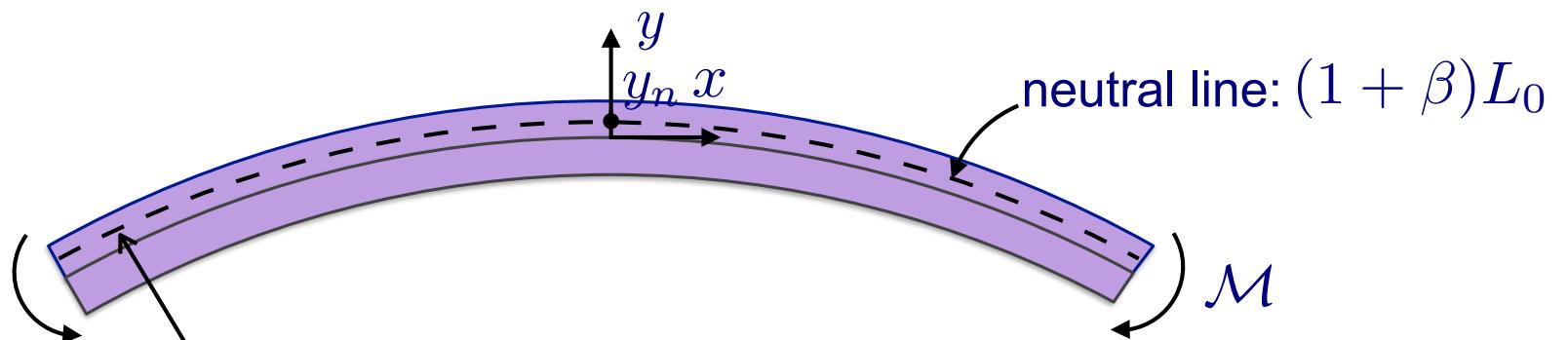
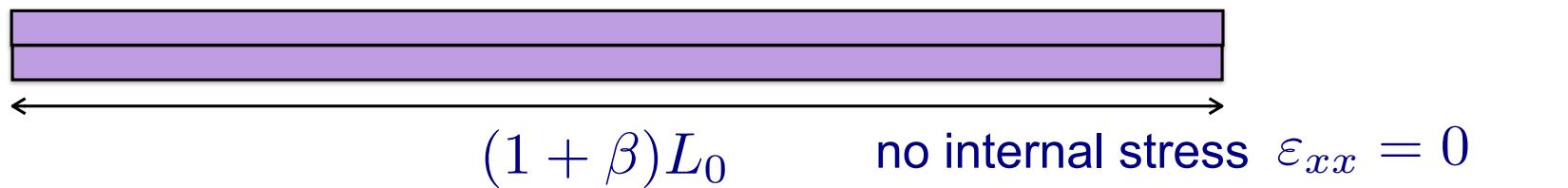
# Superposition

$$(1 + \alpha)L_0$$



$$\mathcal{M}/\ell = \int_{-h}^h \sigma_{xx}(y)y dy = \int_{-h}^0 -\frac{E\alpha}{2}y dy + \int_0^h \frac{E\alpha}{2}y dy = \boxed{\frac{E\alpha h^2}{2}}$$

# Superposition

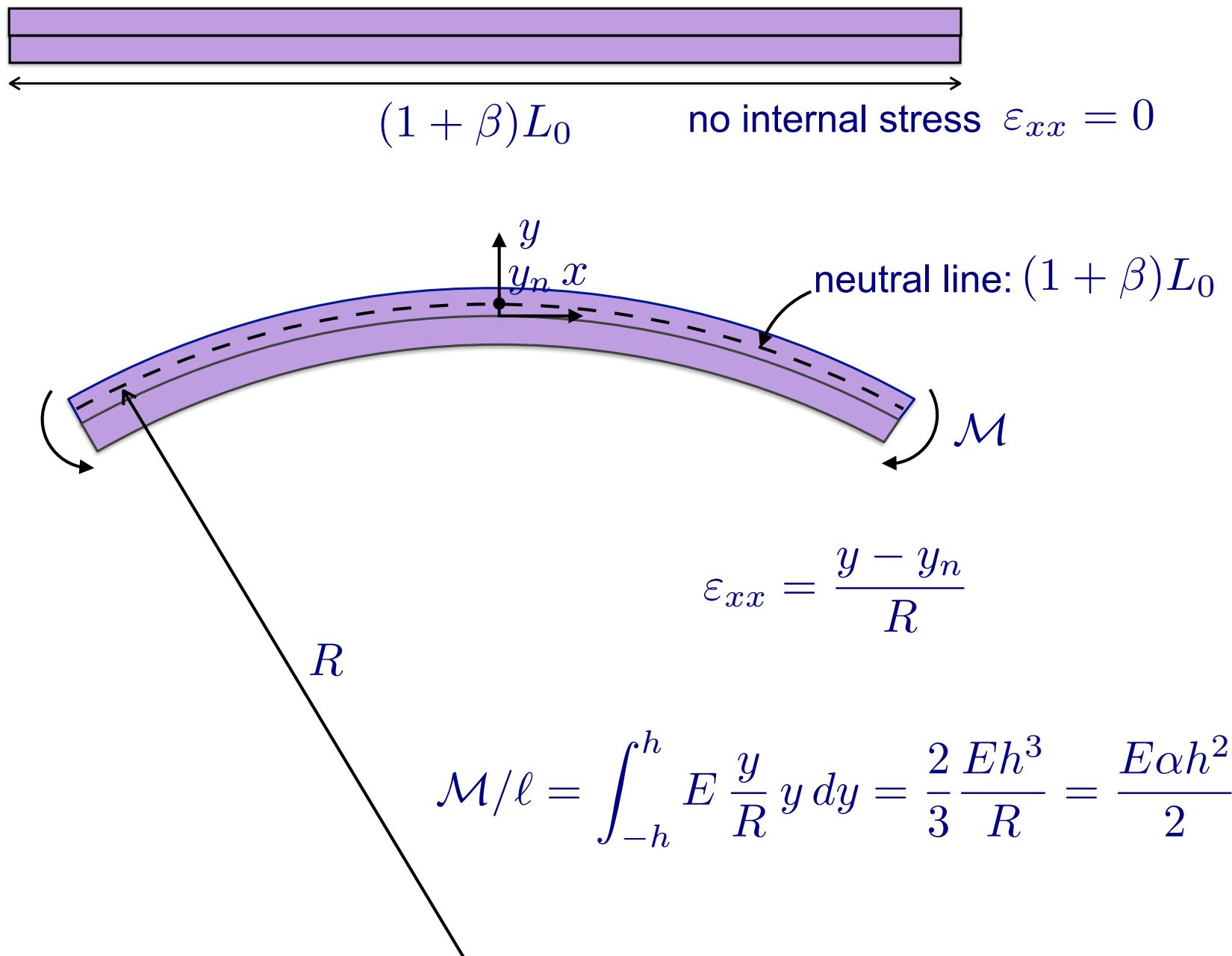


$$\varepsilon_{xx} = \frac{y - y_n}{R}$$

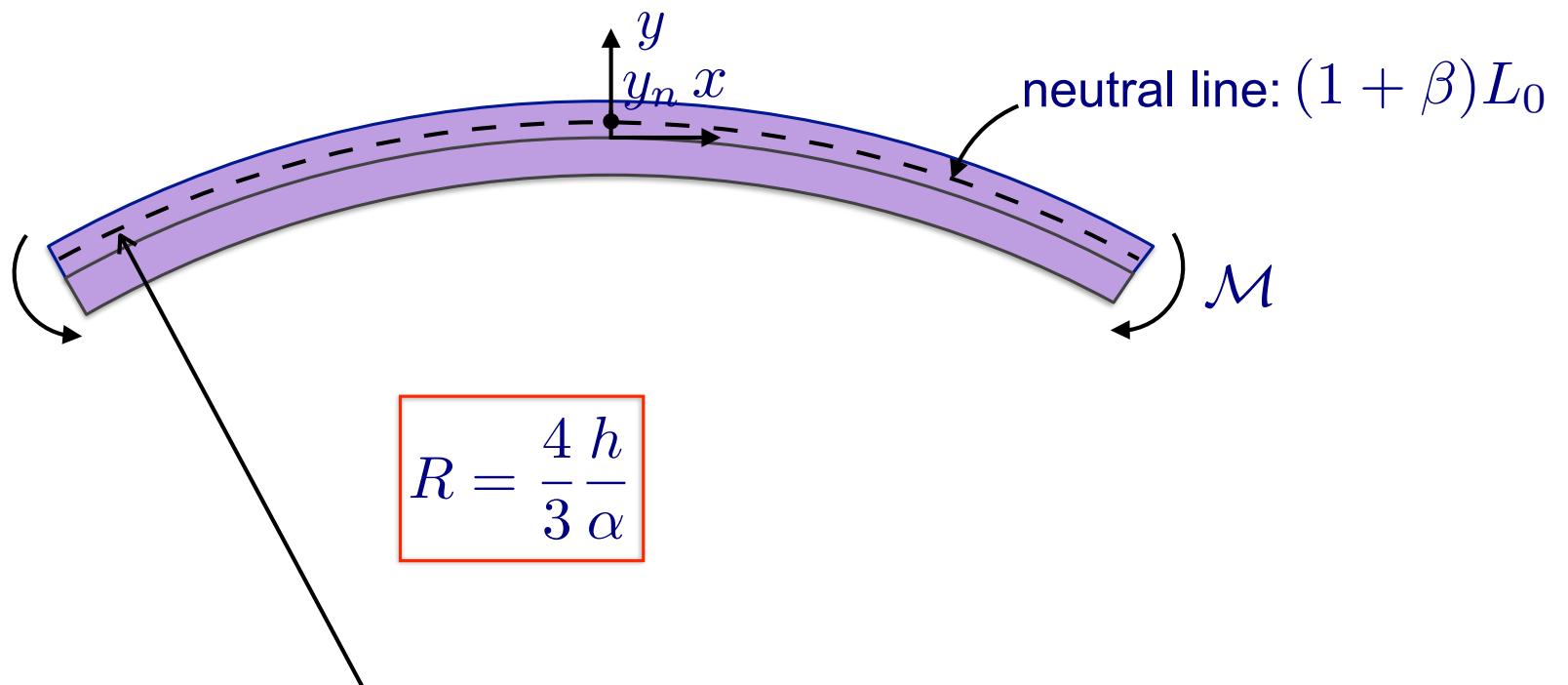
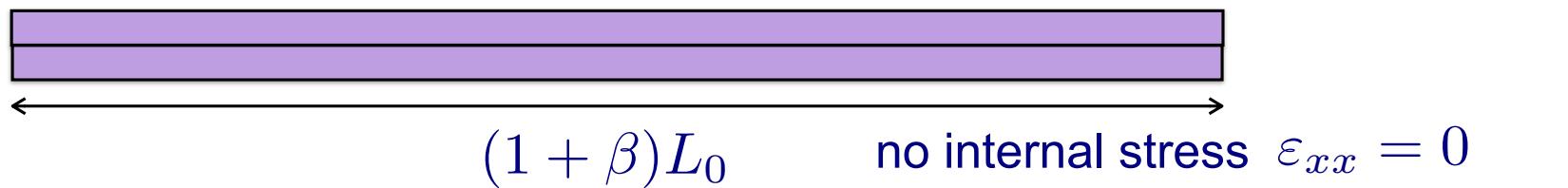
$$F_{ext} = 0 \Rightarrow \int_{-h}^h \sigma_{xx}(y) dy = 0$$

$$\int_{-h}^h (y - y_n) dy = 0 \Rightarrow \boxed{y_n = 0}$$

# Superposition



# Superposition



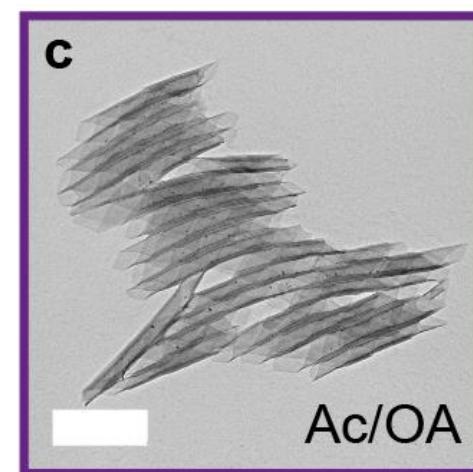
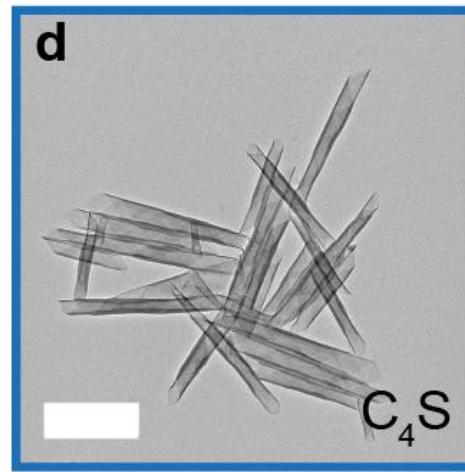
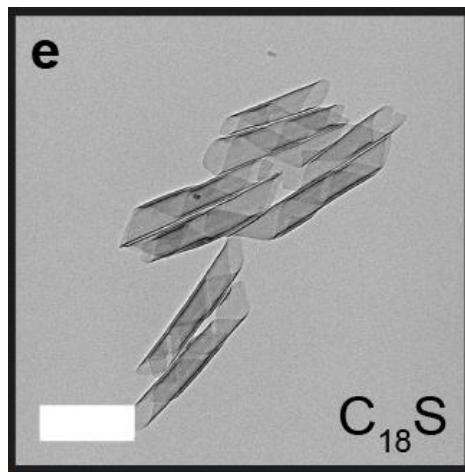
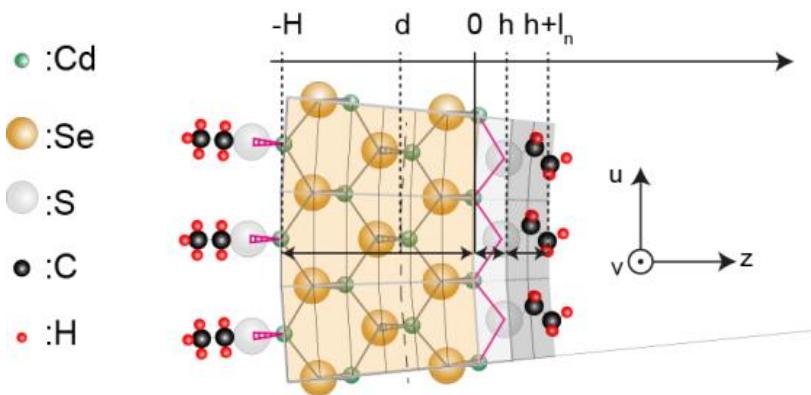
$$R = \frac{4}{3} \frac{h}{\alpha}$$

general case

$$R = \frac{E_1 h_1^4 + E_2 h_2^4 + 6E_1 E_2 h_1^2 h_2^2 + 4E_1 E_2 h_1 h_2 (h_1^2 + h_2^2)}{6E_1 E_2 h_1 h_2 (h_1 + h_2) \alpha}$$

and more complex if  $\eta_1 \neq \eta_2$

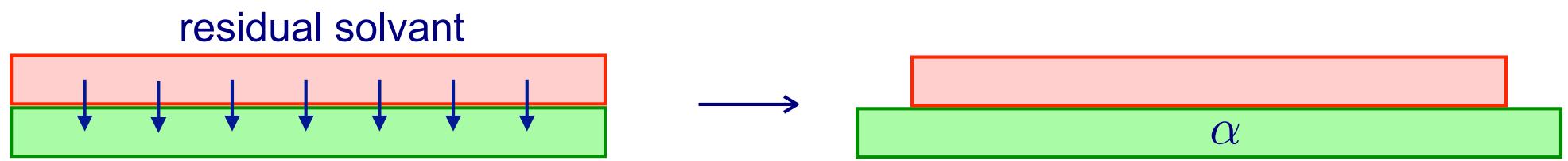
# Also at small scale



$\text{CdSe}$  nanoplatelets + ligands  $\Rightarrow$  surface stress

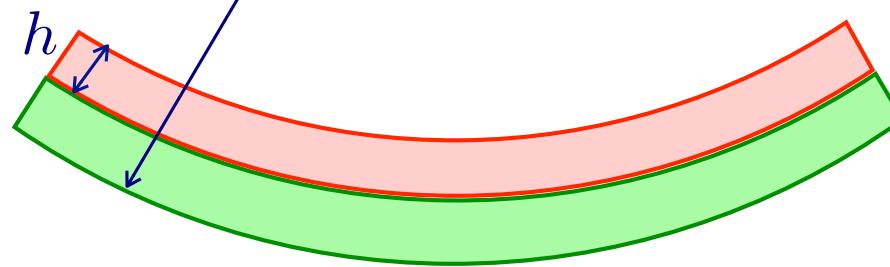
Hong Po & Sandrine Ithurria

# Bilayer sheets



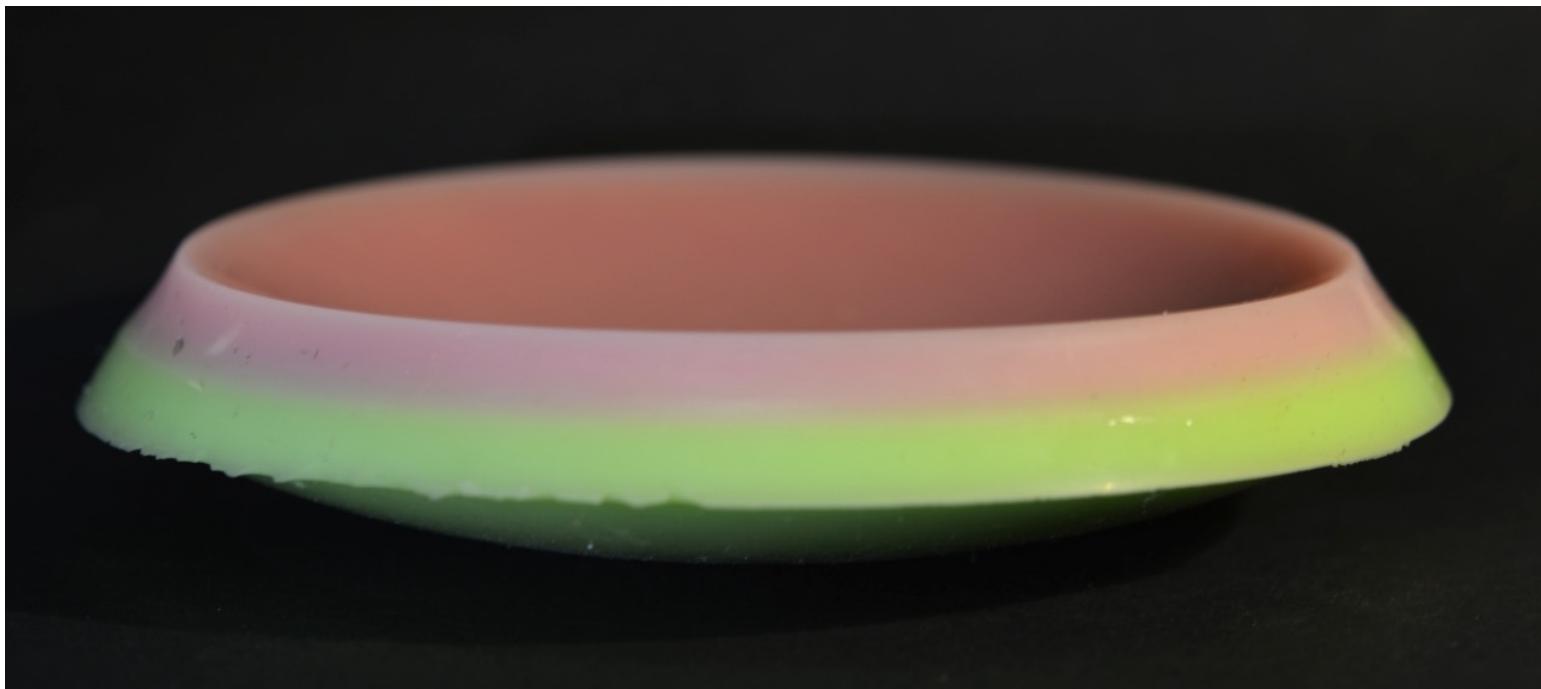
natural curvature:

$$R \sim h/\alpha$$



in 2D ?

## Thick bilayer

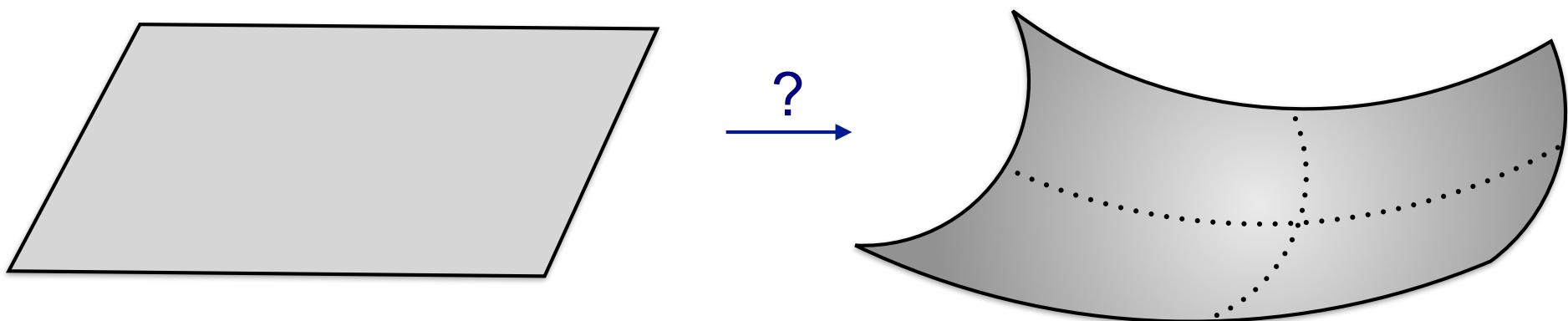


## Thin bilayer: frustrated rolling

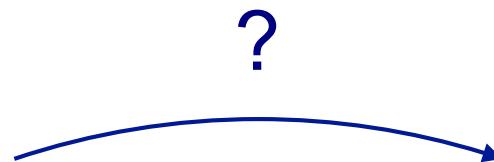
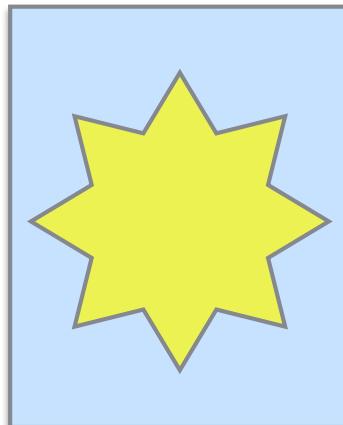


*M.Pezzulla, P.Nardinocchi & D.Holmes (2016)*

Bending a sheet in 2 directions?



# Tag on a bottle





# Curvatures



$$R_2 \leftarrow R_1$$

$$R_2 \leftarrow R_1$$

$$R_2 = \infty$$

$$R_1$$



# Gauß theorem

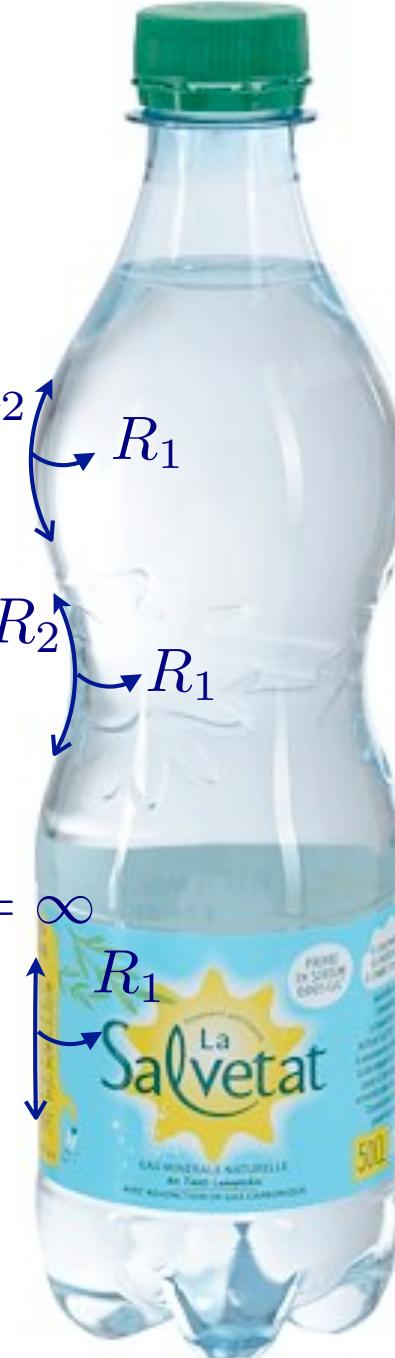
Gaussian curvature

$$K = \frac{1}{R_1} \frac{1}{R_2}$$

$$K > 0$$

$$K < 0$$

$$K = 0$$

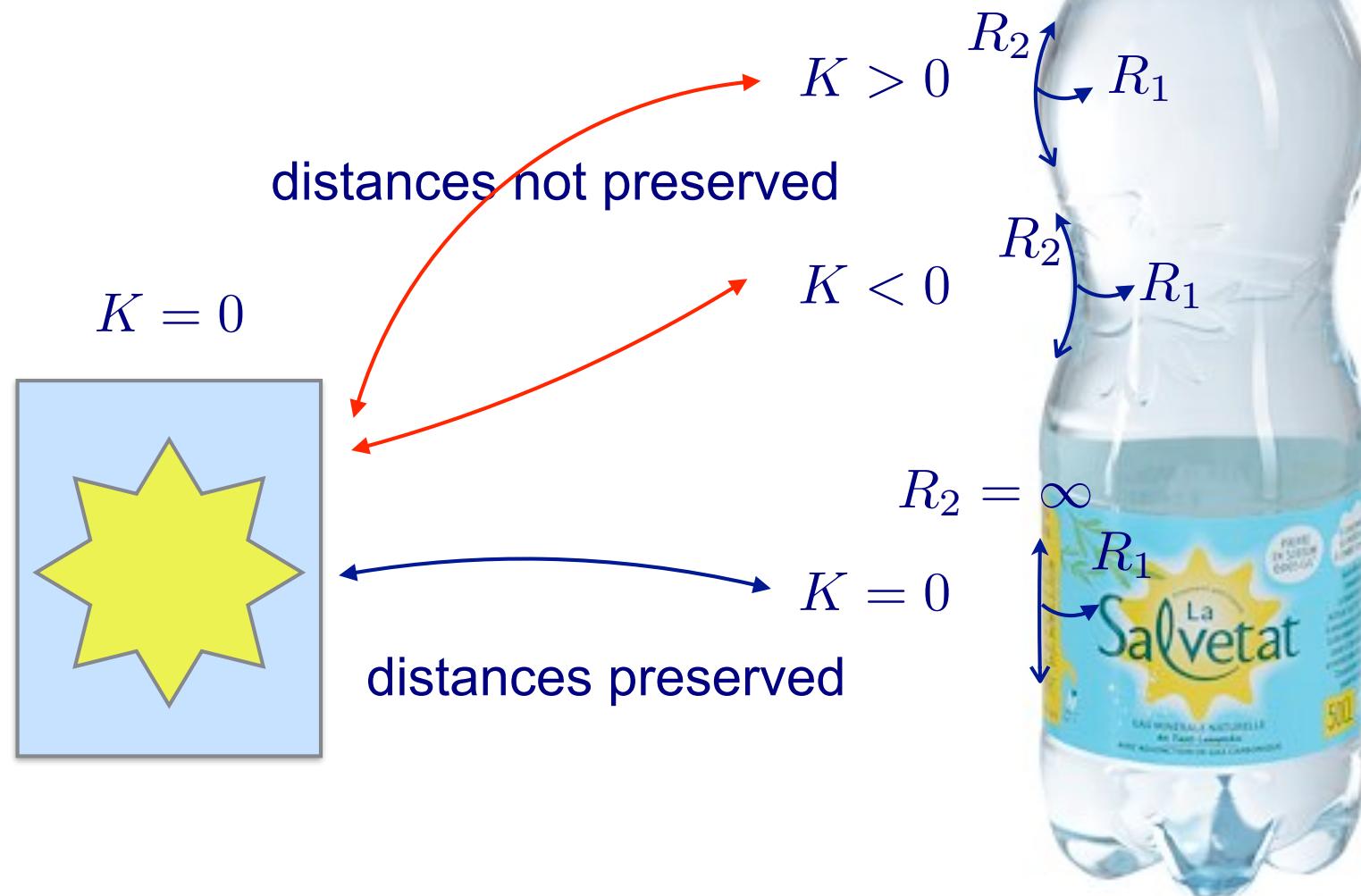




# Gauß theorem

Gaussian curvature

$$K = \frac{1}{R_1} \frac{1}{R_2}$$



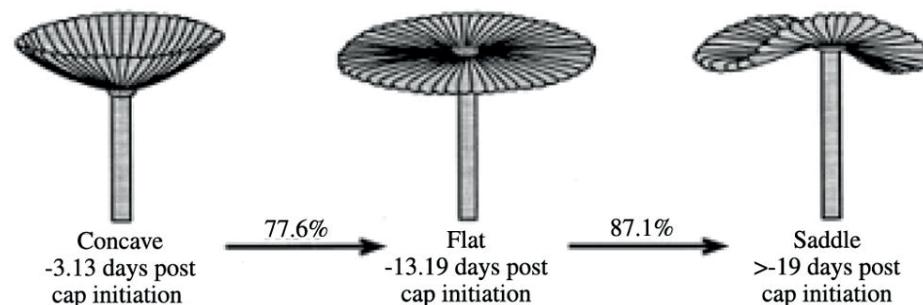
Challenging Gauß theorem ?

the cap of *acetabularia*



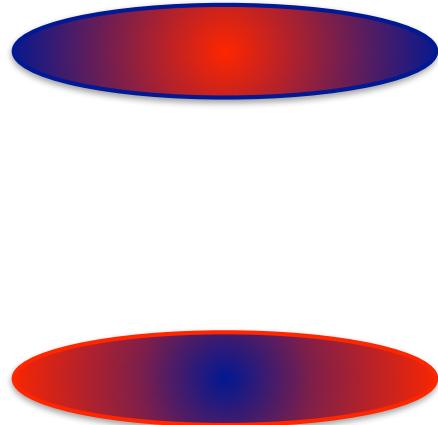
Shihira-Ishikawa  
[paleopolis.rederis.es](http://paleopolis.rederis.es)

# Non uniform/isotropic growth

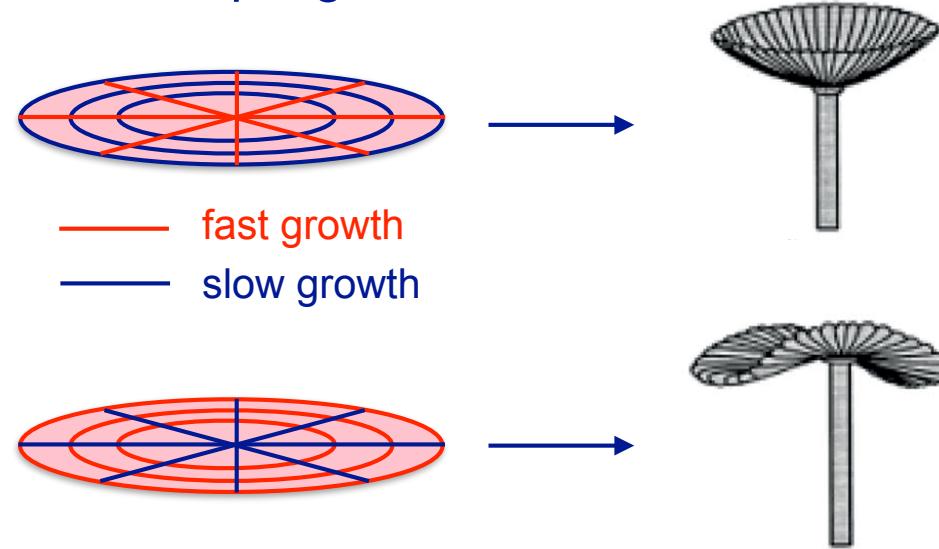


*Serikawa & Monadoli Planta (1998)*

non uniform growth



non isotropic growth



*Dervaux & Ben Amar PRL (2008)*  
*leaf growth: Arezki Boudaoud*

# Inflatable rubber patches



Top view

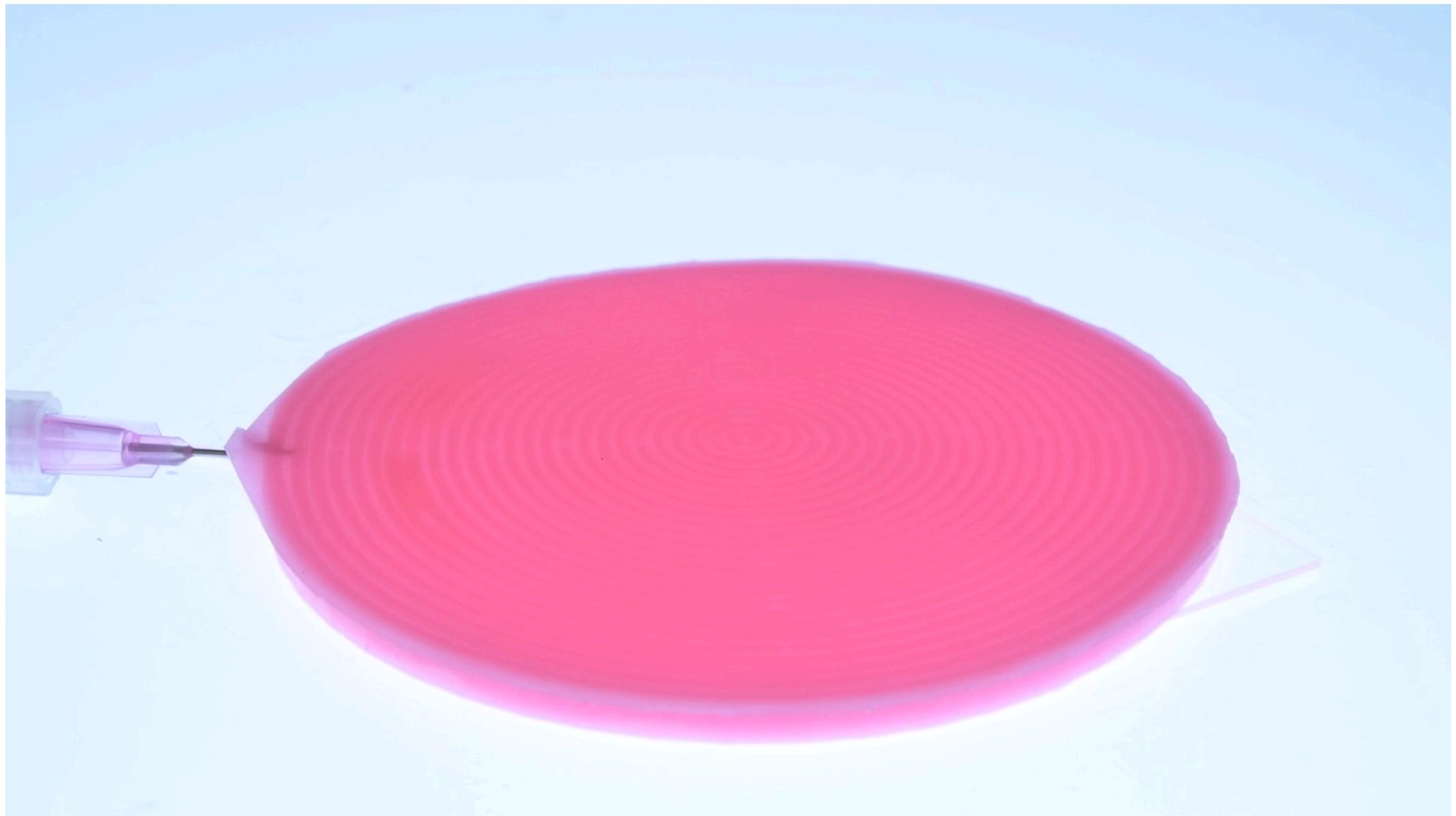


Side view

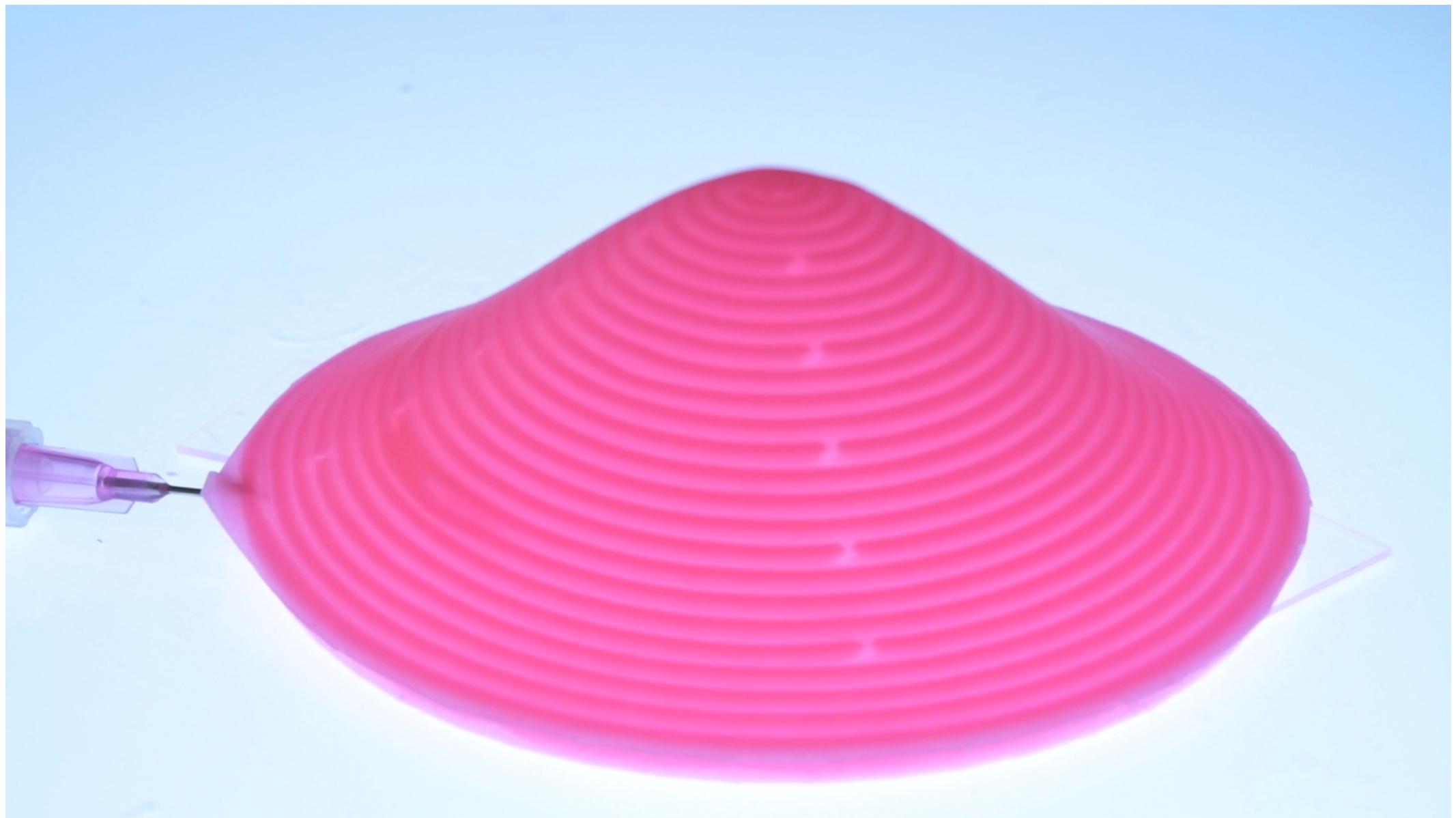


*Siéfert et al., Nature Materials (2018)*

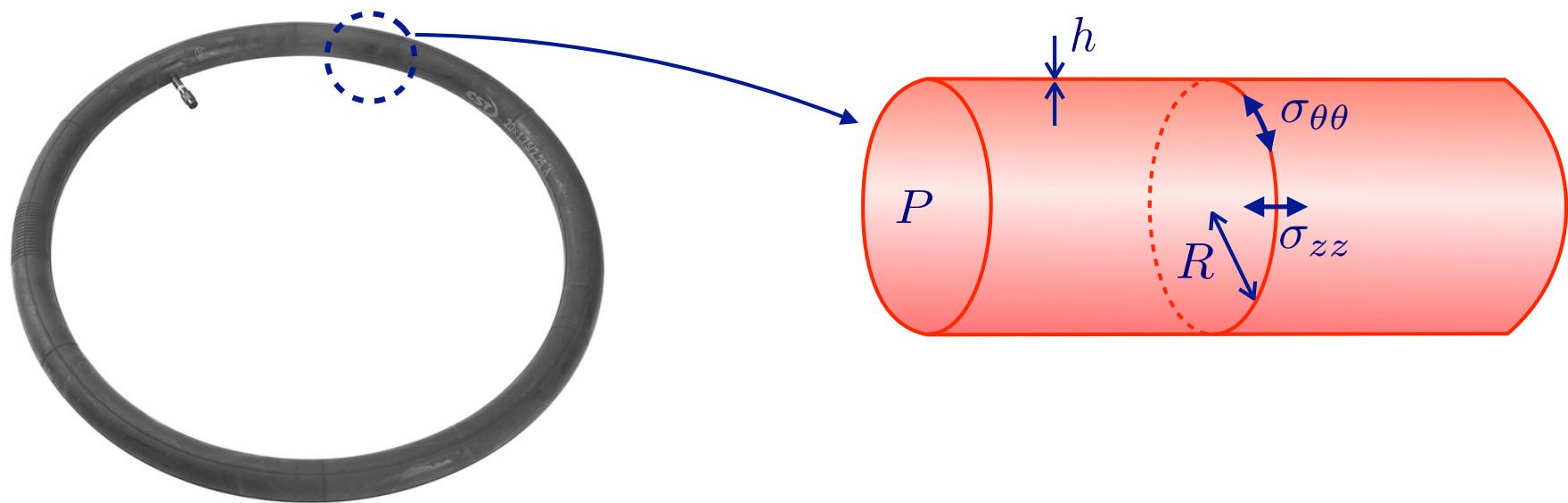
# Inflatable rubber patches



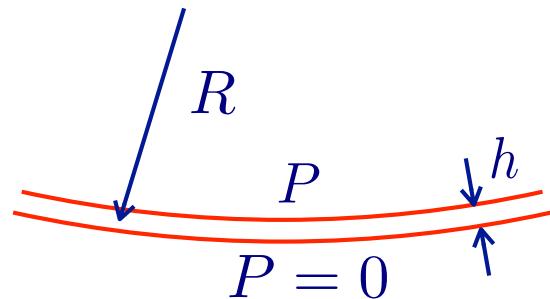
# Inflatable rubber patches



# Inflating a tube

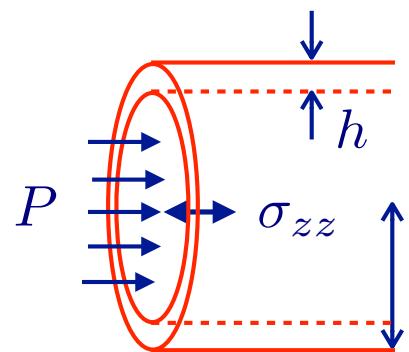


# Inflating a tube



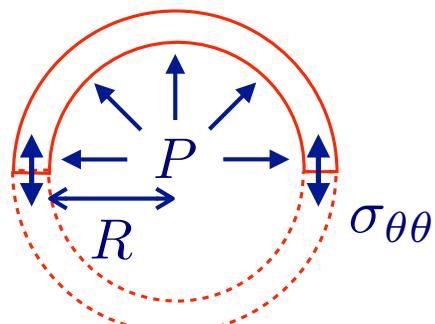
$$h \ll R$$

$$0 \leq |\sigma_{rr}| \leq P$$



$$\pi R^2 P = 2\pi R h \sigma_{zz}$$

$$\sigma_{zz} = \frac{R}{2h} P$$



$$2R P = 2h \sigma_{\theta\theta}$$

$$\sigma_{\theta\theta} = 2\sigma_{zz} = \frac{R}{h} P \gg \sigma_{rr}$$

# Inflating a tube

Hook's law for linear elasticity:

$$\varepsilon_{11} = \frac{1}{E} [\sigma_{11} - \eta(\sigma_{22} + \sigma_{33})]$$

$$\varepsilon_{12} = \frac{1 + \eta}{E} \sigma_{12} \quad + \text{ permutations } 1, 2, 3$$

$$\text{with } \varepsilon_{ij} = \frac{1}{2} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

$$\varepsilon_{\theta\theta} = \frac{1}{E} (\sigma_{\theta\theta} - \nu \sigma_{zz}) = \frac{3}{4} \frac{R}{Eh} P$$

$\nu \simeq 0.5$  for rubber

$$\varepsilon_{zz} = \frac{1}{E} (\sigma_{zz} - \nu \sigma_{\theta\theta}) = 0$$

# Pipe failure



$$\sigma_{\theta\theta} = 2\sigma_{zz}$$

# Inflatable rubber patches



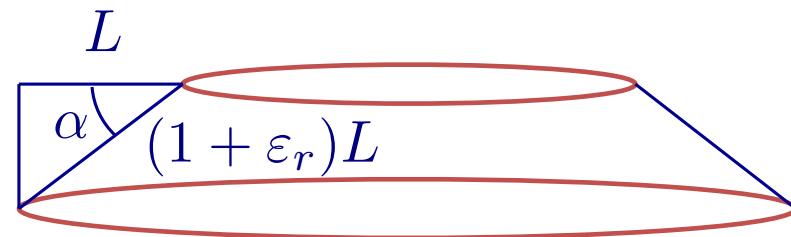
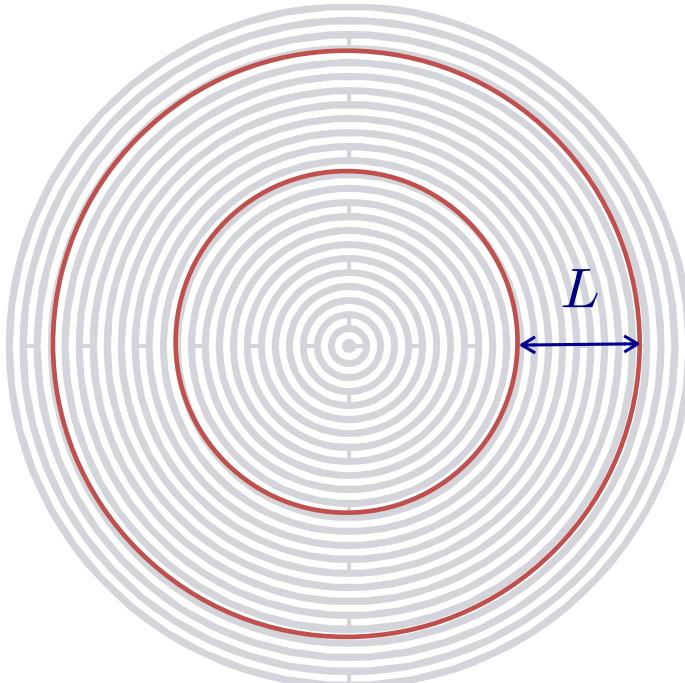
Top view



Side view

*Siéfert et al., Nature Materials (2018)*

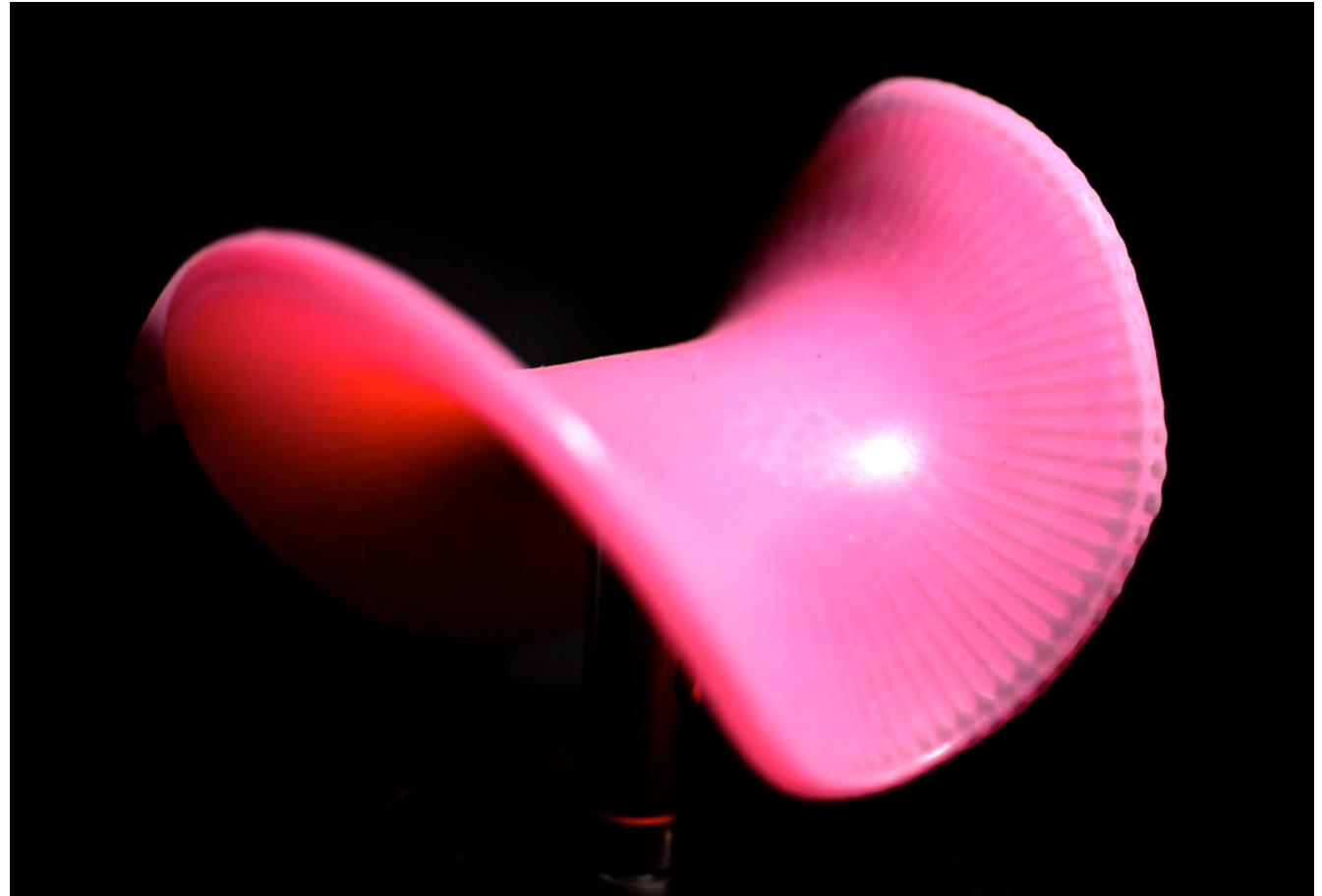
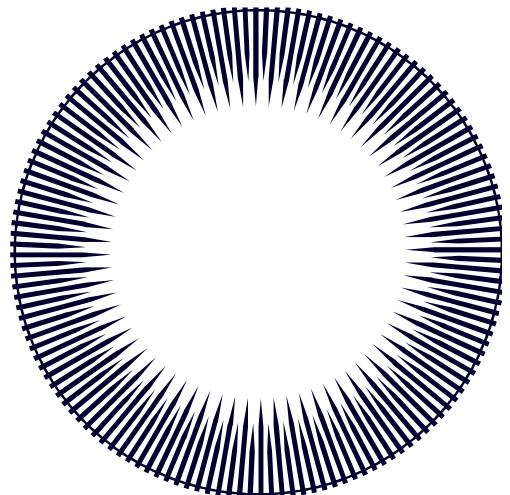
# Geometrical limit (bending negligible)

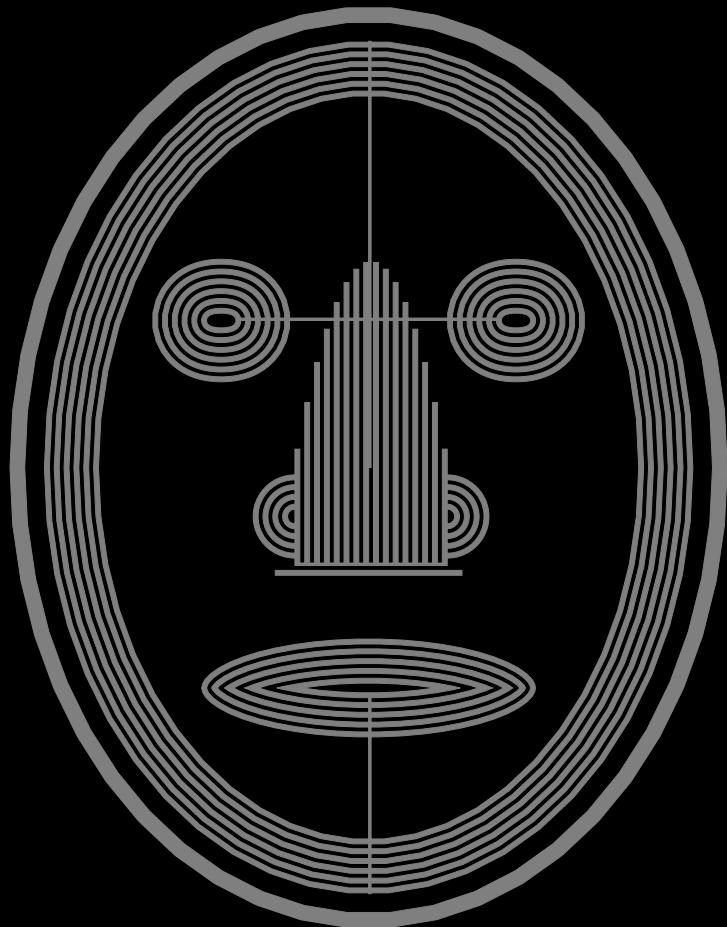


$$\varepsilon_\theta \simeq 0$$

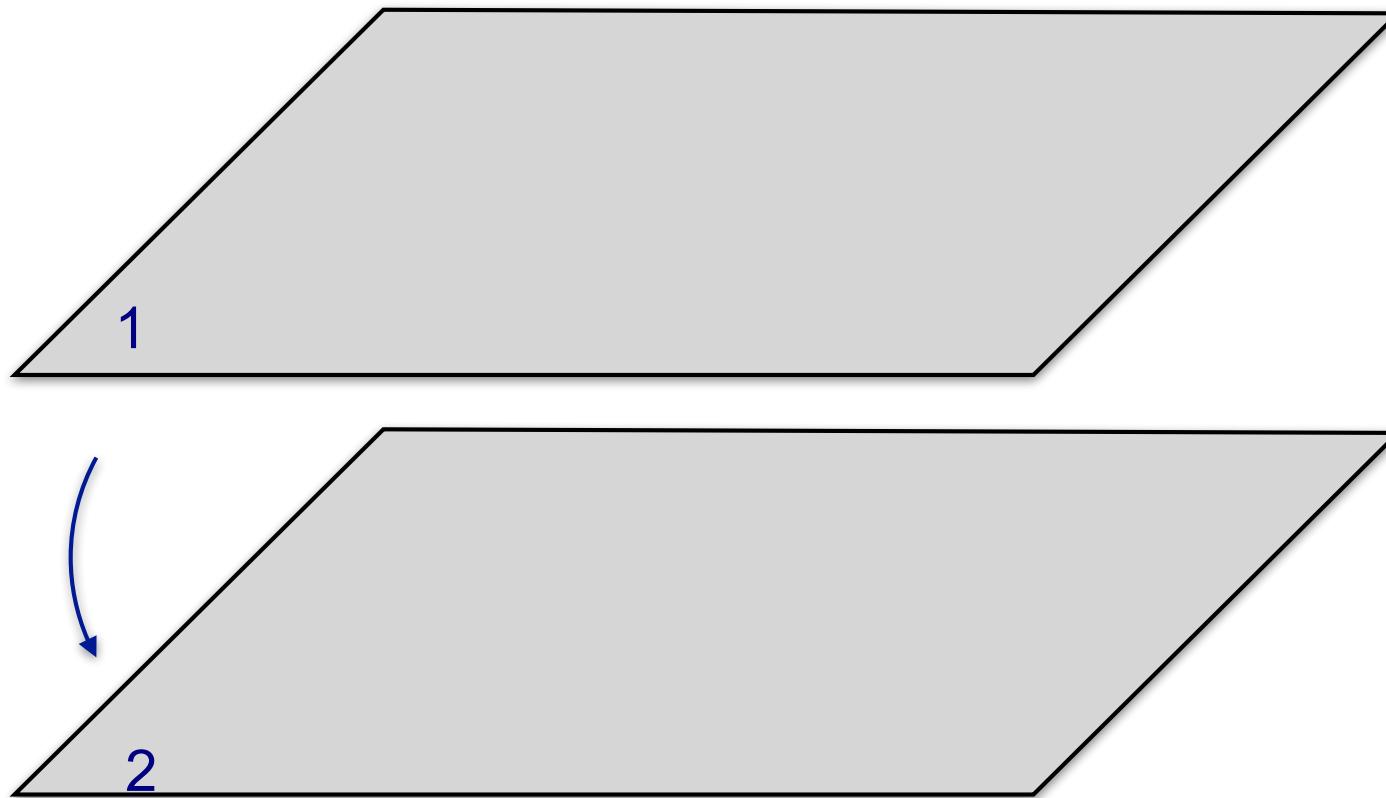
$$\cos \alpha = \frac{1}{(1 + \varepsilon_r)}$$

# Radial channels





# Inflatable fabrics



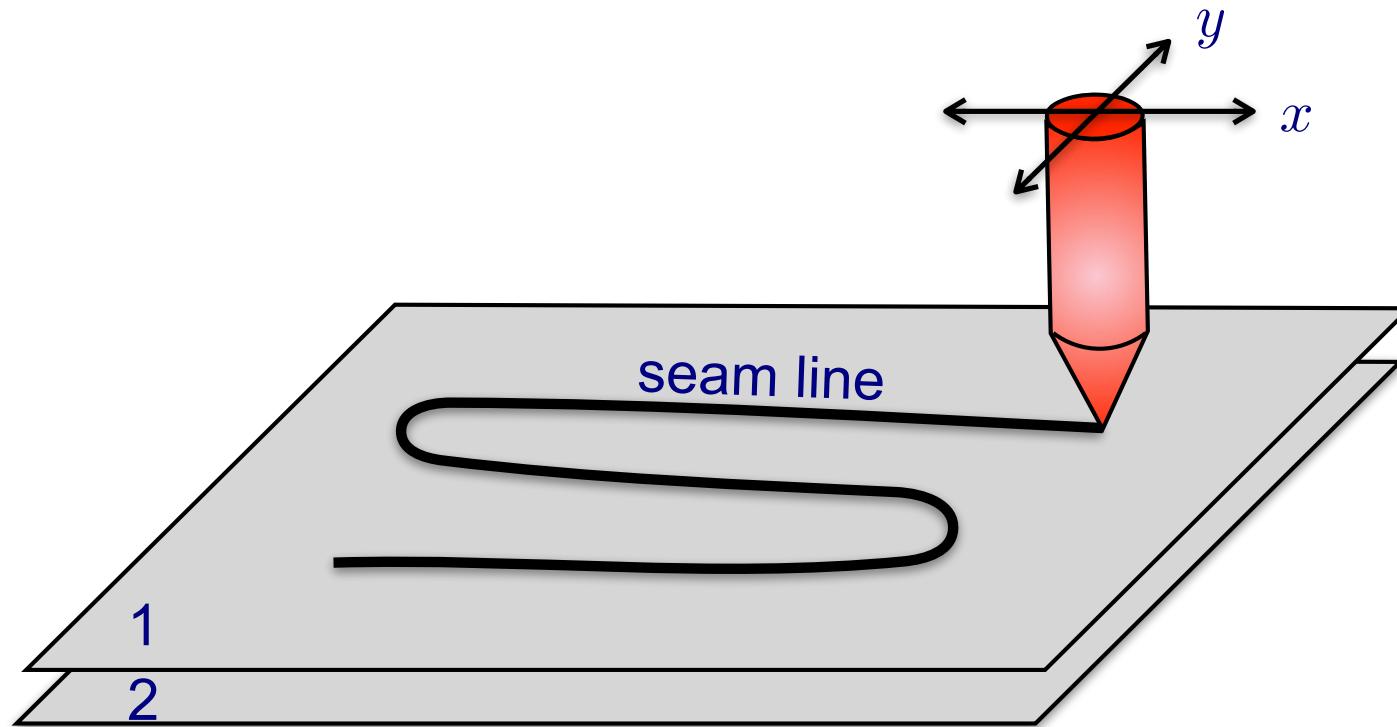
fabric coated with thermo-sealable polymer

# Inflatable fabrics



fabric coated with thermo-sealable polymer

# Inflatable fabrics

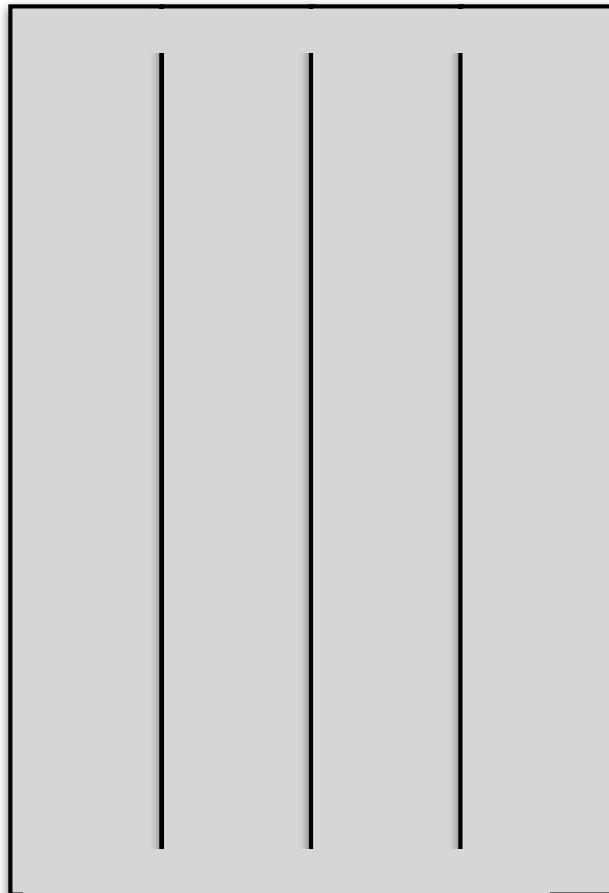


fabric coated with thermo-sealable polymer

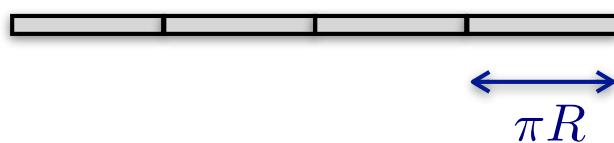
# Inflatable fabrics

$$P = 0$$

top view



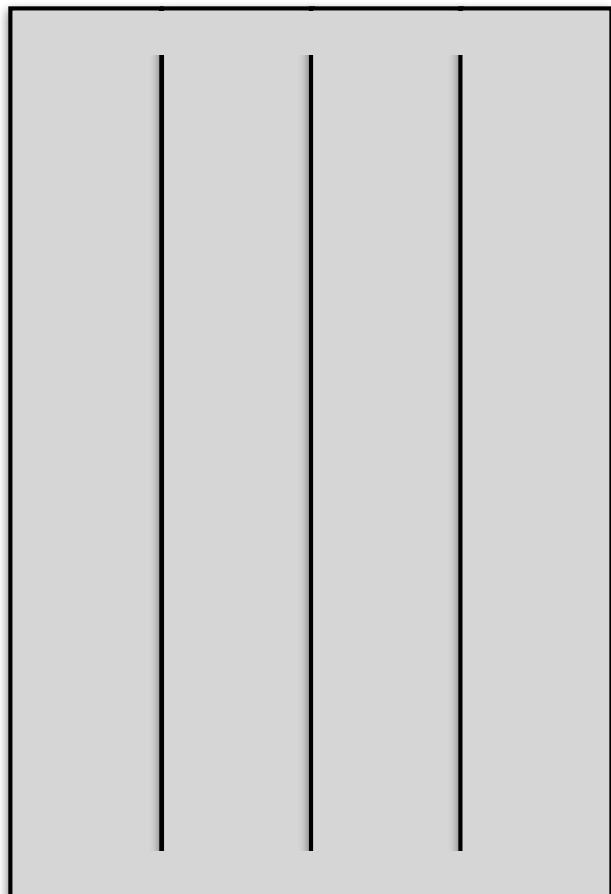
cross section



# Inflatable fabrics

$$P = 0$$

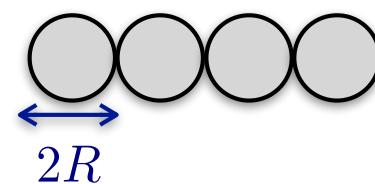
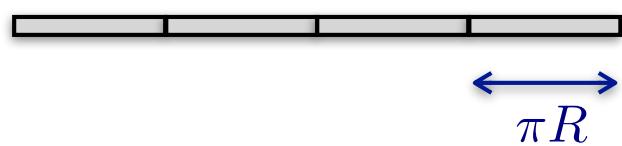
top view



$$P > 0$$



cross section



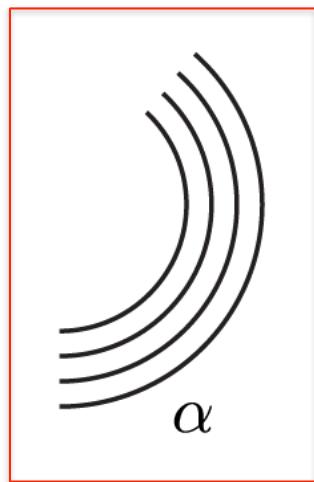
# Inflatable fabrics



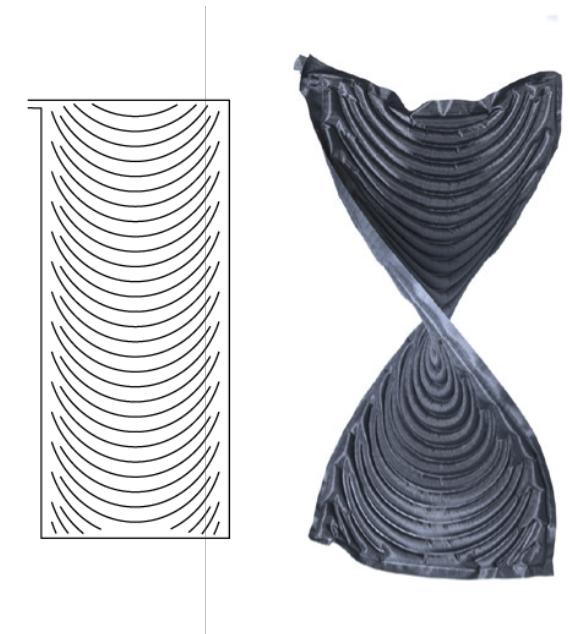
# Inflatable fabrics



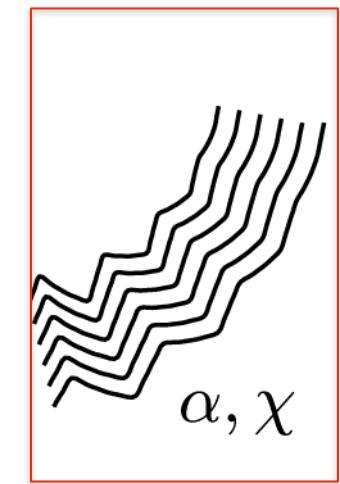
# Different morphing strategies



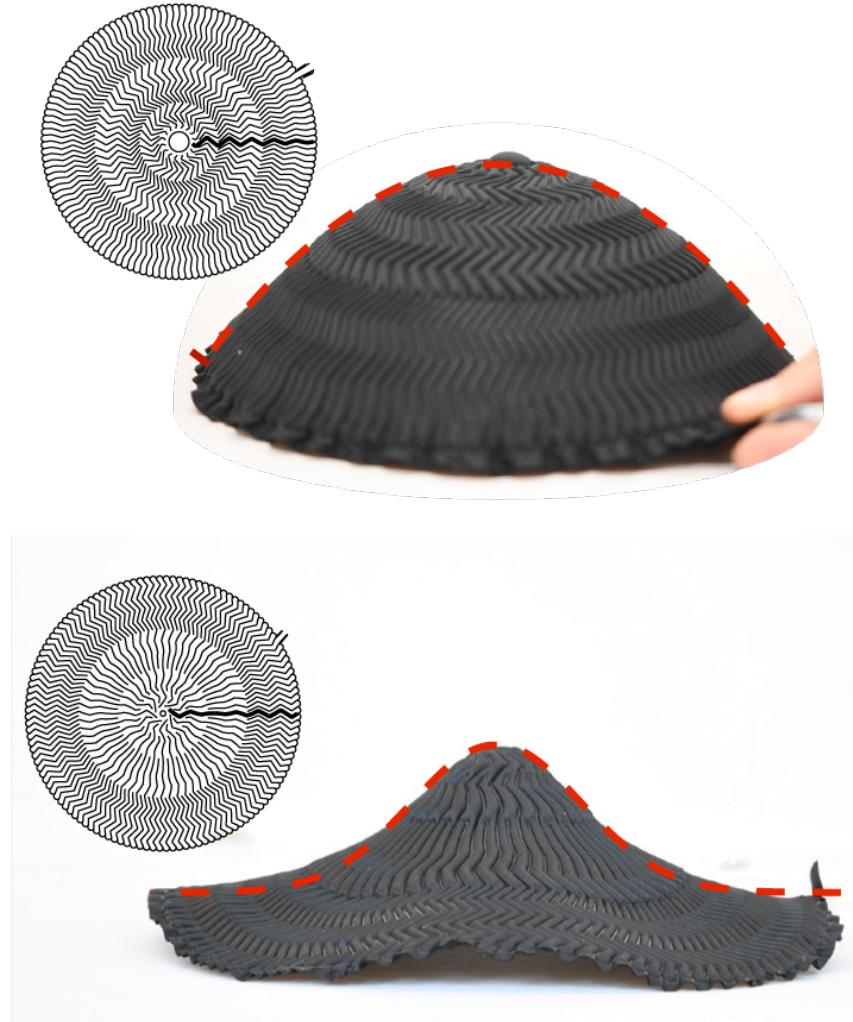
channels direction



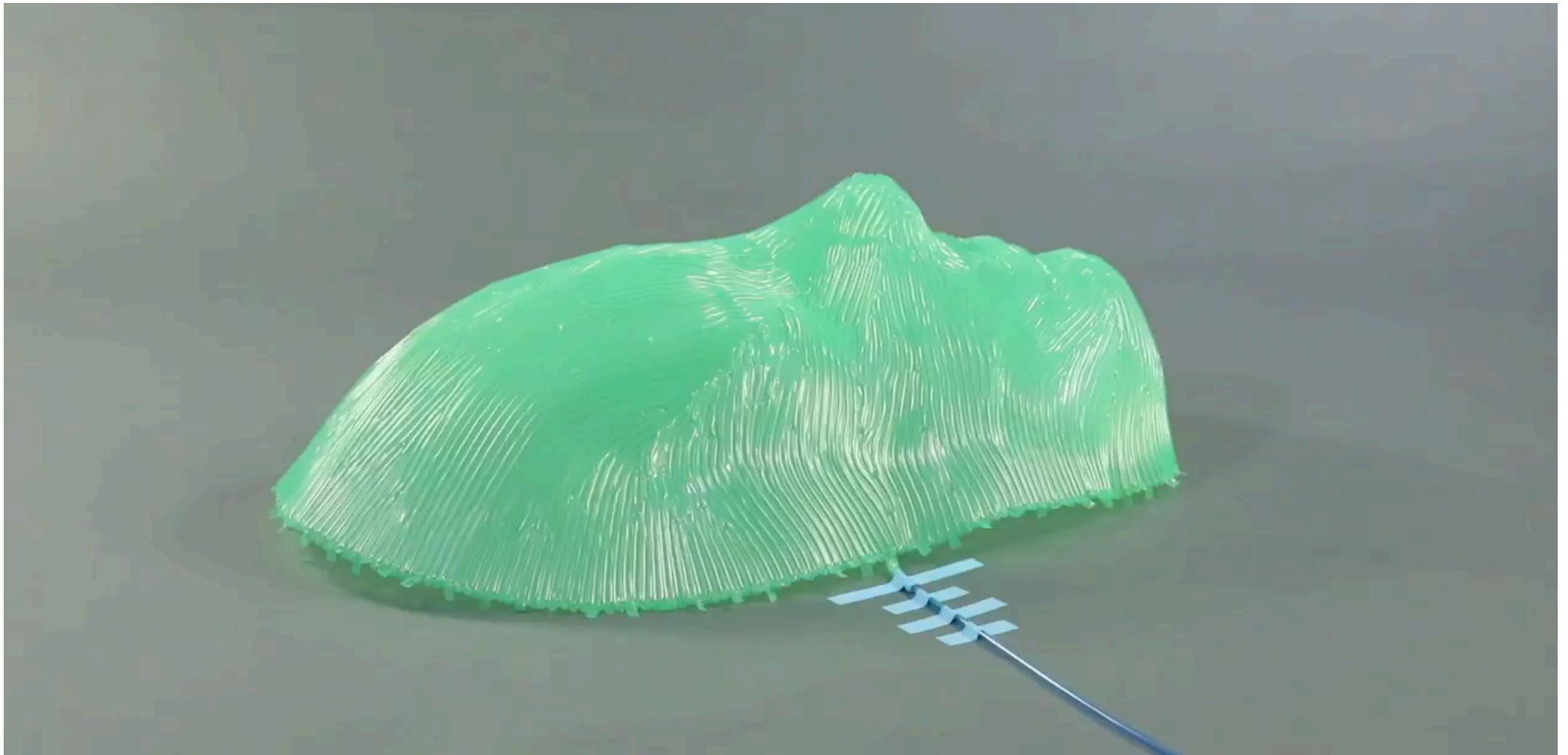
# Zigzags



zig-zags  
↑  
orientation  
+  
contraction ratio



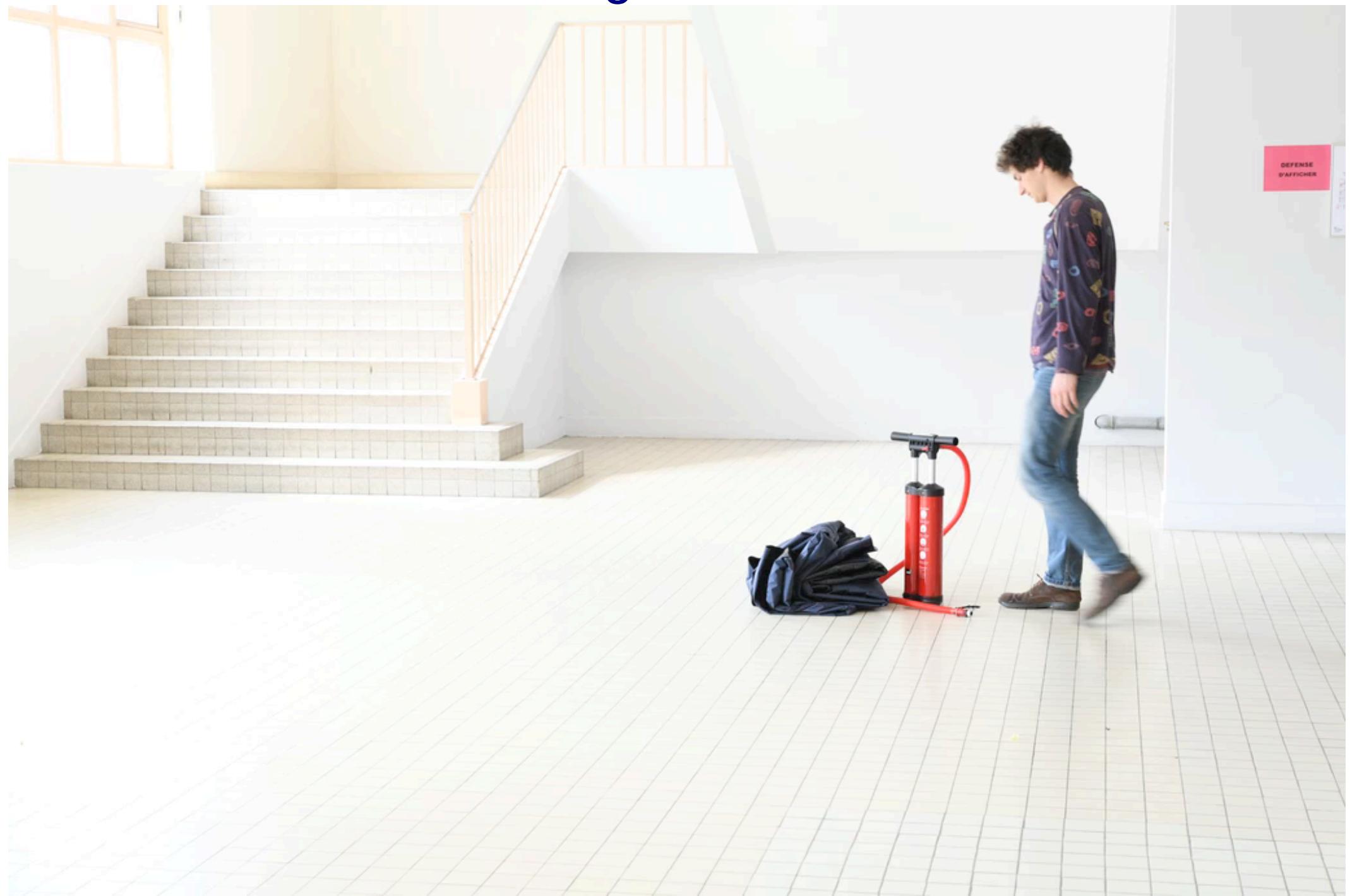
# Reverse engineering?



*collaboration Julian Panetta & Mark Pauly (EPFL)*

*Panetta et al., ACM Transactions on Graphics (2021)*

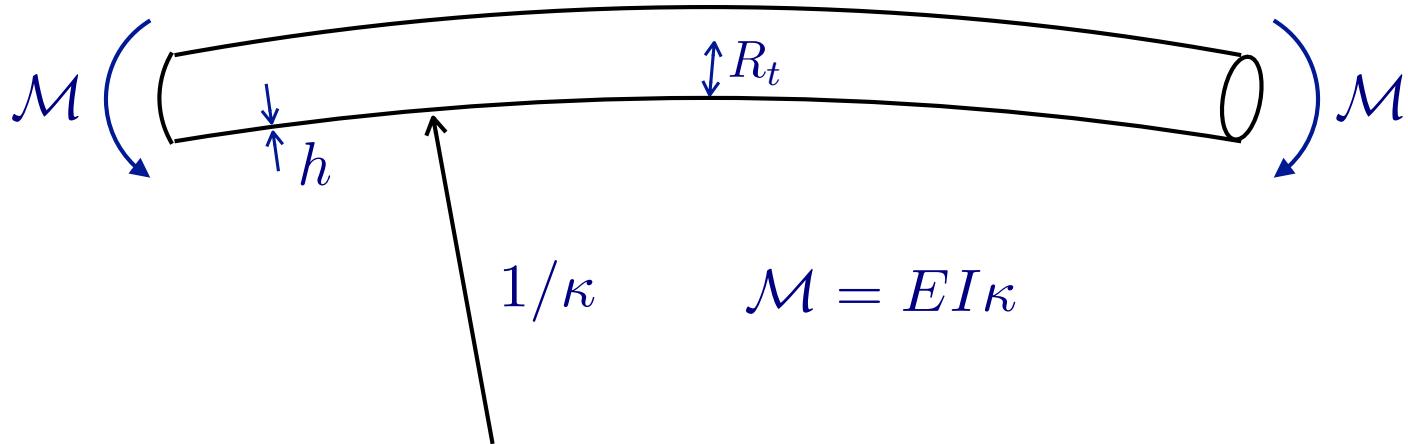
# Large scales



# Large scales



## Stiffness



$$I = \frac{\pi}{4}(R_t + h)^4 - \frac{\pi}{4}R_t^4 \simeq \pi R_t^3 h$$

But failure for  $\sigma_{zz} \lesssim 0$        $\frac{R_t}{2h}P - ER_t\kappa_c \simeq 0$   
inflation bending

$$\kappa_c \simeq \frac{1}{2h} \frac{P}{E}$$

$$\mathcal{M}_c \simeq \frac{\pi}{2} R_p^3$$